

AD-A048 840

MCDONNELL DOUGLAS ASTRONAUTICS CO HUNTINGTON BEACH CALIF F/G 1/1
AERODYNAMIC COMPUTER CODE FOR COMPUTING PRESSURE LOADING ON COM--ETC(U)
JAN 78 K K WANG
MDC-67215

UNCLASSIFIED

NL

1 OF 3

ADAO48840



ADA 048840

122
MDC-67215 NW

6
AERODYNAMIC COMPUTER CODE FOR COMPUTING
PRESSURE LOADING ON COMPLETE MISSILE FOR STRUCTURAL ANALYSIS

AD No. _____
DDC FILE COPY

10
Prepared by Kenneth K. Wang

MCDONNELL DOUGLAS ASTRONAUTICS COMPANY
5301 BOLSA AVENUE
HUNTINGTON BEACH, CALIFORNIA 92647

14
MDC-67215

11
JAN 1978

12 248p.

9 Final rept. 1 Jan 76-31 Dec 77.

15 FINAL REPORT
CONTRACT NUMBER N60921-76-C-0164
JUNE 1, 1976 TO DECEMBER 31, 1977

Approved for Public Release
Distribution Unlimited

DDC
RECEIVED
JAN 19 1978
D

Prepared for
NAVAL SURFACE WEAPONS CENTER
WHITE OAK, SILVER SPRING, MARYLAND 20910

389 310

COPY AVAILABLE TO DDC DOES NOT
PERMIT FULLY LEGIBLE PRODUCTION

This technical report has been reviewed and is approved.

A handwritten signature in dark ink, appearing to read 'P. C. Huang', written in a cursive style.

P. C. Huang
Naval Surface Weapons Center

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

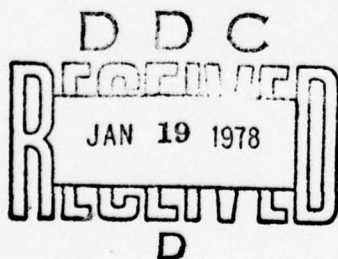
REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER MDC G7215 ✓	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Aerodynamic Computer Code for Computing Pressure Loading on Complete Missile for Structural Analysis		5. TYPE OF REPORT & PERIOD COVERED Final Report June 1, 1976 to December 31, 1977
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Kenneth K. Wang		8. CONTRACT OR GRANT NUMBER(s) N60921-76-C-0164 <i>new</i>
9. PERFORMING ORGANIZATION NAME AND ADDRESS McDonnell Douglas Astronautics Company 5301 Bolsa Avenue Huntington Beach, California 92647		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Surface Weapons Center White Oak Silver Spring, Maryland 20910		12. REPORT DATE January 1978
		13. NUMBER OF PAGES 212
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) For public release, distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Aerodynamics Pressure distribution on missile or its components Structural analysis		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Aerodynamic computer code for calculating the pressure distribution on missile or its components e. g., body and wings and to interpolate by surface fit at locations as specified for structural analysis using the NASTRAN computer code.		

PREFACE

This document reports the work performed by McDonnell Douglas Astronautics Company for the Naval Surface Weapons Center, White Oak Laboratory, Silver Spring, Maryland for the development of an aerodynamic code for computing pressure loads on a missile and/or its components. The work was accomplished under contract number N60921-76-C-0164. The Naval Sea Systems Command sponsored the activity.

An MDAC aerodynamic code was extensively modified to accept missile geometry and finite element descriptions from the NSWC computer codes PING and BING to compute pressure loading on the missile and to interpolate by surface fit the pressure load at specified locations in a NASTRAN bulk data format.

The theoretical background of the method is described briefly in this report. Computer code organization and input parameters are described in detail. For the user's convenience, test cases and instructions are included.



ACCESSION for	
NTIS	White Section <input checked="" type="checkbox"/>
DDC	Ref Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
JUSTIFICATION.....	
BY.....	
DISTRIBUTION/AVAILABILITY CODES	
Dist.	AVAIL. and/or SPECIAL
A	33 E-4

CONTENTS

	LIST OF SYMBOLS	vii
	SUMMARY	ix
Section 1	INTRODUCTION	1
Section 2	AERODYNAMIC THEORY AND SURFACE SPLINE FIT METHOD	3
	2.1 Aerodynamic Theory	3
	2.2 Surface Spline Fit	10
	2.2.1 Theoretical Discussion	11
	2.2.2 Application	12
Section 3	COMPUTER PROGRAM	13
	3.1 Capabilities of the MDAC Aero Code	13
	3.2 Program Input Description	14
	3.3 Various Restrictions and Code Changes Required for Their Removal	22
	3.3.1 Input Parameters	22
	3.3.2 Finite Element and Grid Point	23
Section 4	TEST CASES	25
	4.1 Input Arrangements and Output Printout	25
	4.2 Results of Computation	25
	4.3 Input Cards for Test Cases	30
	4.3.1 Body Only Case	30
	4.3.2 Wing Only Case	33
	4.3.3 Complete Missile Case	38
	4.4 Output Printout of Test Cases	43
	4.4.1 Body Only Case	43
	4.4.2 Wing Only Case	51
	4.4.3 Complete Missile Case	65
Section 5	CONCLUSIONS AND RECOMMENDATIONS	87
Section 6	REFERENCES	89
Appendix A	PROGRAM LISTING	91



LIST OF SYMBOLS

k, K	Interpolation coefficients
u, v, w	Perturbation velocities
x, y, z	Coordinates
ξ, η	Integration variables
ϕ	Potential functions
L	Slope of panel sweep, $\tan \Lambda$
M_∞	Free-stream Mach number
N	Number of data points to be interpolated
P	Pressure load
r	Radial distance
δ	Deflection

SUMMARY

This report represents the work performed under contract number N60921-76-C-0164 for the Naval Surface Weapons Center, White Oak Laboratory, Silver Spring, Maryland under Naval Sea Systems Command sponsorship for the development of an aerodynamic code for computing distributed pressure loads on a missile or its components such as wings, body or tails.

Major modifications were made to the existing MDAC aerodynamic code to streamline the input format, restructure the code and reduce the computer core memory requirement. In addition, new subroutines were developed as necessary to provide versatility in the input specification, efficient computation and informative outputs. The input parameters have been reduced to simplify input preparation. Automated generation of wing camber, thickness and twist directly from the wing surface description has been incorporated. Allowances were made in specifying the finite element in a coordinate system other than that used for aerodynamic calculations. At the completion of aerodynamic analysis, the code generates the pressure distribution on the missile at the centroid of each finite element as specified. They are produced as punched card output in a NASTRAN bulk card format as desired.

Section 1

INTRODUCTION

The design and analysis of flight vehicles requires coordinated, joint efforts among various technical disciplines such as structures, aerodynamics, flight kinetics, and propulsion. For example, aerodynamic calculations provide the loading to be used in the structural analyses, and configuration changes caused by bending, erosion, damage, etc., necessitate renewed aerodynamic calculations. With the development of high-speed, large-capacity computers, the analysis performed for individual disciplines has been highly automated into computing codes capable of analyzing very complex configurations by appropriate modeling for structures, notably NASTRAN (Reference 1), and various finite-element, lifting-surface-theory codes for aerodynamics (References 2 and 3). Since these codes were developed independently of each other, and major physical modeling differences exist among disciplines, some interfacing tasks must be performed when the output of one code is supplied as input of the other. These tasks have been performed manually in the past and can become cumbersome if the analysis requires numerous iterations between the disciplines. It is therefore both desirable and necessary to develop an aerodynamics code to interface with NSWC finite-element generating code PING or BING (References 4 and 5) and NASTRAN structure codes as an initial step toward a more automated design procedure.

A variety of aerodynamics codes applicable to different speed regimes and vehicle configurations are available at MDAC. For present purposes it was decided to modify an existing MDAC finite-element code, which is based on Woodward's method of aerodynamic influence coefficients (Reference 3). As opposed to other available finite-element methods of aerodynamic prediction (Reference 2), Woodward's method has the unique capability of being applicable in both the subsonic and low-supersonic ($M_\infty < 3$) speed regimes. Although the method is theoretically deficient at transonic Mach numbers, predictions for wing-body combinations have been shown to be acceptable. A detailed description of the method will be found in Section 2.

At the conclusion of aerodynamic calculations, the present code generates the pressure loads on a missile (body, wings and nacelles) at the control point of surface panels. Interpolation and rearrangement of the pressure load to suit structural analysis will be required because, in general, placement of the panel is mainly governed by aerodynamic considerations. For this purpose, an efficient and versatile interpolation method is selected.

Many factors entered into the selection of the surface spline fit method for interpolating the pressure loads. In the present case, the method based on the differential equation relating deflection and load of thin plates (Reference 6) was considered to be the most suitable one. It requires less core storage and is extremely simple to code. Furthermore, the method accepts input data either in a regular form or randomly distributed.

The final output of the code is the pressure load at the centroid of each finite element. For structural analysis, these data are produced as punched cards in the NASTRAN bulk data format.

It may be mentioned that this described approach was employed in an initial effort in the development of a MDAC aero code for interface with the NSWC finite-element code PING for pressure loads on missile wings (contract number N60921-75-C-0069). The success achieved and the experience gained in the effort have been most helpful to the present work. In particular, improvements such as input simplification and coordinate system flexibility have been incorporated as a direct result of this earlier effort.

Section 2

AERODYNAMIC THEORY AND SURFACE SPLINE FIT METHOD

The MDAC aerodynamic code modified for computing pressure loads on a missile for structural analysis is based on the method of influence coefficients developed by Woodward (Reference 3). The code provides the pressure load at the control point of each panel as defined in the program. For structural analysis the pressure distribution needs to be interpolated at the centroid of each finite element. An efficient surface spline method is employed for this purpose.

In the following subsections, both the aerodynamic theory and the surface spline method are discussed.

2.1 AERODYNAMIC THEORY

For small perturbations, the governing equation of potential flow can be simplified greatly and solution of many problems becomes possible. The present code solves the linearized, three-dimensional potential equation

$$(1 - M_{\infty}^2) \phi_{xx} + \phi_{yy} + \phi_{zz} = 0 \quad (1)$$

derived from the exact equations of motion by neglecting all terms containing squares of higher powers of the perturbation velocities. Except for the case of transonic flow ($M_{\infty} \sim 1$), Equation 1 is valid for both subsonic ($M_{\infty} \lesssim 1$) or supersonic flows ($1 < M_{\infty} < 3$). For hypersonic flow ($M_{\infty} \gg 3$), the equation requires additional terms to be applicable. It should be noted here that the coordinate system used for aerodynamic analysis follows the accepted convention with the x-axis in the direction of flow, z-axis positive upwards and y-axis completing the right-hand system.

Considering Equation 1, a number of fundamental solutions exist that can be used to solve the problem of computing pressures, forces, and moments over the wing and body of a missile. Physically speaking, they are known as

source, doublet, and vortex singularities. In the present treatment, the effect of body volume, incidence and camber are represented by line sources and doublets distributed along the body axis; the effects of wing thickness are represented by planar source distributions. Wing camber, twist, and angle-of-attack effects are represented by vortex distributions. As Equation 1 is linear, the sum of these fundamental solutions is also a solution. It only remains necessary to determine their strengths to satisfy the boundary condition on the body and wing surface, i. e., flow must be tangent to the surface at selected points. The interference effect of wing on the body is accounted for by additional vortex distributions on the body panel surface.

The fundamental solutions of the linear equation are well known (e. g., Reference 3). For instance, in integral form, the potential for line source is

$$\phi_1 = - \int \frac{\xi d\xi}{\left[(x-\xi)^2 + (1-M_\infty^2) r^2 \right]^{1/2}} \quad (2)$$

The potential for line doublets is

$$\phi_2 = \int \frac{\sin \theta \xi (x-\xi) d\xi}{\left[(x-\xi)^2 + (1-M_\infty^2) r^2 \right]^{1/2} r} \quad (3)$$

The potential for a constant source distribution is

$$\phi_3 = - \frac{C_1}{\pi} \iint \frac{d\xi d\eta}{\left\{ (x-\xi)^2 + (1-M_\infty^2) \left[(y-\eta)^2 + z^2 \right] \right\}^{1/2}} \quad (4)$$

The potential for a linearly varying source distribution is

$$\phi_4 = \frac{C_1}{\pi} \iint \frac{(L\eta - \xi) d\xi d\eta}{\left\{ (x-\xi)^2 + (1-M_\infty^2) \left[(y-\eta)^2 + z^2 \right] \right\}^{1/2}} \quad (5)$$

For constant pressure vortex distributions, the potential is

$$\begin{aligned} \phi_5 = & \frac{C_1}{\pi} \iint \frac{z(x-\xi) d\xi d\eta}{\left[(y-\eta)^2 + z^2 \right] \left\{ (x-\xi)^2 + (1-M_\infty^2) \left[(y-\eta)^2 + z^2 \right] \right\}^{1/2}} \\ & + \frac{1-C_1}{\pi} \iint \frac{z d\xi d\eta}{(y-\eta)^2 + z^2} \end{aligned} \quad (6)$$

where

$C_1 = 1$ for supersonic flow, and $C_1 = 0.5$ for subsonic flow.

Integrating Equation 2 between limits $\xi = 0$ and $\xi = \ell$ as shown in Figure 1 yields the potential due to a finite line source of unit strength.

$$\phi_1 = \text{Re} \left[d_1 - d_2 \right] - x_1 (F_1 - F_2) \quad (7)$$

CR103

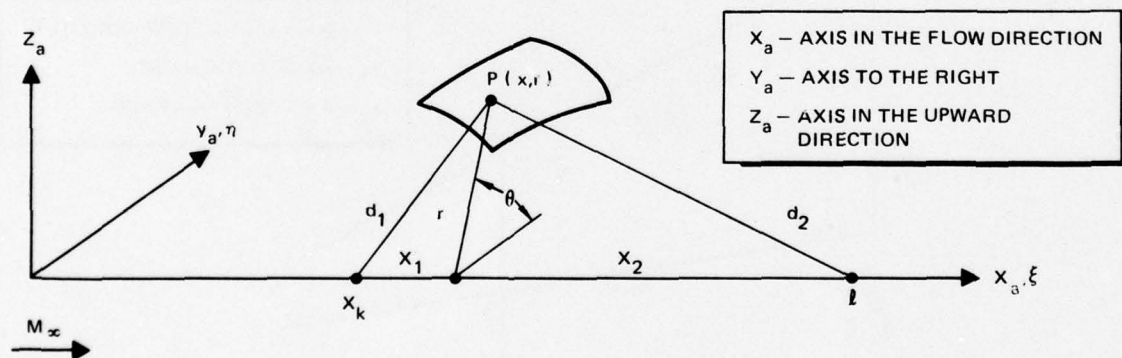


Figure 1. Line Source or Doublet Geometry

For line doublets of unit strength, the potential obtained from Equation 3 after integration is

$$\phi_2 = \frac{\sin \theta}{2r} \text{Re} \left[x_1 (d_1 - d_2) - \ell d_2 + r^2 (1-M_\infty^2) \log \frac{x_1 + d_1}{x_2 + d_2} \right] \quad (8)$$

where

$$d_1 = \left[(x-x_k)^2 + (1-M_\infty^2) r^2 \right]^{1/2}$$

$$d_2 = \left[(x-\ell)^2 + (1-M_\infty^2) r^2 \right]^{1/2}$$

$$F_1 = \text{Re} \log (x-x_k + d_1) / \left(|1-M_\infty^2| \right)^{1/2}_r$$

$$F_2 = \text{Re} \log (x-\ell + d_2) / \left(|1-M_\infty^2| \right)^{1/2}_r$$

r = radial distance

θ = angle between r and x - y plane

For source distribution over a panel, the limits of integration for Equations 4, 5 and 6 are defined by the boundaries of the panel as shown in Figure 2.

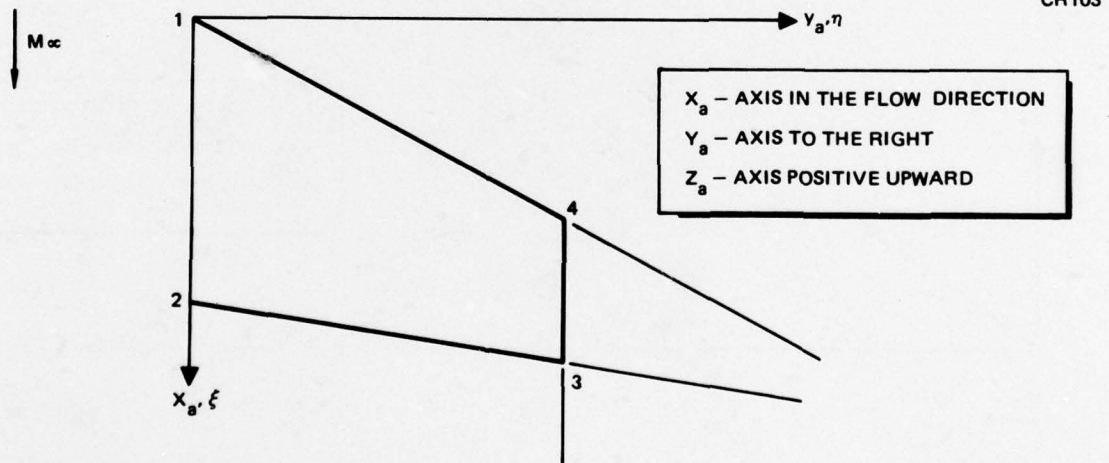


Figure 2. Source Panel Geometry

The above integrals can be considered as the sum of four integrals each representing a semi-infinite triangular region having origins at each of the corners. In other words, we have the potential for a particular panel as

$$\phi = \sum_{i=3}^5 (\phi_{i1} - \phi_{i2} - \phi_{i3} + \phi_{i4}) \quad (9)$$

where ϕ_{ik} is the component potential of the semi-infinite triangular region with the k-th corner as its origin. The limit of integration for each region can easily be found (Reference 3) and the integrals subsequently evaluated. For a constant source, a linearly varying source and constant pressure vortex distributions, the component potentials are

$$\phi_{3k} = -\frac{C_1}{\pi} \left[yF_3 + (x-Ly) F_4 - zF_5 \right] \quad (10)$$

$$\begin{aligned} \phi_{4k} = & -\frac{C_1}{2\pi} \left\{ \left[2xy + L(z^2 - y^2) \right] F_3 \right. \\ & \left. + \left[(x-Ly)^2 - L^2 + 1-M_\infty^2 \right] F_4 - 2z(x-Ly) F_5 - yd \right\} \end{aligned} \quad (11)$$

$$\phi_{5k} = C_1 \Delta u \left\{ (x-Ly)(F_5 + F_6) + z \left[L^2 + 1-M_\infty^2 \right] F_4 - L(F_3 - F_7) \right\} / 2\pi \quad (12)$$

where

$$F_3 = R_e \left\{ \log(x+d) / \left[\left| 1-M_\infty^2 \right| r \right]^{1/2} \right\}$$

$$F_4 = R_e \left\{ \log(x'+d') / \left[\left| 1-M_\infty^2 \right| r' \right]^{1/2} / \left(L^2 + 1-M_\infty^2 \right)^{1/2} \right\}$$

$$F_5 = R_e \left[\tan^{-1} zd / (Lr - xy) \right]$$

$$F_6 = \tan^{-1} (y/z) \text{ for } M_\infty < 1$$

$$= 0 \text{ for } M_\infty \geq 1$$

$$F_7 = \log (Lr/r') \text{ for } M_\infty \leq 1$$

$$= 0 \text{ for } M_\infty > 1$$

and

$$r = (y^2 + z^2)^{1/2}$$

$$d = \left[x^2 + (1 - M_\infty^2) r^2 \right]^{1/2}$$

$$x' = Lx + (1 - M_\infty^2) y$$

$$y' = x - Ly$$

$$r' = \left[(x - Ly)^2 + (L^2 + 1 - M_\infty^2) z^2 \right]^{1/2}$$

$$d' = \left\{ \left[Lx + (1 - M_\infty^2) y \right]^2 + (1 - M_\infty^2) \left[(x - Ly)^2 + (L^2 + 1 - M_\infty^2) z^2 \right] \right\}^{1/2}$$

$$\Delta u = \text{axial velocity discontinuity} = -1/2 \Delta C_p$$

$$R_e = \text{real part}$$

The velocity components are obtained from the potentials by differentiation

$$u = \frac{\partial \phi}{\partial x}$$

$$v = \frac{\partial \phi}{\partial y}$$

$$w = \frac{\partial \phi}{\partial z}$$

Applying the tangency condition to the control point of each panel, a system of linear algebraic equations is formed with the strength of singularities of each panel constituting an unknown which is to be determined. The location of the control point (i. e., the point where the pressure is computed for each panel) has been determined empirically to be 95 percent of the local panel chord through the centroid. This selection has been correlated with extensive numerical computations of pressure distributions and lift curve slopes for a

variety of wing planforms at both subsonic and supersonic speeds. By relating the strength of singularities to the velocity components, the solution of this system of equations yields a coefficient matrix of influence coefficients which are to be used for computing the surface pressure, lift, drag, and pitching moments.

The pressure coefficients on the body resulting from line sources and doublets are

$$C_{PBBi} = -2\bar{U}_{Bi} + \beta^2 \bar{U}_{Bi}^2 - \bar{V}_{Bi}^2 - \bar{W}_{Bi}^2 \quad (13)$$

where \bar{U}_{Bi} , \bar{V}_{Bi} and \bar{W}_{Bi} are velocity components on body panel i induced by the sources and doublets. The pressure coefficients on the body panel resulting from surface distributions of singularities on the body and wing are

$$C_{PBWi} = -2\hat{U}_{Bi} + \beta^2 \hat{U}_{Bi}^2 - \hat{V}_{Bi}^2 - \hat{W}_{Bi}^2 \quad (14)$$

where \hat{U}_{Bi} , \hat{V}_{Bi} and \hat{W}_{Bi} are velocity components on body panel i induced by body and wing panels. The combined pressure coefficient C_{PBi} on the body panel i in the presence of wing is the sum of these two coefficients, C_{PBBi} and C_{PBWi} .

The pressure coefficients on the wing panels are

$$C_{PWi} = -2U_{Wi} + \beta^2 U_{Wi}^2 - V_{Wi}^2 - W_{Wi}^2 \quad (15)$$

where

$$U_{Wi} = U_{WBi} + U_{WWi}, \quad V_{Wi} = V_{WBi} + V_{WWi} \text{ and}$$

$W_{Wi} = W_{WBi} + W_{WWi}$ are the velocity components due to the presence of body and wing panels.

The lift, drag, and pitching moment coefficients are obtained by summing the contribution from all panels.

$$C_L = \frac{1}{A_T} \left\{ \sum_i^{NC} \sum_j^{NB} [C_{PW}^A]_{ij} + \sum_i^{NX} \sum_j^{NT} [C_{PB}^A]_{ij} \right\} \quad (16)$$

$$C_D = \frac{1}{A_T} \left\{ \sum_i^{NC} \sum_j^{NB} \left[C_{PW} \left(\frac{dz}{dx} - \alpha \right) A \right]_{ij} + \sum_i^{NX} \sum_j^{NT} \left[C_{PB} \left(\frac{dz}{dx} - \alpha \right) A \right]_{ij} \right\} \quad (17)$$

$$C_M = \frac{1}{A_T \bar{c}} \sum_i^{NC} \sum_j^{NB} \left[C_{PW}^A \{ x_i + z_i \left(\frac{dz}{dx} - \alpha \right) \} \right]_{ij} + \frac{1}{A_T \bar{c}} \sum_i^{NX} \sum_j^{NT} \left[C_{PB}^A \{ x_i + z_i \left(\frac{dz}{dx} - \alpha \right) \} \right]_{ij} \quad (18)$$

where

- C_{PB}, C_{PW} = Pressure coefficient for body or wing panel
- A_T = Total area of wing
- NC, NB = Chordwise and spanwise number of panel segments of wing
- NX, NT = Axial and azimuthal panel segments of body
- A = Area of panel, body or wing
- dz/dx = Panel slope
- α = Angle of attack
- \bar{c} = Moment arm about reference point.

2.2 SURFACE SPLINE FIT

A versatile surface spline fit method (Reference 6) has been incorporated into the aero code for the following purposes. Firstly, from the experience gained in the operation of the code developed for the analysis of missile wings, it is clear that input preparation must be greatly simplified for any wing surface except for the plane one. The calculation of wing camber,

thickness and twist at the locations as specified in the aero code (control point of each panel) proved to be difficult and time consuming. Thus, a surface spline fit that is efficient and flexible is strongly suggested. Secondly, the pressure loads on the missile as computed by the code are originally prescribed at the control point of aero panels. To satisfy the requirement of structural analysis the pressure loads at the centroid of each finite element are needed. Interpolation of the pressure loads therefore becomes necessary.

2.2.1 Theoretical Discussion

The one-dimensional spline curve is the numerical analogue to the french curve used in curve plotting. It is based on the premise that by bending a thin flexible beam that is constrained to pass through a number of coordinates, a smooth curve is formed. Mathematically, the curve represented by the spline is the thin-beam equation whose solution is the desired spline.

Analogous to the one-dimensional spline, the surface spline is that of a thin plate subject to a bending moment while it is constrained at a number of points. The differential equation for the plate is

$$\nabla^4 \delta = P \quad (19)$$

where

δ and P represent the deflection and load, respectively.

The solution that satisfies the equilibrium conditions and vanishingly small deflection at large distance is

$$\delta(x_j, y_j) = k_1 + k_2 x_j + k_3 y_j + \sum_{i=1}^N k_{i+3} r_{ij}^2 \ln(r_{ij}^2) \quad j = 1, N \quad (20)$$

In Equation 20, $r_{ij}^2 = (x_i - x_j)^2 + (y_i - y_j)^2$ and k_1 , k_2 , and k_3 , and k_i are coefficients describing the deflection of the plate. These coefficients, which total $3 + N$, are determined using the constraints at N points, i. e., Equation 20 and the equilibrium conditions

$$\sum_{i=1}^N K_i = 0, \quad \sum_{i=1}^N K_i x_i = 0, \quad \sum_{i=1}^N K_i y_i = 0 \quad (21)$$

These yield the necessary and sufficient conditions for their evaluation.

The calculation of the deflections, δ , at any arbitrary location (x, y) is achieved by substituting the calculated values of coefficients and computing from Equation 20

$$\delta(x, y) = k_1 + k_2 x + k_3 y + \sum_{i=1}^N K_{i+3} r_i^2 \ln(r_i^2) \quad (22)$$

where

$$r_i^2 = (x - x_i)^2 + (y - y_i)^2$$

2.2.2 Application

In interpolating either the wing surface geometry or the aerodynamic load over wing surfaces, it is necessary to first calculate the $3 + N$ coefficients using the wing description data. The desired value of the interpolated quantities at any location can then be evaluated using Equation 22.

It will be appropriate to mention some advantages of this particular spline method as compared to others. Generally, spline fit methods require large storage for the coefficients. In the two-dimensional case, the storage requirement is approximately $16N$, where N is the number of data points given. For this method of surface fit only $(N + 3)$ storage locations are required. In addition, searching for the correct patch on which the desired point of interpolation is located is avoided thereby increasing computing efficiency. Further, the method is capable of accepting input data given at points randomly located. Hence, additional processing is eliminated in these cases. Especially important is the fact that some locations of the finite element centroid can and often do lie outside the domain of the control point of the panel. In general most methods fail when it is required to interpolate at such locations. The present method, however, can interpolate at these locations without special provisions.

Section 3

COMPUTER PROGRAM

The present version of the MDAC aerodynamic code is developed to provide a practical and user-oriented tool for the purpose of analyzing the pressure load on a missile or its components. Using the output of NSWC computer code PING or BING which specifies the finite element and grid point distribution on the missile, it computes the aerodynamic pressures on the missile and interpolates by surface fit to produce the desired pressure load at the centroid of each element. Punch card output in the bulk data format of NASTRAN are generated as desired for subsequent structural analysis.

In the following sections, the capabilities and restrictions of the present code will be discussed, followed by the input description for all three test cases. Outputs at the end of computation are reproduced to aid users.

3.1 CAPABILITIES OF THE MDAC AERO CODE

As presently modified, the code is capable of computing the pressure load on a missile, or if desired its component such as wing, body or tail, for both subsonic and low-supersonic flows. Restricted to small disturbances, the code analyzes a slender body of circular or near circular cross-section at zero or small angle of attack. Wings of various forms are represented as the sum of camber, thickness and twist slopes. The pressure load at the control point of each panel whether it lies on the body or on the wing are computed from the strength of the distributed sources satisfying the tangency condition at the panel surface. The pressure load at the centroid of the finite element as generated from NSWC codes is next computed by interpolation using the surface fit method successfully tested in the earlier effort. They are produced as punched card output in the bulk data format of NASTRAN.

For use on the CDC CYBER 74 computer with KRONOS 2.1 system, the code requires a field length of 160,000 using the FTN compiler. As written, it

permits the use of 700 finite elements and 350 grid points for the body and wing each. For the case where the number of finite elements or grid points exceeds the above limit, updating of the program will be necessary.

The code has certain limitations when treating a missile with complex configuration that are inherent in the original MDAC-Woodward program. One of them is the missile attitude restrictions. Although it can be removed by modification of the code, at present the code can only be used to treat the case with small angle of attack without any out of pitch-plane attitude changes (roll or yaw). The code assumes that the missile configuration is composed of one main fuselage, multiple wings and two pairs of nacelles. Consequently, a multiple body problem cannot be analyzed without code alterations. Furthermore, the cross section of the body must be approximately circular for the calculation to be valid. These restrictions, however, are not fundamental to the basic theory of small disturbances and hence can be dealt with successfully in future development.

3.2 PROGRAM INPUT DESCRIPTION

Numerous input parameters are required in the present code for correct numerical computation of a desired case. To minimize the labor of input preparation, their numbers have been kept to a minimum and appropriate default values for some parameters depending on the case analyzed have been set in the code.

The input parameters and data have been organized into two main groups in accordance with their assigned functions similar to the overall organization of the code. The first group contains all the parameters needed for the specification of case selection, missile configuration and flow conditions. They form the input parameter of the namelist UNIFID. The second group specifies the finite element and grid point system as generated by the NSWC computer codes BING and/or PING. It includes the specification for the coordinate system used for the finite elements.

For the convenience of the user, card format for inputs are described in their sequential order as required by the code.

(A) Aerodynamic Control Parameters

Card 1 Title and case description, format (20A4), alphanumeric

Card 2 \$UNIFID, begins at Column 2 with the symbol \$.

Card 3 and additional cards if necessary, contain the following parameters as input.

ICASE = 1 Wing only

= 2 Body only

= 3 Complete missile

NTRANS Number of coordinate transformations required to convert the coordinates for the finite element to the coordinates used in the aerodynamic code. Two transformations are allowed for each missile component, in the following order; body, wings and nacelles.

IPUNCH = 0 No punched card output, default value

= 1 Punched card output requested

IRW = 0 Computation results are not saved on tape, default value

= 1 Aerodynamic computation results are saved on tape 12 for restart, first run only.

= 2 Restart run, bypass all aerodynamic computations and begins computation at the start of pressure interpolation.

POLAR Number of incremental angles of attack, default value = 0

XMACH Mach number of flow, default value = 2.0

PINF Free stream pressure, default value = 14.7 psi

DADEG Incremental angle of attack of missile in degrees, default value = 0.

SID Case identification number for each missile component (up to 20 allowed), default values have been set at 1. Also used for selecting the sign convention for pressure output. Code uses the accepted rule for pressure, i. e. positive acting toward the surface and negative acting away from the surface. For opposite sign convention, set SID(L) as negative for pressure output on

the desired component L (body, wing surfaces, upper or lower).

The following input parameters are required for the case where missile body is included.

NBPFL	Number of body profile stations for specifying body geometry $r = r(x)$, up to 51 stations allowed
$XB \leq 51$	Axial coordinate of body stations in the direction of flow for specifying the body profile.
$RB \leq 51$	Radial coordinate of body profile at corresponding body stations
$ZD \leq 51$	Body camber at corresponding body stations
ARB	Angle of attack of missile body in degrees, default value = 0

The following inputs are required for the case where the missile wing is included.

ISOLID = 0	Wing of built-up construction, pressure load on both upper and lower wing surface generated, default value
= 1	Wing of solid section, sum of the pressure loads on wing surface generated
IFORM = 0	Wing of built-up construction, both upper and lower surface height (ZWI) are given at identical locations (XWI, YWI)
= 1	Wing of built-up construction, upper and lower surface height (ZWI) are not given at identical locations
= 2	Flat wing surface
NWPI	Number of coordinate points specify the wing surface contour (≤ 30). Code allows a maximum of 20 wing surfaces (upper and lower). Each wing surface must be defined in the form of equation of a surface, $ZWI = f(XWI, YWI)$. A maximum of 30 points are permitted with the provision that the first four points are restricted to the specification of the corners of the wing only. The coordinates for the corners must be given in the following order. Starting with the innermost

point of the leading edge, the remaining corners are to be given in a clockwise order viewing from the above.

NWING Number of wings or tails. A maximum of 10 is allowed, default value = 0.

XWI(i, j), Wing surface coordinates where indices i and j designate the surface coordinate point and wing surface, respectively.

YWI(i, j),
ZWI(i, j)

DIHED Dihedral angle, degrees

PIVØT Indicates dihedral, 0 for no dihedral and >0 for dihedral present

ARW Angle of attack of wing in degrees, with respect to the body axis if complete missile is considered, default value = 0

The following input parameters are required for the case where nacelle is present.

XNACEL Number of nacelles, default value = 0

NACELP Number of stations defining the nacelle profile, restricted to a maximum of 51 points each

XN ≤ 51 Axial coordinate of nacelle stations in the direction of flow for specifying the nacelle profile

RN ≤ 51 Radial coordinate of nacelle profile at corresponding nacelle stations

ZN ≤ 51 Nacelle camber given at the corresponding nacelle station

ARN Angle of attack of nacelle in degrees with respect to the body axis, default values have been set at 0.0.

Card 4 \$END Begin at column 2 the symbol \$ for ending input.

(B) Finite Element and Grid Inputs

The second group of input cards are arranged immediately following Card 4 as follows:

Cards 5 and 6 Coordinate system specifications in the format of NASTRAN bulk data deck [page 2.4-49 - 2.4-54, NASTRAN User's Manual, NAS SP-221(01), 1972]. Three position vectors, A, B and C, are used to define the coordinate system. The

first defines the origin. The second defines the Z axis and the third defines a point in the XZ plane.

For Card 5 the following format is used:

Col 1-8, Coordinate system CØRDJRbb for rectangular, CØRDJCbb for cylindrical and CØRDJSbb for spherical where J identifies the coordinate system numbers.

Col 9-16, Coordinate identification number J, integer

Col 17-24, Reference coordinate system, integer, optional

Col 25-32, 33-40, 41-48, Components of vector A (3F8.2)

Col 49-56, 57-64, 65-72, Components of vector B (3F8.2)

For Card 6: Col 1-8, blank

Col 9-16, 17-24, 25-32, Components of vector C (3F8.2)

Cards 5 and 6 are to be repeated as many times as the number of coordinate systems (NTRANS) required for specifying the finite element. They are to be arranged in the order of body, wings and nacelles if any.

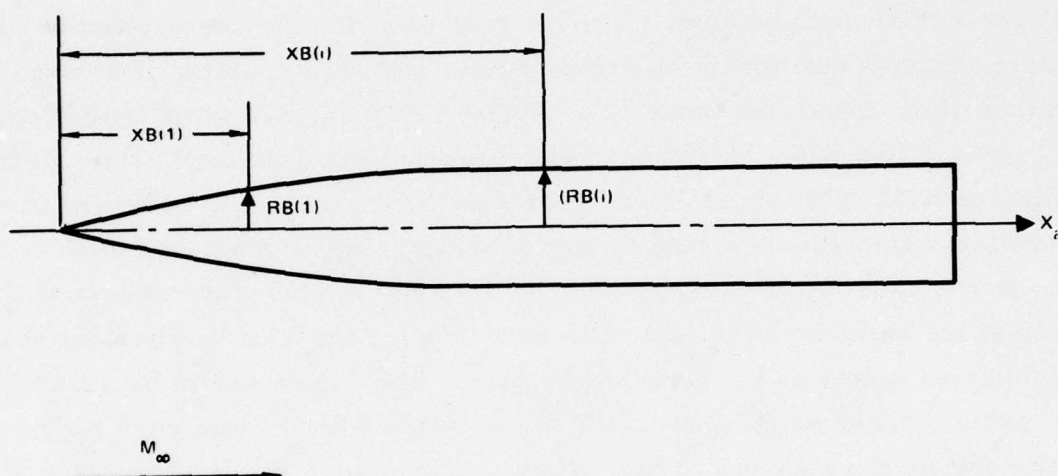
The finite element and grid specifications are arranged immediately following the coordinate system input in the same order, i. e., body, wings and nacelles.

Card 7 Specifies the number of grid cards (NGRIDP) and element cards (NE), Format (2I10).

The grid and the element cards as generated by the NSWC computer code BING are first sorted into two separate groups accordingly. They are placed immediately after card 7 with the grid cards in front.

Some remarks in regard to the input preparation need be made here to facilitate the use of the aero code.

For the body-only case, inputs of the body profiles, expressed as $r = r(x)$, for aero panel generation must be in the aero coordinate system. It is required that x be the axial distance from the tip and r the radius of the body cross section (Figure 3). For the finite element and grid point, their rela-



X_a - AXIS IN THE FLOW DIRECTION
 Y_a - AXIS TO THE RIGHT
 Z_a - AXIS POSITIVE UPWARD

Figure 3. Body Profile Input

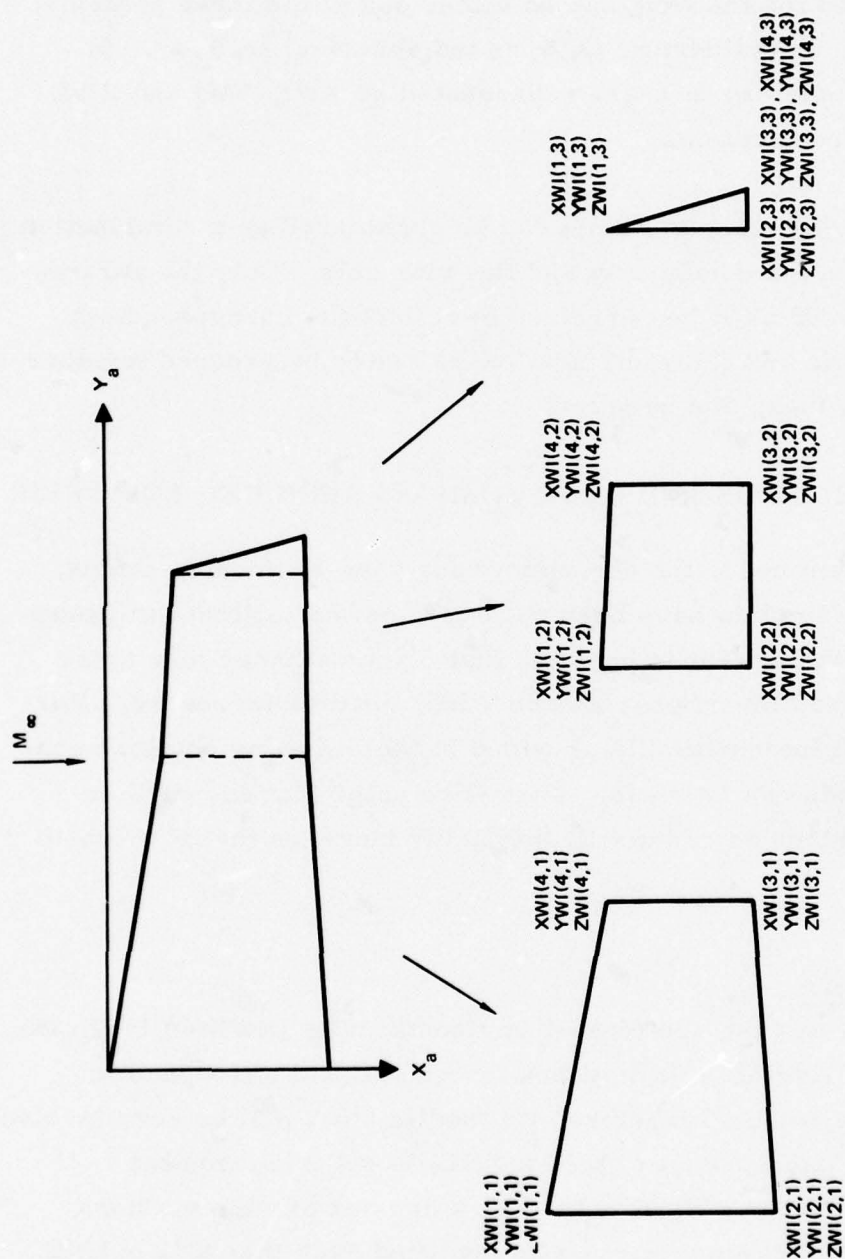
tionship to the basic coordinate system and the basic coordinate system to aero coordinate system are to be specified in the coordinate input card immediately following the namelist input. The grid card and the element card are to be separated and placed after the coordinate system specification with a card specifying their numbers placed behind the coordinate card.

For the wing only case, its input requires the specification of both the wing plan form and its surface contour. The input used for the description of wing planform are the coordinates of corner points and break points. For each individual wing, inputs for those of quadrilateral shape are their four corner coordinates. The codes as written have allocated the first four values of the coordinates XWI, YWI and ZWI for each wing or wing region, arranged in a counterclockwise order starting from the leading-edge corner or break point. In the case of triangular wings, there are only three corner points. To satisfy the same requirement, the apex or wing tip is to be considered as two coincident points of the same coordinate. The inputs are to be arranged in the same manner as that of quadrilateral shape with leading edge body-corner point as the starting point. Wings with complex shapes (see Figure 4) must be subdivided into appropriate quadrilateral or triangular regions and inputs prepared accordingly. The only requirement is the condition that the control chords, apart from either the leading edge or the trailing edge, must be in the streamwise direction.

All inputs for the wing surface are to be given in the form of equation of surface $Z = f(x, y)$ in terms of XWI, YWI and ZWI. Starting with the fifth value, XWI(5, I), YWI(5, I), ZWI(5, I), their total number may not exceed 26 points. For wings with flat surfaces, only the first four points are necessary.

Inputs defining wing thickness, camber and twist have been eliminated to reduce the input preparation effort. The code generates the required values of camber, thickness slope and twist angle for the wing using the existing surface fit scheme from the input.

The finite element and grid point coordinate system cards are placed similar to the body only case immediately behind the namelist input. They are followed by a card specifying the number of grid cards and element cards. The



NWING = 3, NTRANS (1) = 1, 1, 1,
IF BUILT-UP WING IS USED, NWPI(1), NWPI(2), AND NWPI(3) MUST BE
SPECIFIED

Figure 4. Subdivision of Complex Wing

grid point and element card as generated by PING occupies the last position in the input.

Coordinate system used for the wing can be either one of the three systems, i. e., rectilinear (x, y, z), cylindrical (r, θ, z) and spherical (r, θ, ϕ). In terms of the input parameters they are represented by XWI, YWI and ZWI, respectively for all three systems.

For the complete missile case, the input can be considered as a combination of these two cases, i. e., the body only and the wing only. Only the parameters ICASE and NTRANS need be corrected to reflect the changes. Both coordinate system cards and finite element cards are to be grouped together in the order of body, wings, and nacelles.

3.3 VARIOUS RESTRICTIONS AND CODE CHANGES REQUIRED FOR THEIR REMOVAL

In developing the present code, the dimensions for wing segments, panels, finite elements and grid points have been set based on the estimate of future requirements. Nevertheless, it is possible that circumstances may arise when one or more of the dimensions, as specified, need be increased. For convenience, pertinent information is provided in the following section necessary changes in the code can be made. It must be noted that any further increase in the dimensions as coded will inevitably increase the field length and CPU time.

3.3.1 Input Parameters

The maximum number of wing sections or horizontal tails (NWING) is limited to a total of 10. This limitation is imposed by the original aerodynamic analysis section of the code. Therefore, its modification will be very involved and costly. The wing panel number (XNB x XNC) is set in subroutine DEFAULT as 6×11 or 66 for NWING = 1. For a number of wing sections greater than one, the panel number must be modified such that $XNB \times XNC \times NWING \leq 110$. This can best be achieved by changing the value of the wing panel number through the selecting of appropriate values of XNB and XNC.

3.3.2 Finite Element and Grid Point

The maximum number of finite elements and grid points have been set at 700 and 350, respectively, for body, wing and horizontal tail. Their modification can be made by changing the dimensions of variables XC, NG, NELM in common statement PBDATA as it appears in subroutines PBODY, PSUM, WINGPR, WINGO, SAVE and PNACEL.

Correspondingly, changes are to be made also to the dimension statement of variables XI and PB in subroutine PBODY, variable XI in subroutine PWING, variables XI and PB in subroutine PNACEL.

Section 4

TEST CASES

A test case was selected for aerodynamic analysis by the present code for the purpose of validating the theoretical approach and code verification. A missile of swept wing with ogive-cylinder body as described in Reference 8 was chosen for the purposes. Its geometry and panels are shown in Figure 5 and the wing cross section is shown in Figure 6. In the noted reference experimental measurements were made for flow at Mach number 2.01 with the model placed at different angles of attack and sideslips.

4.1 INPUT ARRANGEMENTS AND OUTPUT PRINTOUT

To demonstrate the versatility of the code, computations were made for (a) body only, (b) wing only, and (c) complete missile. The corresponding input arrangements and output printouts are reproduced at the end of Section 4.

4.2 RESULTS OF COMPUTATION

Pressure loads on body as computed are shown in Figure 7. Effects of the wing obtained from the complete missile case are also plotted. It is seen that the influence of the wing on the body lies mainly in the neighborhood of the wing-body junction. Comparison with the experimental data indicates that the analysis provides a good approximation.

For the wing only case, computed loads vary from good to divergent when compared with the data as shown in Figure 8. The leading edge effect apparently needs to be considered in the future development.

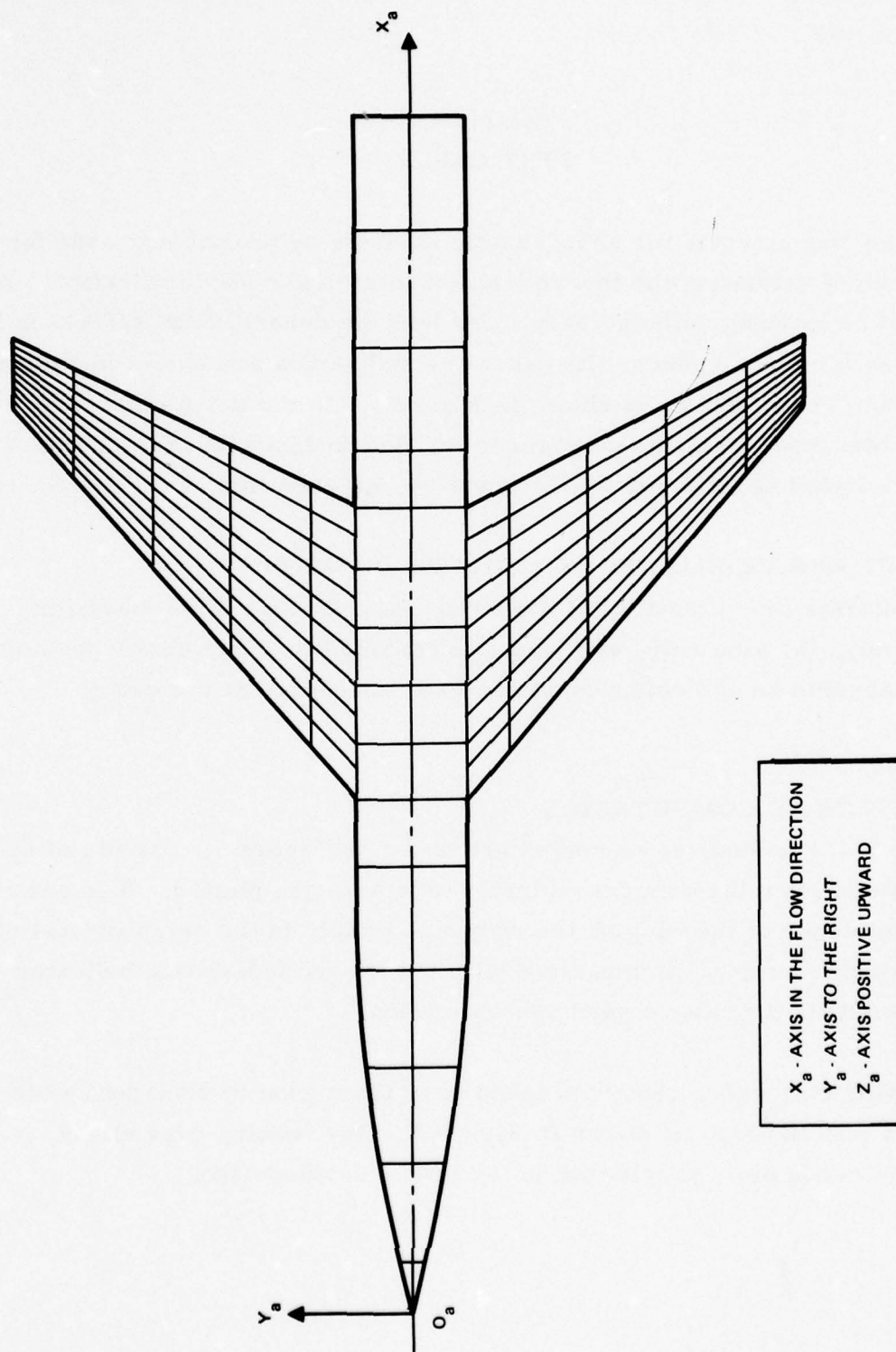


Figure 5. Test Case Wing Body Combination

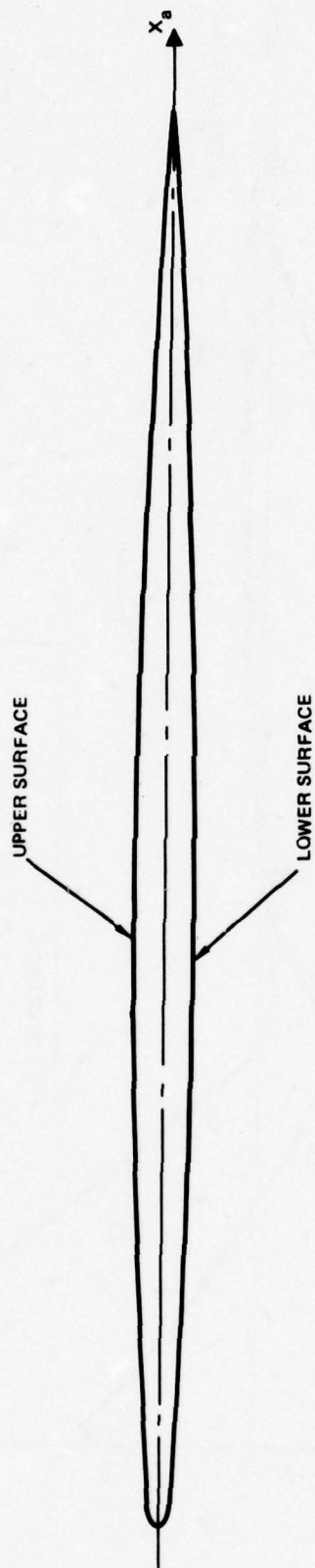


Figure 6. Wing Section - NACA 64A005

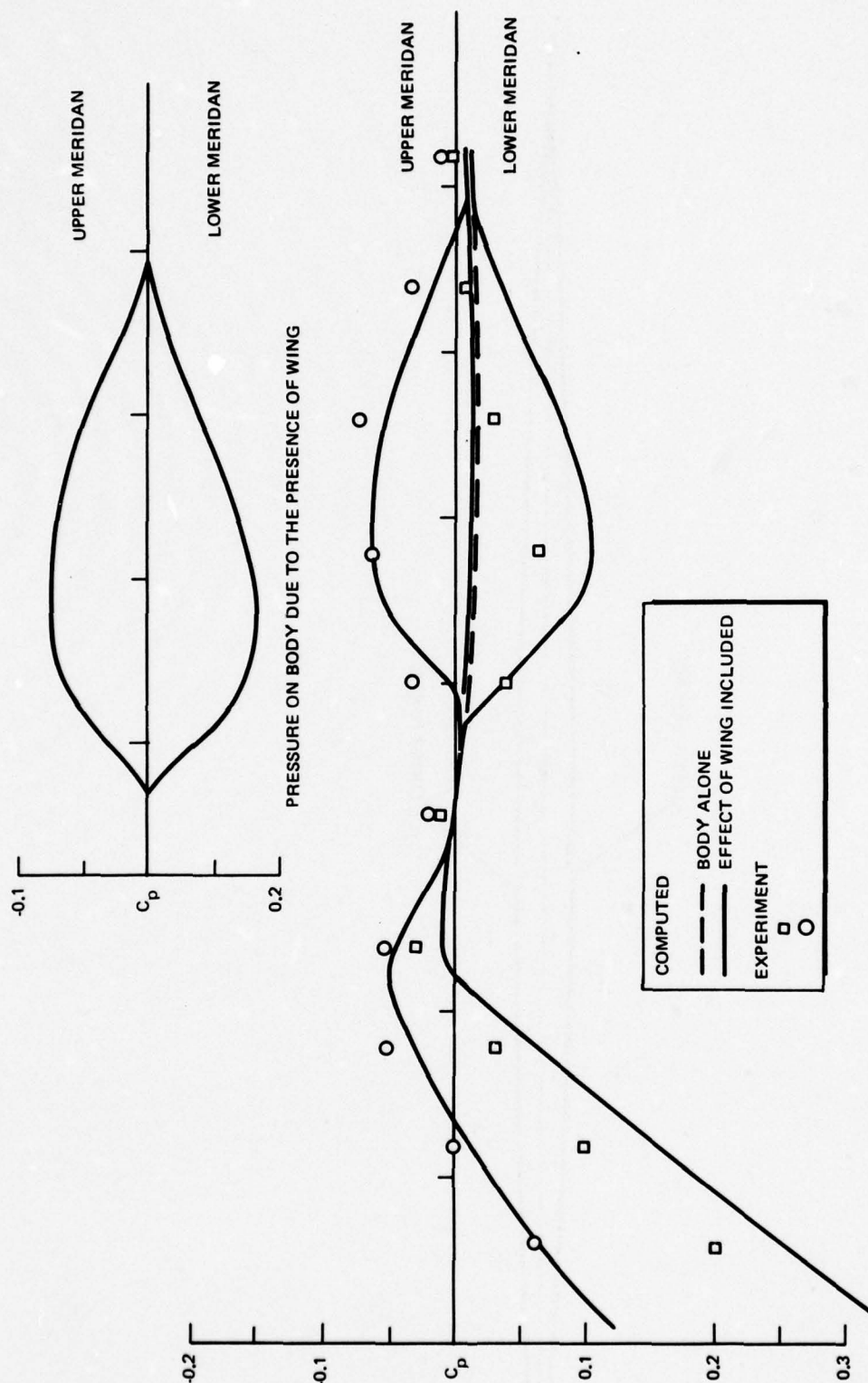


Figure 7. Pressure Distribution on Body at Mach 2.01 and 5° Angle of Attack

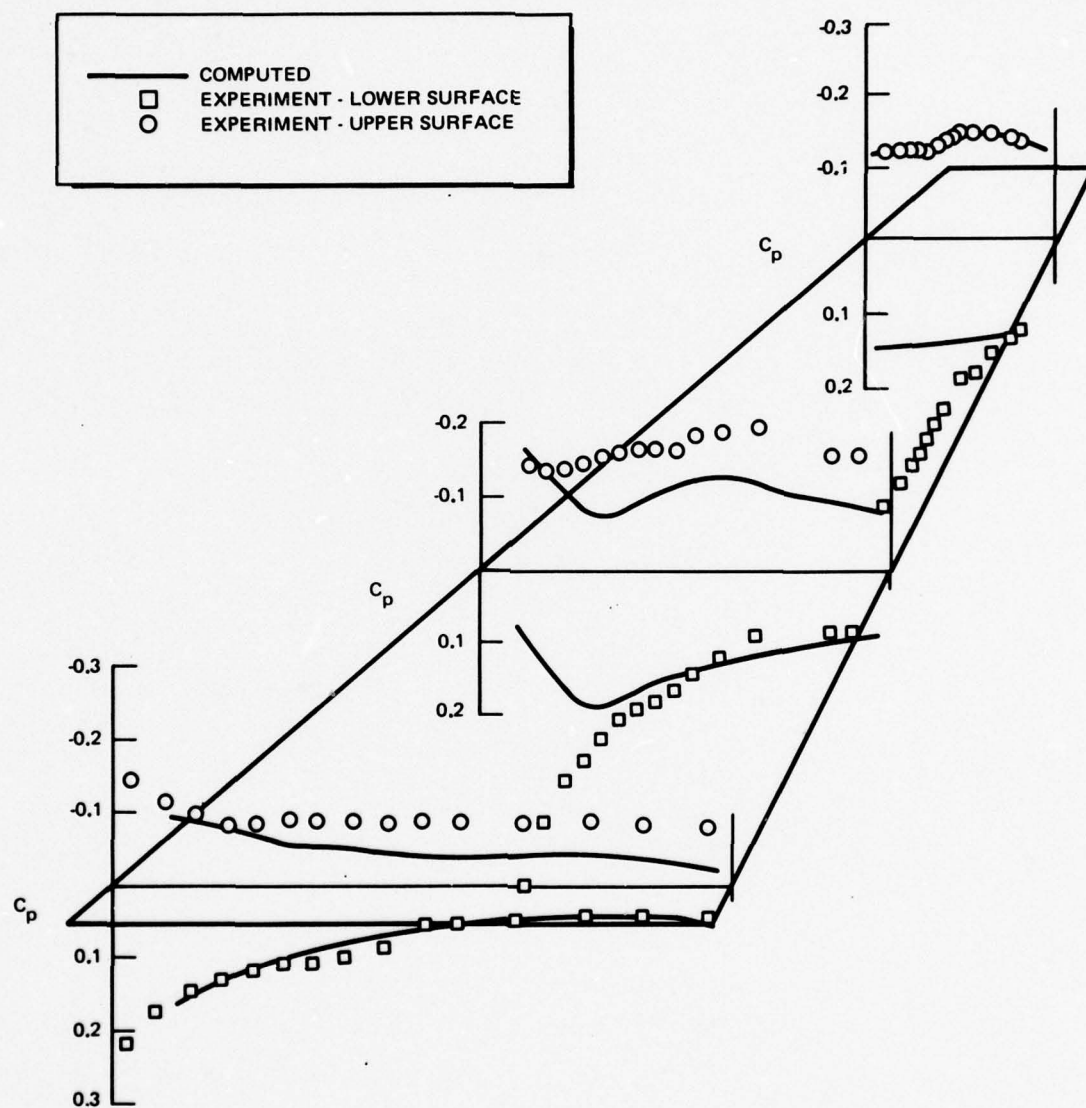


Figure 8. Pressure Distribution on Wing at Mach 2.01 and 5° Angle of Attack

4.3 INPUT CARDS FOR TEST CASES

4.3.1 Body Only Case



FINAL TEST, BODY ALONE, NSWC CARD INPUT

SUNIFID

ICASE = 2, NTRANS(1) = 1, NRPFL = 24, XWACH = 2.01, ARB = 5.0,
 XE(1) = 0.0, 0.5033, 1.1667, 1.75, 2.333, 2.916, 3.5, 4.0833, 4.6667,
 5.25, 5.8333, 6.4167, 7.0, 7.5833, 8.1667, 8.75, 9.333, 9.9167,
 10.5, 11.0833, 11.6667, 12.2, 12.75, 13.333, 13.9167, 14.5,
 15.0833, 15.6667, 16.25, 16.8333, 17.4167, 18.0, 18.5833, 19.1667,
 19.75, 20.333, 20.9167, 21.5, 22.0833, 22.6667, 23.25, 23.8333, 24.4167,
 25.0, 25.5833, 26.1667, 26.75, 27.333, 27.9167, 28.5, 29.0833, 29.6667,
 30.25, 30.8333, 31.4167, 32.0, 32.5833, 33.1667, 33.75, 34.333, 34.9167,
 35.5, 36.0833, 36.6667, 37.25, 37.8333, 38.4167, 39.0, 39.5833, 40.1667,
 40.75, 41.333, 41.9167, 42.5, 43.0833, 43.6667, 44.25, 44.8333, 45.4167,
 46.0, 46.5833, 47.1667, 47.75, 48.333, 48.9167, 49.5, 50.0833, 50.6667,
 51.25, 51.8333, 52.4167, 53.0, 53.5833, 54.1667, 54.75, 55.333, 55.9167,
 56.5, 57.0833, 57.6667, 58.25, 58.8333, 59.4167, 60.0, 60.5833, 61.1667,
 61.75, 62.333, 62.9167, 63.5, 64.0833, 64.6667, 65.25, 65.8333, 66.4167,
 67.0, 67.5833, 68.1667, 68.75, 69.333, 69.9167, 70.5, 71.0833, 71.6667,
 72.25, 72.8333, 73.4167, 74.0, 74.5833, 75.1667, 75.75, 76.333, 76.9167,
 77.5, 78.0833, 78.6667, 79.25, 79.8333, 80.4167, 81.0, 81.5833, 82.1667,
 82.75, 83.333, 83.9167, 84.5, 85.0833, 85.6667, 86.25, 86.8333, 87.4167,
 88.0, 88.5833, 89.1667, 89.75, 90.333, 90.9167, 91.5, 92.0833, 92.6667,
 93.25, 93.8333, 94.4167, 95.0, 95.5833, 96.1667, 96.75, 97.333, 97.9167,
 98.5, 99.0833, 99.6667, 100.25, 100.8333, 101.4167, 102.0, 102.5833, 103.1667,
 103.75, 104.333, 104.9167, 105.5, 106.0833, 106.6667, 107.25, 107.8333, 108.4167,
 109.0, 109.5833, 110.1667, 110.75, 111.333, 111.9167, 112.5, 113.0833, 113.6667,
 114.25, 114.8333, 115.4167, 116.0, 116.5833, 117.1667, 117.75, 118.333, 118.9167,
 119.5, 120.0833, 120.6667, 121.25, 121.8333, 122.4167, 123.0, 123.5833, 124.1667,
 124.75, 125.333, 125.9167, 126.5, 127.0833, 127.6667, 128.25, 128.8333, 129.4167,
 130.0, 130.5833, 131.1667, 131.75, 132.333, 132.9167, 133.5, 134.0833, 134.6667,
 135.25, 135.8333, 136.4167, 137.0, 137.5833, 138.1667, 138.75, 139.333, 139.9167,
 140.5, 141.0833, 141.6667, 142.25, 142.8333, 143.4167, 144.0, 144.5833, 145.1667,
 145.75, 146.333, 146.9167, 147.5, 148.0833, 148.6667, 149.25, 149.8333, 150.4167,
 151.0, 151.5833, 152.1667, 152.75, 153.333, 153.9167, 154.5, 155.0833, 155.6667,
 156.25, 156.8333, 157.4167, 158.0, 158.5833, 159.1667, 159.75, 160.333, 160.9167,
 161.5, 162.0833, 162.6667, 163.25, 163.8333, 164.4167, 165.0, 165.5833, 166.1667,
 166.75, 167.333, 167.9167, 168.5, 169.0833, 169.6667, 170.25, 170.8333, 171.4167,
 172.0, 172.5833, 173.1667, 173.75, 174.333, 174.9167, 175.5, 176.0833, 176.6667,
 177.25, 177.8333, 178.4167, 179.0, 179.5833, 180.1667, 180.75, 181.333, 181.9167,
 182.5, 183.0833, 183.6667, 184.25, 184.8333, 185.4167, 186.0, 186.5833, 187.1667,
 187.75, 188.333, 188.9167, 189.5, 190.0833, 190.6667, 191.25, 191.8333, 192.4167,
 193.0, 193.5833, 194.1667, 194.75, 195.333, 195.9167, 196.5, 197.0833, 197.6667,
 198.25, 198.8333, 199.4167, 200.0, 200.5833, 201.1667, 201.75, 202.333, 202.9167,
 203.5, 204.0833, 204.6667, 205.25, 205.8333, 206.4167, 207.0, 207.5833, 208.1667,
 208.75, 209.333, 209.9167, 210.5, 211.0833, 211.6667, 212.25, 212.8333, 213.4167,
 214.0, 214.5833, 215.1667, 215.75, 216.333, 216.9167, 217.5, 218.0833, 218.6667,
 219.25, 219.8333, 220.4167, 221.0, 221.5833, 222.1667, 222.75, 223.333, 223.9167,
 224.5, 225.0833, 225.6667, 226.25, 226.8333, 227.4167, 228.0, 228.5833, 229.1667,
 229.75, 230.333, 230.9167, 231.5, 232.0833, 232.6667, 233.25, 233.8333, 234.4167,
 235.0, 235.5833, 236.1667, 236.75, 237.333, 237.9167, 238.5, 239.0833, 239.6667,
 240.25, 240.8333, 241.4167, 242.0, 242.5833, 243.1667, 243.75, 244.333, 244.9167,
 245.5, 246.0833, 246.6667, 247.25, 247.8333, 248.4167, 249.0, 249.5833, 250.1667,
 250.75, 251.333, 251.9167, 252.5, 253.0833, 253.6667, 254.25, 254.8333, 255.4167,
 256.0, 256.5833, 257.1667, 257.75, 258.333, 258.9167, 259.5, 260.0833, 260.6667,
 261.25, 261.8333, 262.4167, 263.0, 263.5833, 264.1667, 264.75, 265.333, 265.9167,
 266.5, 267.0833, 267.6667, 268.25, 268.8333, 269.4167, 270.0, 270.5833, 271.1667,
 271.75, 272.333, 272.9167, 273.5, 274.0833, 274.6667, 275.25, 275.8333, 276.4167,
 277.0, 277.5833, 278.1667, 278.75, 279.333, 279.9167, 280.5, 281.0833, 281.6667,
 282.25, 282.8333, 283.4167, 284.0, 284.5833, 285.1667, 285.75, 286.333, 286.9167,
 287.5, 288.0833, 288.6667, 289.25, 289.8333, 290.4167, 291.0, 291.5833, 292.1667,
 292.75, 293.333, 293.9167, 294.5, 295.0833, 295.6667, 296.25, 296.8333, 297.4167,
 298.0, 298.5833, 299.1667, 299.75, 300.333, 300.9167, 301.5, 302.0833, 302.6667,
 303.25, 303.8333, 304.4167, 305.0, 305.5833, 306.1667, 306.75, 307.333, 307.9167,
 308.5, 309.0833, 309.6667, 310.25, 310.8333, 311.4167, 312.0, 312.5833, 313.1667,
 313.75, 314.333, 314.9167, 315.5, 316.0833, 316.6667, 317.25, 317.8333, 318.4167,
 319.0, 319.5833, 320.1667, 320.75, 321.333, 321.9167, 322.5, 323.0833, 323.6667,
 324.25, 324.8333, 325.4167, 326.0, 326.5833, 327.1667, 327.75, 328.333, 328.9167,
 329.5, 330.0833, 330.6667, 331.25, 331.8333, 332.4167, 333.0, 333.5833, 334.1667,
 334.75, 335.333, 335.9167, 336.5, 337.0833, 337.6667, 338.25, 338.8333, 339.4167,
 340.0, 340.5833, 341.1667, 341.75, 342.333, 342.9167, 343.5, 344.0833, 344.6667,
 345.25, 345.8333, 346.4167, 347.0, 347.5833, 348.1667, 348.75, 349.333, 349.9167,
 350.5, 351.0833, 351.6667, 352.25, 352.8333, 353.4167, 354.0, 354.5833, 355.1667,
 355.75, 356.333, 356.9167, 357.5, 358.0833, 358.6667, 359.25, 359.8333, 360.4167,
 361.0, 361.5833, 362.1667, 362.75, 363.333, 363.9167, 364.5, 365.0833, 365.6667,
 366.25, 366.8333, 367.4167, 368.0, 368.5833, 369.1667, 369.75, 370.333, 370.9167,
 371.5, 372.0833, 372.6667, 373.25, 373.8333, 374.4167, 375.0, 375.5833, 376.1667,
 376.75, 377.333, 377.9167, 378.5, 379.0833, 379.6667, 380.25, 380.8333, 381.4167,
 382.0, 382.5833, 383.1667, 383.75, 384.333, 384.9167, 385.5, 386.0833, 386.6667,
 387.25, 387.8333, 388.4167, 389.0, 389.5833, 390.1667, 390.75, 391.333, 391.9167,
 392.5, 393.0833, 393.6667, 394.25, 394.8333, 395.4167, 396.0, 396.5833, 397.1667,
 397.75, 398.333, 398.9167, 399.5, 400.0833, 400.6667, 401.25, 401.8333, 402.4167,
 403.0, 403.5833, 404.1667, 404.75, 405.333, 405.9167, 406.5, 407.0833, 407.6667,
 408.25, 408.8333, 409.4167, 410.0, 410.5833, 411.1667, 411.75, 412.333, 412.9167,
 413.5, 414.0833, 414.6667, 415.25, 415.8333, 416.4167, 417.0, 417.5833, 418.1667,
 418.75, 419.333, 419.9167, 420.5, 421.0833, 421.6667, 422.25, 422.8333, 423.4167,
 424.0, 424.5833, 425.1667, 425.75, 426.333, 426.9167, 427.5, 428.0833, 428.6667,
 429.25, 429.8333, 430.4167, 431.0, 431.5833, 432.1667, 432.75, 433.333, 433.9167,
 434.5, 435.0833, 435.6667, 436.25, 436.8333, 437.4167, 438.0, 438.5833, 439.1667,
 439.75, 440.333, 440.9167, 441.5, 442.0833, 442.6667, 443.25, 443.8333, 444.4167,
 445.0, 445.5833, 446.1667, 446.75, 447.333, 447.9167, 448.5, 449.0833, 449.6667,
 450.25, 450.8333, 451.4167, 452.0, 452.5833, 453.1667, 453.75, 454.333, 454.9167,
 455.5, 456.0833, 456.6667, 457.25, 457.8333, 458.4167, 459.0, 459.5833, 460.1667,
 460.75, 461.333, 461.9167, 462.5, 463.0833, 463.6667, 464.25, 464.8333, 465.4167,
 466.0, 466.5833, 467.1667, 467.75, 468.333, 468.9167, 469.5, 470.0833, 470.6667,
 471.25, 471.8333, 472.4167, 473.0, 473.5833, 474.1667, 474.75, 475.333, 475.9167,
 476.5, 477.0833, 477.6667, 478.25, 478.8333, 479.4167, 480.0, 480.5833, 481.1667,
 481.75, 482.333, 482.9167, 483.5, 484.0833, 484.6667, 485.25, 485.8333, 486.4167,
 487.0, 487.5833, 488.1667, 488.75, 489.333, 489.9167, 490.5, 491.0833, 491.6667,
 492.25, 492.8333, 493.4167, 494.0, 494.5833, 495.1667, 495.75, 496.333, 496.9167,
 497.5, 498.0833, 498.6667, 499.25, 499.8333, 500.4167, 501.0, 501.5833, 502.1667,
 502.75, 503.333, 503.9167, 504.5, 505.0833, 505.6667, 506.25, 506.8333, 507.4167,
 508.0, 508.5833, 509.1667, 509.75, 510.333, 510.9167, 511.5, 512.0833, 512.6667,
 513.25, 513.8333, 514.4167, 515.0, 515.5833, 516.1667, 516.75, 517.333, 517.9167,
 518.5, 519.0833, 519.6667, 520.25, 520.8333, 521.4167, 522.0, 522.5833, 523.1667,
 523.75, 524.333, 524.9167, 525.5, 526.0833, 526.6667, 527.25, 527.8333, 528.4167,
 529.0, 529.5833, 530.1667, 530.75, 531.333, 531.9167, 532.5, 533.0833, 533.6667,
 534.25, 534.8333, 535.4167, 536.0, 536.5833, 537.1667, 537.75, 538.333, 538.9167,
 539.5, 540.0833, 540.6667, 541.25, 541.8333, 542.4167, 543.0, 543.5833, 544.1667,
 544.75, 545.333, 545.9167, 546.5, 547.0833, 547.6667, 548.25, 548.8333, 549.4167,
 550.0, 550.5833, 551.1667, 551.75, 552.333, 552.9167, 553.5, 554.0833, 554.6667,
 555.25, 555.8333, 556.4167, 557.0, 557.5833, 558.1667, 558.75, 559.333, 559.9167,
 560.5, 561.0833, 561.6667, 562.25, 562.8333, 563.4167, 564.0, 564.5833, 565.1667,
 565.75, 566.333, 566.9167, 567.5, 568.0833, 568.6667, 569.25, 569.8333, 570.4167,
 571.0, 571.5833, 572.1667, 572.75, 573.333, 573.9167, 574.5, 575.0833, 575.6667,
 576.25, 576.8333, 577.4167, 578.0, 578.5833, 579.1667, 579.75, 580.333, 580.9167,
 581.5, 582.0833, 582.6667, 583.25, 583.8333, 584.4167, 585.0, 585.5833, 586.1667,
 586.75, 587.333, 587.9167, 588.5, 589.0833, 589.6667, 590.25, 590.8333, 591.4167,
 592.0, 592.5833, 593.1667, 593.75, 594.333, 594.9167, 595.5, 596.0833, 596.6667,
 597.25, 597.8333, 598.4167, 599.0, 599.5833, 600.1667, 600.75, 601.333, 601.9167,
 602.5, 603.0833, 603.6667, 604.25, 604.8333, 605.4167, 606.0, 606.5833, 607.1667,
 607.75, 608.333, 608.9167, 609.5, 610.0833, 610.6667, 611.25, 611.8333, 612.4167,
 613.0, 613.5833, 614.1667, 614.75, 615.333, 615.9167, 616.5, 617.0833, 617.6667,
 618.25, 618.8333, 619.4167, 620.0, 620.5833, 621.1667, 621.75, 622.333, 622.9167,
 623.5, 624.0833, 624.6667, 625.25, 625.8333, 626.4167, 627.0, 627.5833, 628.1667,
 628.75, 629.333, 629.9167, 630.5, 631.0833, 631.6667, 632.25, 632.8333, 633.4167,
 634.0, 634.5833, 635.1667, 635.75, 636.333, 636.9167, 637.5, 638.0833, 638.6667,
 639.25, 639.8333, 640.4167, 641.0, 641.5833, 642.1667, 642.75, 643.333, 643.9167,
 644.5, 645.0833, 645.6667, 646.25, 646.8333, 647.4167, 648.0, 648.5833, 649.1667,
 649.75, 650.333, 650.9167, 651.5, 652.0833, 652.6667, 653.25, 653.8333, 654.4167,
 655.0, 655.5833, 656.1667, 656.75, 657.333, 657.9167, 658.5, 659.0833, 659.6667,
 660.25, 660.8333, 661.4167, 662.0, 662.5833, 663.1667, 663.75, 664.333, 664.9167,
 665.5, 666.0833, 666.6667, 667.25, 667.8333, 668.4167, 669.0, 669.5833, 670.1667,
 670.75, 671.333, 671.9167, 672.5, 673.0833, 673.6667, 674.25, 674.8333, 675.4167,
 676.0, 676.5833, 677.1667, 677.75, 678.333, 678.9167, 679.5, 680.0833, 680.6667,
 681.25, 681.8333, 682.4167, 683.0, 683.5833, 684.1667, 684.75, 685.333, 685.9167,
 686.5, 687.0833, 687.6667, 688.25, 688.8333, 689.4167, 690.0, 690.5833, 691.1667,
 691.75, 692.333, 692.9167, 693.5, 694.0833, 694.6667, 695.25, 695.8333, 696.4167,
 697.0, 697.5833, 698.1667, 698.75, 699.333, 699.9167, 700.5, 701.0833, 701.6667,
 702.25, 702.8333, 703.4167, 704.0, 704.5833, 705.1667, 705.75, 706.333, 706.9167,
 707.5, 708.0833, 708.6667, 709.25, 709.8333, 710.4167, 711.0, 711.5833, 712.1667,
 712.75, 713.333, 713.9167, 714.5, 715.0833, 715.6667, 716.25, 716.8333, 717.4167,
 718.0, 718.5833, 719.1667, 719.75, 720.333, 720.9167, 721.5, 722.0833, 722.6667,
 723.25, 723.8333, 724.4167, 725.0, 725.5833, 726.1667, 726.75, 727.333, 727.9167,
 728.5, 729.0833, 729.6667, 730.25, 730.8333, 731.4167, 732.0, 732.5833, 733.1667,
 733.75, 734.333, 734.9167, 735.5, 736.0833, 736.6667, 737.25, 737.8333, 738.4167,
 739.0, 739.5833, 740.1667, 740.75, 741.333, 741.9167, 742.5, 743.0833, 743.6667,
 744.25, 744.8333, 745.4167, 746.0, 746.5833, 747.1667, 747.75, 748.333, 748.9167,
 749.5, 750.0833, 750.6667, 751.25, 751.8333, 752.4167, 753.0, 753.5833, 754.1667,
 754.75, 755.333, 755.9167, 756.5, 757.0833, 757.66

The input cards as shown, in sequence, are:

(I) Title Card

Notes: For input of any descriptive title

Format: (20A4)

(II) Namelist UNIFID input

Notes: For input of aerodynamic control parameters appropriate to the case of interest.

Format: In accordance with the input variables, real or integer.

Test Case:

ICASE = 2, body only case

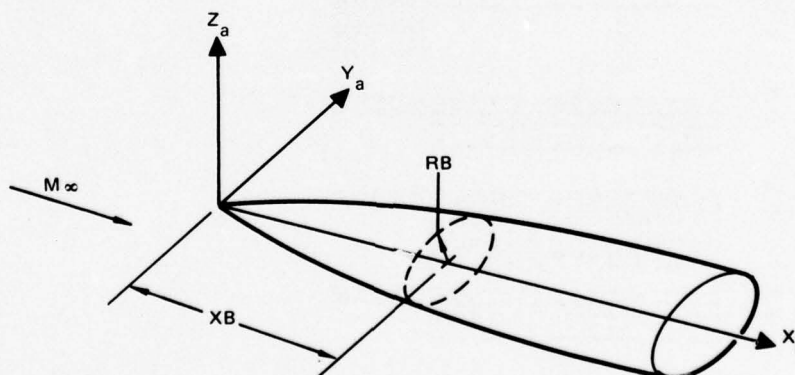
NTRANS(1) = 1, no intermediate coordinate system

XMACH = 2.01, flow Mach number

NBPFL = 24, number of point for body profile input

ARB = 5.0, angle of attack of body

For body profile inputs they are the radius RB and axial distance XB using the cylindrical coordinate system oriented as shown in the sketch. X_a , Y_a and Z_a represent the aerodynamic coordinate system.



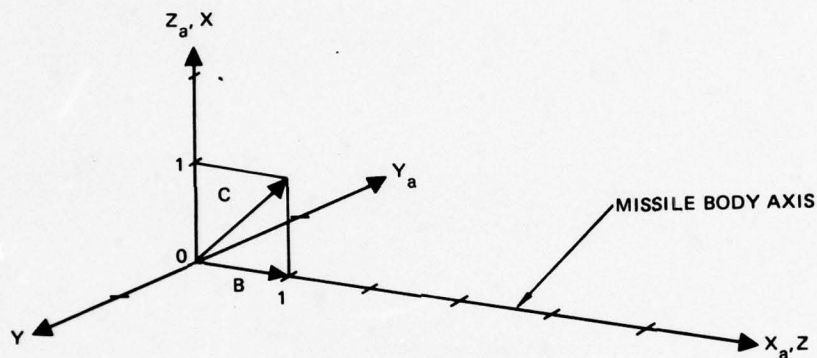
(III) Coordinate Card

Notes: The coordinate cards are needed for input of vectors A, B and C used in defining the relations between the coordinate systems of the finite element (X , Y , Z) and the aero code (X_a , Y_a , Z_a).

In accordance with NASTRAN, vector A defines the origin, sector B defines the Z axis and vector C defines the X-Z plane.
 Format: NASTRAN bulk data deck, first card (A3, 2I8, 6F8.2) and second card (A8, 3F8.2).

Test Case:

Coordinate systems for the finite element and the aero codes are shown in the sketch.



Since their origin coincides, vector A becomes a null vector or (0.0, 0.0, 0.0). With the Z axis coincident with the X_a axis, vector B has components (1.0, 0.0, 0.0). As vector B lies in the X_aZ_a plane, its components are (1.0, 0.0, 1.0).

(IV) Finite Element Cards

Notes: The finite element and grid point cards as generated by BING or PING are used for defining element coordinates. They must be divided into two separate groups with the grid point card preceding the element card. A card specifies that the numbers of grid card and element card in a format 2I10 must be placed before them.

Format: For grid and element number card (2I10), grid and finite element cards must be the same as generated by BING or PING.

Test Case: As shown.

4.3.2 Wing Only Case

34

COUAD2	516	264	274	275	265	0.0000
COUAD2	517	274	284	285	275	0.0000
COUAD2	518	284	294	295	285	0.0000
COUAD2	519	294	304	305	295	0.0000
	10					
GRID	351	1.6650	-0.0000	0.0000	2	0.0000
GRID	352	1.6650	-0.0000	0.0000	2	0.0000
GRID	353	1.6650	-0.0000	0.0000	2	0.0000
GRID	354	1.6650	-0.0000	0.0000	2	0.0000
GRID	355	1.6650	-0.0000	0.0000	2	0.0000
GRID	356	1.6650	-0.0000	0.0000	2	0.0000
GRID	357	1.6650	-0.0000	0.0000	2	0.0000
GRID	358	1.6650	-0.0000	0.0000	2	0.0000
GRID	359	1.6650	-0.0000	0.0000	2	0.0000
GRID	360	1.6650	-0.0000	0.0000	2	0.0000
GRID	361	1.6650	-0.0000	0.0000	2	0.0000
GRID	362	1.6650	-0.0000	0.0000	2	0.0000
GRID	363	1.6650	-0.0000	0.0000	2	0.0000
GRID	364	1.6650	-0.0000	0.0000	2	0.0000
GRID	365	1.6650	-0.0000	0.0000	2	0.0000
GRID	366	1.6650	-0.0000	0.0000	2	0.0000
GRID	367	1.6650	-0.0000	0.0000	2	0.0000
GRID	368	1.6650	-0.0000	0.0000	2	0.0000
GRID	369	1.6650	-0.0000	0.0000	2	0.0000
GRID	370	1.6650	-0.0000	0.0000	2	0.0000
GRID	371	1.6650	-0.0000	0.0000	2	0.0000
GRID	372	1.6650	-0.0000	0.0000	2	0.0000
GRID	373	1.6650	-0.0000	0.0000	2	0.0000
GRID	374	1.6650	-0.0000	0.0000	2	0.0000
GRID	375	1.6650	-0.0000	0.0000	2	0.0000
GRID	376	1.6650	-0.0000	0.0000	2	0.0000
GRID	377	1.6650	-0.0000	0.0000	2	0.0000
GRID	378	1.6650	-0.0000	0.0000	2	0.0000
GRID	379	1.6650	-0.0000	0.0000	2	0.0000
GRID	380	1.6650	-0.0000	0.0000	2	0.0000
GRID	381	1.6650	-0.0000	0.0000	2	0.0000
GRID	382	1.6650	-0.0000	0.0000	2	0.0000
GRID	383	1.6650	-0.0000	0.0000	2	0.0000
GRID	384	1.6650	-0.0000	0.0000	2	0.0000
GRID	385	1.6650	-0.0000	0.0000	2	0.0000
GRID	386	1.6650	-0.0000	0.0000	2	0.0000
GRID	387	1.6650	-0.0000	0.0000	2	0.0000
GRID	388	1.6650	-0.0000	0.0000	2	0.0000
GRID	389	1.6650	-0.0000	0.0000	2	0.0000
GRID	390	1.6650	-0.0000	0.0000	2	0.0000
GRID	391	1.6650	-0.0000	0.0000	2	0.0000
GRID	392	1.6650	-0.0000	0.0000	2	0.0000
GRID	393	1.6650	-0.0000	0.0000	2	0.0000
GRID	394	1.6650	-0.0000	0.0000	2	0.0000
GRID	395	1.6650	-0.0000	0.0000	2	0.0000
GRID	396	1.6650	-0.0000	0.0000	2	0.0000
GRID	397	1.6650	-0.0000	0.0000	2	0.0000
GRID	398	1.6650	-0.0000	0.0000	2	0.0000
GRID	399	1.6650	-0.0000	0.0000	2	0.0000
GRID	400	1.6650	-0.0000	0.0000	2	0.0000

The input cards as shown, in sequence, are:

(I) Title Card

Notes: For input of any descriptive title

Format: (20A4)

(II) Namelist UNIFID input

Notes: For input of aerodynamic control parameters appropriate to the case.

Format: In accordance with the input variables whether real or integer.

Test Case:

ICASE = 1, wing only case

NTRANS(1) = 1, no intermediate coordinate system

NWING = 1, one wing section

NWPI(1) = 30, (2) = 30, number of points of input defining the upper and lower surface contours given at different locations of the upper and lower surfaces.

IFORM(1) = 1, signifies the fact that the wing surfaces are of airfoil type for the present case.

XMACH = 2.01, flow Mach number

ARW = 5.0, wing angle of attack

XWI(i), YWZ(i) and ZWI(i) represent the wing surface $Z = f(x, y)$, with ZWI as the height of wing surface. They can be given in either rectangular, cylindrical or spherical coordinate systems as desired. The first four points must be used to specify the wing planform as shown in the sketch. Therefore, for the test case, we have

XWI(1, 1) = -1.665, -1.665, -11.995, -11.995

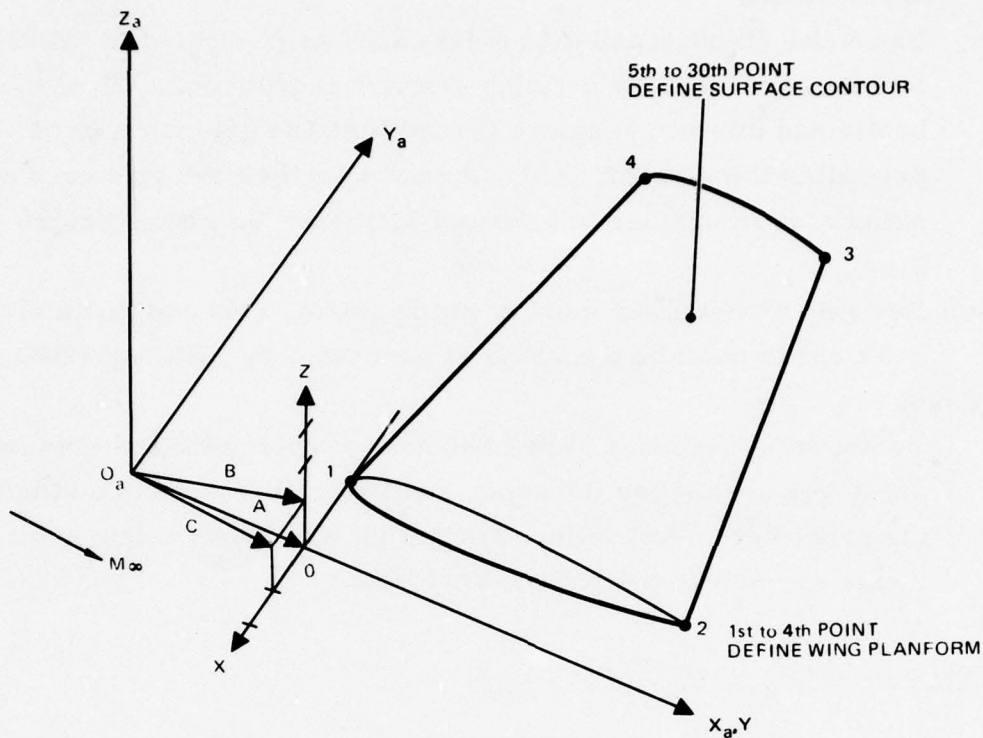
XWI(5, 1) = -1.665, -1.665, ... ,

YWI(1, 1) = 0.0, 8.89, 14.05, 12.05,

YWI(5, 1) = 2.2225, 4.445, 6.6675, ...

ZWI(5, 1) = 0.1594, 0.1731, 0.1044, ... etc.

It should be noted that all the inputs for wing surface coordinates must be that of the right wing of the missile. The coordinate system for the wing (X, Y, Z) and the aero code (X_a, Y_a, Z_a) are shown in the sketch.



(III) Coordinate Card

Notes: The coordinate cards are read for input of vectors A, B and C used in defining the relation between the coordinate systems of the finite element (X, Y, Z) and aero code (X_a , Y_a , Z_a). In accordance with NASTRAN, vector A defines the origin, vector B defines the Z axis and vector C defines the X-Z plane.

Format: NASTRAN bulk data deck, first card (A8, 2I8, 6F8.2) and second card (A8, 3F8.2).

Test Case:

As shown in the previous sketch, the vector A has components (15.59, 0.0, 0.0), vector B (15.59, 0.0, 1.0) and vector C (15.59, 1.0, 1.0). Two sets of coordinate cards are needed for the case as the upper and lower surfaces are specified separately at different locations.

(IV) Finite Element Cards

Notes: The finite element and grid point cards as generated by BING or PING are used for defining element coordinates. They must be divided into two separate groups with the grid point card preceding the element card. A card specifies the grid card and element card number in a format 2I10 must be placed before them.

Format: For grid and element number cards (2I10), grid and finite element cards must be the same as generated by BING or PING.

Test Case:

As shown in the input listing two sets of grid point and element cards are needed for the upper and lower surfaces. To simplify the presentation and reduce computing effort only a few elements are selected for pressure outputs.

4.3.3 Complete Missile Case

FINAL TEST CASE, COMPLETE MISSILE, NASA MEMO 10 - 15 - 58L

SUNIFID
 ICASE=3, NTRANS(1)= 1, NBPFL= 24, NWPI(1) = 30, NWING = 1,
 AFB = 5.0, XMACH = 2.0,
 XB(1) = 0.0, 0.5833, 1.1667, 1.75, 2.333, 2.916, 3.5, 4.0833, 4.6667,
 5.25, 5.8333, 6.4167, 7.0, 7.5833, 8.1667, 8.75, 9.333, 9.9167,
 10.5, 11.0833, 11.6667, 12.25, 12.8333, 13.4167, 14.0, 14.5833, 15.1667,
 15.75, 16.3333, 16.9167, 17.5, 18.0833, 18.6667, 19.25, 20.8333, 21.4167,
 22.0, 22.5833, 23.1667, 23.75, 24.3333, 24.9167, 25.5, 26.0833, 26.6667,
 27.25, 27.8333, 28.4167, 29.0, 29.5833, 30.1667, 30.75, 31.3333, 31.9167,
 32.5, 33.0833, 33.6667, 34.25, 34.8333, 35.4167, 36.0, 36.5833, 37.1667,
 37.75, 38.3333, 38.9167, 39.5, 40.0833, 40.6667, 41.25, 41.8333, 42.4167,
 43.0, 43.5833, 44.1667, 44.75, 45.3333, 45.9167, 46.5, 47.0833, 47.6667,
 48.25, 48.8333, 49.4167, 50.0, 50.5833, 51.1667, 51.75, 52.3333, 52.9167,
 53.5, 54.0833, 54.6667, 55.25, 55.8333, 56.4167, 57.0, 57.5833, 58.1667,
 58.75, 59.3333, 59.9167, 60.5, 61.0833, 61.6667, 62.25, 62.8333, 63.4167,
 64.0, 64.5833, 65.1667, 65.75, 66.3333, 66.9167, 67.5, 68.0833, 68.6667,
 69.25, 69.8333, 70.4167, 71.0, 71.5833, 72.1667, 72.75, 73.3333, 73.9167,
 74.5, 75.0833, 75.6667, 76.25, 76.8333, 77.4167, 78.0, 78.5833, 79.1667,
 79.75, 80.3333, 80.9167, 81.5, 82.0833, 82.6667, 83.25, 83.8333, 84.4167,
 85.0, 85.5833, 86.1667, 86.75, 87.3333, 87.9167, 88.5, 89.0833, 89.6667,
 90.25, 90.8333, 91.4167, 92.0, 92.5833, 93.1667, 93.75, 94.3333, 94.9167,
 95.5, 96.0833, 96.6667, 97.25, 97.8333, 98.4167, 99.0, 99.5833, 100.1667,
 100.75, 101.3333, 101.9167, 102.5, 103.0833, 103.6667, 104.25, 104.8333, 105.4167,
 106.0, 106.5833, 107.1667, 107.75, 108.3333, 108.9167, 109.5, 110.0833, 110.6667,
 111.25, 111.8333, 112.4167, 113.0, 113.5833, 114.1667, 114.75, 115.3333, 115.9167,
 116.5, 117.0833, 117.6667, 118.25, 118.8333, 119.4167, 120.0, 120.5833, 121.1667,
 121.75, 122.3333, 122.9167, 123.5, 124.0833, 124.6667, 125.25, 125.8333, 126.4167,
 127.0, 127.5833, 128.1667, 128.75, 129.3333, 129.9167, 130.5, 131.0833, 131.6667,
 132.25, 132.8333, 133.4167, 134.0, 134.5833, 135.1667, 135.75, 136.3333, 136.9167,
 137.5, 138.0833, 138.6667, 139.25, 139.8333, 140.4167, 141.0, 141.5833, 142.1667,
 142.75, 143.3333, 143.9167, 144.5, 145.0833, 145.6667, 146.25, 146.8333, 147.4167,
 148.0, 148.5833, 149.1667, 149.75, 150.3333, 150.9167, 151.5, 152.0833, 152.6667,
 153.25, 153.8333, 154.4167, 155.0, 155.5833, 156.1667, 156.75, 157.3333, 157.9167,
 158.5, 159.0833, 159.6667, 160.25, 160.8333, 161.4167, 162.0, 162.5833, 163.1667,
 163.75, 164.3333, 164.9167, 165.5, 166.0833, 166.6667, 167.25, 167.8333, 168.4167,
 169.0, 169.5833, 170.1667, 170.75, 171.3333, 171.9167, 172.5, 173.0833, 173.6667,
 174.25, 174.8333, 175.4167, 176.0, 176.5833, 177.1667, 177.75, 178.3333, 178.9167,
 179.5, 180.0833, 180.6667, 181.25, 181.8333, 182.4167, 183.0, 183.5833, 184.1667,
 184.75, 185.3333, 185.9167, 186.5, 187.0833, 187.6667, 188.25, 188.8333, 189.4167,
 190.0, 190.5833, 191.1667, 191.75, 192.3333, 192.9167, 193.5, 194.0833, 194.6667,
 195.25, 195.8333, 196.4167, 197.0, 197.5833, 198.1667, 198.75, 199.3333, 199.9167,
 200.5, 201.0833, 201.6667, 202.25, 202.8333, 203.4167, 204.0, 204.5833, 205.1667,
 205.75, 206.3333, 206.9167, 207.5, 208.0833, 208.6667, 209.25, 209.8333, 210.4167,
 211.0, 211.5833, 212.1667, 212.75, 213.3333, 213.9167, 214.5, 215.0833, 215.6667,
 216.25, 216.8333, 217.4167, 218.0, 218.5833, 219.1667, 219.75, 220.3333, 220.9167,
 221.5, 222.0833, 222.6667, 223.25, 223.8333, 224.4167, 225.0, 225.5833, 226.1667,
 226.75, 227.3333, 227.9167, 228.5, 229.0833, 229.6667, 230.25, 230.8333, 231.4167,
 232.0, 232.5833, 233.1667, 233.75, 234.3333, 234.9167, 235.5, 236.0833, 236.6667,
 237.25, 237.8333, 238.4167, 239.0, 239.5833, 240.1667, 240.75, 241.3333, 241.9167,
 242.5, 243.0833, 243.6667, 244.25, 244.8333, 245.4167, 246.0, 246.5833, 247.1667,
 247.75, 248.3333, 248.9167, 249.5, 250.0833, 250.6667, 251.25, 251.8333, 252.4167,
 253.0, 253.5833, 254.1667, 254.75, 255.3333, 255.9167, 256.5, 257.0833, 257.6667,
 258.25, 258.8333, 259.4167, 260.0, 260.5833, 261.1667, 261.75, 262.3333, 262.9167,
 263.5, 264.0833, 264.6667, 265.25, 265.8333, 266.4167, 267.0, 267.5833, 268.1667,
 268.75, 269.3333, 269.9167, 270.5, 271.0833, 271.6667, 272.25, 272.8333, 273.4167,
 274.0, 274.5833, 275.1667, 275.75, 276.3333, 276.9167, 277.5, 278.0833, 278.6667,
 279.25, 279.8333, 280.4167, 281.0, 281.5833, 282.1667, 282.75, 283.3333, 283.9167,
 284.5, 285.0833, 285.6667, 286.25, 286.8333, 287.4167, 288.0, 288.5833, 289.1667,
 289.75, 290.3333, 290.9167, 291.5, 292.0833, 292.6667, 293.25, 293.8333, 294.4167,
 295.0, 295.5833, 296.1667, 296.75, 297.3333, 297.9167, 298.5, 299.0833, 299.6667,
 300.25, 300.8333, 301.4167, 302.0, 302.5833, 303.1667, 303.75, 304.3333, 304.9167,
 305.5, 306.0833, 306.6667, 307.25, 307.8333, 308.4167, 309.0, 309.5833, 310.1667,
 310.75, 311.3333, 311.9167, 312.5, 313.0833, 313.6667, 314.25, 314.8333, 315.4167,
 316.0, 316.5833, 317.1667, 317.75, 318.3333, 318.9167, 319.5, 320.0833, 320.6667,
 321.25, 321.8333, 322.4167, 323.0, 323.5833, 324.1667, 324.75, 325.3333, 325.9167,
 326.5, 327.0833, 327.6667, 328.25, 328.8333, 329.4167, 330.0, 330.5833, 331.1667,
 331.75, 332.3333, 332.9167, 333.5, 334.0833, 334.6667, 335.25, 335.8333, 336.4167,
 337.0, 337.5833, 338.1667, 338.75, 339.3333, 339.9167, 340.5, 341.0833, 341.6667,
 342.25, 342.8333, 343.4167, 344.0, 344.5833, 345.1667, 345.75, 346.3333, 346.9167,
 347.5, 348.0833, 348.6667, 349.25, 349.8333, 350.4167, 351.0, 351.5833, 352.1667,
 352.75, 353.3333, 353.9167, 354.5, 355.0833, 355.6667, 356.25, 356.8333, 357.4167,
 358.0, 358.5833, 359.1667, 359.75, 360.3333, 360.9167, 361.5, 362.0833, 362.6667,
 363.25, 363.8333, 364.4167, 365.0, 365.5833, 366.1667, 366.75, 367.3333, 367.9167,
 368.5, 369.0833, 369.6667, 370.25, 370.8333, 371.4167, 372.0, 372.5833, 373.1667,
 373.75, 374.3333, 374.9167, 375.5, 376.0833, 376.6667, 377.25, 377.8333, 378.4167,
 379.0, 379.5833, 380.1667, 380.75, 381.3333, 381.9167, 382.5, 383.0833, 383.6667,
 384.25, 384.8333, 385.4167, 386.0, 386.5833, 387.1667, 387.75, 388.3333, 388.9167,
 389.5, 390.0833, 390.6667, 391.25, 391.8333, 392.4167, 393.0, 393.5833, 394.1667,
 394.75, 395.3333, 395.9167, 396.5, 397.0833, 397.6667, 398.25, 398.8333, 399.4167,
 400.0, 400.5833, 401.1667, 401.75, 402.3333, 402.9167, 403.5, 404.0833, 404.6667,
 405.25, 405.8333, 406.4167, 407.0, 407.5833, 408.1667, 408.75, 409.3333, 409.9167,
 410.5, 411.0833, 411.6667, 412.25, 412.8333, 413.4167, 414.0, 414.5833, 415.1667,
 415.75, 416.3333, 416.9167, 417.5, 418.0833, 418.6667, 419.25, 419.8333, 420.4167,
 421.0, 421.5833, 422.1667, 422.75, 423.3333, 423.9167, 424.5, 425.0833, 425.6667,
 426.25, 426.8333, 427.4167, 428.0, 428.5833, 429.1667, 429.75, 430.3333, 430.9167,
 431.5, 432.0833, 432.6667, 433.25, 433.8333, 434.4167, 435.0, 435.5833, 436.1667,
 436.75, 437.3333, 437.9167, 438.5, 439.0833, 439.6667, 440.25, 440.8333, 441.4167,
 442.0, 442.5833, 443.1667, 443.75, 444.3333, 444.9167, 445.5, 446.0833, 446.6667,
 447.25, 447.8333, 448.4167, 449.0, 449.5833, 450.1667, 450.75, 451.3333, 451.9167,
 452.5, 453.0833, 453.6667, 454.25, 454.8333, 455.4167, 456.0, 456.5833, 457.1667,
 457.75, 458.3333, 458.9167, 459.5, 460.0833, 460.6667, 461.25, 461.8333, 462.4167,
 463.0, 463.5833, 464.1667, 464.75, 465.3333, 465.9167, 466.5, 467.0833, 467.6667,
 468.25, 468.8333, 469.4167, 470.0, 470.5833, 471.1667, 471.75, 472.3333, 472.9167,
 473.5, 474.0833, 474.6667, 475.25, 475.8333, 476.4167, 477.0, 477.5833, 478.1667,
 478.75, 479.3333, 479.9167, 480.5, 481.0833, 481.6667, 482.25, 482.8333, 483.4167,
 484.0, 484.5833, 485.1667, 485.75, 486.3333, 486.9167, 487.5, 488.0833, 488.6667,
 489.25, 489.8333, 490.4167, 491.0, 491.5833, 492.1667, 492.75, 493.3333, 493.9167,
 494.5, 495.0833, 495.6667, 496.25, 496.8333, 497.4167, 498.0, 498.5833, 499.1667,
 499.75, 500.3333, 500.9167, 501.5, 502.0833, 502.6667, 503.25, 503.8333, 504.4167,
 505.0, 505.5833, 506.1667, 506.75, 507.3333, 507.9167, 508.5, 509.0833, 509.6667,
 510.25, 510.8333, 511.4167, 512.0, 512.5833, 513.1667, 513.75, 514.3333, 514.9167,
 515.5, 516.0833, 516.6667, 517.25, 517.8333, 518.4167, 519.0, 519.5833, 520.1667,
 520.75, 521.3333, 521.9167, 522.5, 523.0833, 523.6667, 524.25, 524.8333, 525.4167,
 526.0, 526.5833, 527.1667, 527.75, 528.3333, 528.9167, 529.5, 530.0833, 530.6667,
 531.25, 531.8333, 532.4167, 533.0, 533.5833, 534.1667, 534.75, 535.3333, 535.9167,
 536.5, 537.0833, 537.6667, 538.25, 538.8333, 539.4167, 540.0, 540.5833, 541.1667,
 541.75, 542.3333, 542.9167, 543.5, 544.0833, 544.6667, 545.25, 545.8333, 546.4167,
 547.0, 547.5833, 548.1667, 548.75, 549.3333, 549.9167, 550.5, 551.0833, 551.6667,
 552.25, 552.8333, 553.4167, 554.0, 554.5833, 555.1667, 555.75, 556.3333, 556.9167,
 557.5, 558.0833, 558.6667, 559.25, 559.8333, 560.4167, 561.0, 561.5833, 562.1667,
 562.75, 563.3333, 563.9167, 564.5, 565.0833, 565.6667, 566.25, 566.8333, 567.4167,
 568.0, 568.5833, 569.1667, 569.75, 570.3333, 570.9167, 571.5, 572.0833, 572.6667,
 573.25, 573.8333, 574.4167, 575.0, 575.5833, 576.1667, 576.75, 577.3333, 577.9167,
 578.5, 579.0833, 579.6667, 580.25, 580.8333, 581.4167, 582.0, 582.5833, 583.1667,
 583.75, 584.3333, 584.9167, 585.5, 586.0833, 586.6667, 587.25, 587.8333, 588.4167,
 589.0, 589.5833, 590.1667, 590.75, 591.3333, 591.9167, 592.5, 593.0833, 593.6667,
 594.25, 594.8333, 595.4167, 596.0, 596.5833, 597.1667, 597.75, 598.3333, 598.9167,
 599.5, 600.0833, 600.6667, 601.25, 601.8333, 602.4167, 603.0, 603.5833, 604.1667,
 604.75, 605.3333, 605.9167, 606.5, 607.0833, 607.6667, 608.25, 608.8333, 609.4167,
 610.0, 610.5833, 611.1667, 611.75, 612.3333, 612.9167, 613.5, 614.0833, 614.6667,
 615.25, 615.8333, 616.4167, 617.0, 617.5833, 618.1667, 618.75, 619.3333, 619.9167,
 620.5, 621.0833, 621.6667, 622.25, 622.8333, 623.4167, 624.0, 624.5833, 625.1667,
 625.75, 626.3333, 626.9167, 627.5, 628.0833, 628.6667, 629.25, 629.8333, 630.4167,
 631.0, 631.5833, 632.1667, 632.75, 633.3333, 633.9167, 634.5, 635.0833, 635.6667,
 636.25, 636.8333, 637.4167, 638.0, 638.5833, 639.1667, 639.75, 640.3333, 640.9167,
 641.5, 642.0833, 642.6667, 643.25, 643.8333, 644.4167, 645.0, 645.5833, 646.1667,
 646.75, 647.3333, 647.9167, 648.5, 649.0833, 649.6667, 650.25, 650.8333, 651.4167,
 652.0, 652.5833, 653.1667, 653.75, 654.3333, 654.9167, 655.5, 656.0833, 656.6667,
 657.25, 657.8333, 658.4167, 659.0, 659.5833, 660.1667, 660.75, 661.3333, 661.9167,
 662.5, 663.0833, 663.6667, 664.25, 664.8333, 665.4167, 666.0, 666.5833, 667.1667,
 667.75, 668.3333, 668.9167, 669.5, 670.0833, 670.6667, 671.25, 671.8333, 672.4167,
 673.0, 673.5833, 674.1667, 674.75, 675.3333, 675.9167, 676.5, 677.0833, 677.6667,
 678.25, 678.8333, 679.4167, 680.0, 680.5833, 681.1667, 681.75, 682.3333, 682.9167,
 683.5, 684.0833, 684.6667, 685.25, 685.8333, 686.4167, 687.0, 687.5833, 688.1667,
 688.75, 689.3333, 689.9167, 690.5, 691.0833, 691.6667, 692.25, 692.8333, 693.4167,
 694.0, 694.5833, 695.1667, 695.75, 696.3333, 696.9167, 697.5, 698.0833, 698.6667,
 699.25, 699.8333, 700.4167, 701.0, 701.5833, 702.1667, 702.75, 703.3333, 703.9167,
 704.5, 705.0833, 705.6667, 706.25, 706.8333, 707.4167, 708.0, 708.5833, 709.1667,
 709.75, 710.3333, 710.9167, 711.5, 712.0833, 712.6667, 713.25, 713.8333, 714.4167,
 715.0, 715.5833, 716.1667, 716.75, 717.3333, 717.9167, 718.5, 719.0833, 719.6667,
 720.25, 720.8333, 721.4167, 722.0, 722.5833, 723.1667, 723.75, 724.3333, 724.9167,
 725.5, 726.0833, 726.6667, 727.25, 727.8333, 728.4167, 729.0, 729.5833, 730.1667,
 730.75, 731.3333, 731.9167, 732.5, 733.0833, 733.6667, 734.25, 734.8333, 735.4167,
 736.0, 736.5833, 737.1667, 737.75, 738.3333, 738.9167, 739.5, 740.0833, 740.6667,
 741.25, 741.8333, 742.4167, 743.0, 743.5833, 744.1667, 744.75, 745.3333, 745.9167,
 746.5, 747.0833, 747.6667, 748.25, 748.8333, 749.4167, 750.0, 750.5833, 751.1667,
 751.75, 752.3333, 752.9167, 753.



GRID	274	251	24	GRID	312	324	GRID	312	322	332	342	352	362	372	382	392	402	412	422	432	442	452	462	472	482	492	502	512	522	532	542	552	562	572	582	592	602	612	622	632	642	652	662	672	682	692	702	712	722	732	742	752	762	772	782	792	802	812	822	832	842	852	862	872	882	892	902	912	922	932	942	952	962	972	982	992	1002	1012	1022	1032	1042	1052	1062	1072	1082	1092	1102	1112	1122	1132	1142	1152	1162	1172	1182	1192	1202	1212	1222	1232	1242	1252	1262	1272	1282	1292	1302	1312	1322	1332	1342	1352	1362	1372	1382	1392	1402	1412	1422	1432	1442	1452	1462	1472	1482	1492	1502	1512	1522	1532	1542	1552	1562	1572	1582	1592	1602	1612	1622	1632	1642	1652	1662	1672	1682	1692	1702	1712	1722	1732	1742	1752	1762	1772	1782	1792	1802	1812	1822	1832	1842	1852	1862	1872	1882	1892	1902	1912	1922	1932	1942	1952	1962	1972	1982	1992	2002	2012	2022	2032	2042	2052	2062	2072	2082	2092	2102	2112	2122	2132	2142	2152	2162	2172	2182	2192	2202	2212	2222	2232	2242	2252	2262	2272	2282	2292	2302	2312	2322	2332	2342	2352	2362	2372	2382	2392	2402	2412	2422	2432	2442	2452	2462	2472	2482	2492	2502	2512	2522	2532	2542	2552	2562	2572	2582	2592	2602	2612	2622	2632	2642	2652	2662	2672	2682	2692	2702	2712	2722	2732	2742	2752	2762	2772	2782	2792	2802	2812	2822	2832	2842	2852	2862	2872	2882	2892	2902	2912	2922	2932	2942	2952	2962	2972	2982	2992	3002	3012	3022	3032	3042	3052	3062	3072	3082	3092	3102	3112	3122	3132	3142	3152	3162	3172	3182	3192	3202	3212	3222	3232	3242	3252	3262	3272	3282	3292	3302	3312	3322	3332	3342	3352	3362	3372	3382	3392	3402	3412	3422	3432	3442	3452	3462	3472	3482	3492	3502	3512	3522	3532	3542	3552	3562	3572	3582	3592	3602	3612	3622	3632	3642	3652	3662	3672	3682	3692	3702	3712	3722	3732	3742	3752	3762	3772	3782	3792	3802	3812	3822	3832	3842	3852	3862	3872	3882	3892	3902	3912	3922	3932	3942	3952	3962	3972	3982	3992	4002	4012	4022	4032	4042	4052	4062	4072	4082	4092	4102	4112	4122	4132	4142	4152	4162	4172	4182	4192	4202	4212	4222	4232	4242	4252	4262	4272	4282	4292	4302	4312	4322	4332	4342	4352	4362	4372	4382	4392	4402	4412	4422	4432	4442	4452	4462	4472	4482	4492	4502	4512	4522	4532	4542	4552	4562	4572	4582	4592	4602	4612	4622	4632	4642	4652	4662	4672	4682	4692	4702	4712	4722	4732	4742	4752	4762	4772	4782	4792	4802	4812	4822	4832	4842	4852	4862	4872	4882	4892	4902	4912	4922	4932	4942	4952	4962	4972	4982	4992	5002	5012	5022	5032	5042	5052	5062	5072	5082	5092	5102	5112	5122	5132	5142	5152	5162	5172	5182	5192	5202	5212	5222	5232	5242	5252	5262	5272	5282	5292	5302	5312	5322	5332	5342	5352	5362	5372	5382	5392	5402	5412	5422	5432	5442	5452	5462	5472	5482	5492	5502	5512	5522	5532	5542	5552	5562	5572	5582	5592	5602	5612	5622	5632	5642	5652	5662	5672	5682	5692	5702	5712	5722	5732	5742	5752	5762	5772	5782	5792	5802	5812	5822	5832	5842	5852	5862	5872	5882	5892	5902	5912	5922	5932	5942	5952	5962	5972	5982	5992	6002	6012	6022	6032	6042	6052	6062	6072	6082	6092	6102	6112	6122	6132	6142	6152	6162	6172	6182	6192	6202	6212	6222	6232	6242	6252	6262	6272	6282	6292	6302	6312	6322	6332	6342	6352	6362	6372	6382	6392	6402	6412	6422	6432	6442	6452	6462	6472	6482	6492	6502	6512	6522	6532	6542	6552	6562	6572	6582	6592	6602	6612	6622	6632	6642	6652	6662	6672	6682	6692	6702	6712	6722	6732	6742	6752	6762	6772	6782	6792	6802	6812	6822	6832	6842	6852	6862	6872	6882	6892	6902	6912	6922	6932	6942	6952	6962	6972	6982	6992	7002	7012	7022	7032	7042	7052	7062	7072	7082	7092	7102	7112	7122	7132	7142	7152	7162	7172	7182	7192	7202	7212	7222	7232	7242	7252	7262	7272	7282	7292	7302	7312	7322	7332	7342	7352	7362	7372	7382	7392	7402	7412	7422	7432	7442	7452	7462	7472	7482	7492	7502	7512	7522	7532	7542	7552	7562	7572	7582	7592	7602	7612	7622	7632	7642	7652	7662	7672	7682	7692	7702	7712	7722	7732	7742	7752	7762	7772	7782	7792	7802	7812	7822	7832	7842	7852	7862	7872	7882	7892	7902	7912	7922	7932	7942	7952	7962	7972	7982	7992	8002	8012	8022	8032	8042	8052	8062	8072	8082	8092	8102	8112	8122	8132	8142	8152	8162	8172	8182	8192	8202	8212	8222	8232	8242	8252	8262	8272	8282	8292	8302	8312	8322	8332	8342	8352	8362	8372	8382	8392	8402	8412	8422	8432	8442	8452	8462	8472	8482	8492	8502	8512	8522	8532	8542	8552	8562	8572	8582	8592	8602	8612	8622	8632	8642	8652	8662	8672	8682	8692	8702	8712	8722	8732	8742	8752	8762	8772	8782	8792	8802	8812	8822	8832	8842	8852	8862	8872	8882	8892	8902	8912	8922	8932	8942	8952	8962	8972	8982	8992	9002	9012	9022	9032	9042	9052	9062	9072	9082	9092	9102	9112	9122	9132	9142	9152	9162	9172	9182	9192	9202	9212	9222	9232	9242	9252	9262	9272	9282	9292	9302	9312	9322	9332	9342	9352	9362	9372	9382	9392	9402	9412	9422	9432	9442	9452	9462	9472	9482	9492	9502	9512	9522	9532	9542	9552	9562	9572	9582	9592	9602	9612	9622	9632	9642	9652	9662	9672	9682	9692	9702	9712	9722	9732	9742	9752	9762	9772	9782	9792	9802	9812	9822	9832	9842	9852	9862	9872	9882	9892	9902	9912	9922	9932	9942	9952	9962	9972	9982	9992	10002	10012	10022	10032	10042	10052	10062	10072	10082	10092	10102	10112	10122	10132	10142	10152	10162	10172	10182	10192	10202	10212	10222	10232	10242	10252	10262	10272	10282	10292	10302	10312	10322	10332	10342	10352	10362	10372	10382	10392	10402	10412	10422	10432	10442	10452	10462	10472	10482	10492	10502	10512	10522	10532	10542	10552	10562	10572	10582	10592	10602	10612	10622	10632	10642	10652	10662	10672	10682	10692	10702	10712	10722	10732	10742	10752	10762	10772	10782	10792	10802	10812	10822	10832	10842	10852	10862	10872	10882	10892	10902	10912	10922	10932	10942	10952	10962	10972	10982	10992	11002	11012	11022	11032	11042	11052	11062	11072	11082	11092	11102	11112	11122	11132	11142	11152	11162	11172	11182	11192	11202	11212	11222	11232	11242	11252	11262	11272	11282	11292	11302	11312	11322	11332	11342	11352	11362	11372	11382	11392	11402	11412	11422	11432	11442	11452	11462	11472	11482	11492	11502	11512	11522	11532	11542	11552	11562	11572	11582	11592	11602	11612	11622	11632	11642	11652	11662	11672	11682	11692	11702	11712	11722	11732	11742	11752	11762	11772	11782	11792	11802	11812	11822	11832	11842	11852	11862	11872	11882	11892	11902	11912	11922	11932	11942	11952	11962	11972	11982	11992	12002	12012	12022	12032	12042	12052	12062	12072	12082	12092	12102	12112	12122	12132	12142	12152	12162	12172	12182	12192	12202	12212	12222	12232	12242	12252	12262	12272	12282	12292	12302	12312	12322	12332	12342	12352	12362	12372	12382	12392	12402	12412	12422	12432	12442	12452	12462	12472	12482	12492	12502	12512	12522	12532	12542	12552	12562	12572	12582	12592	12602	12612	12622	12632	12642	12652	12662	12672	12682	12692	12702	12712	12722	12732	12742	12752	12762	12772	12782	12792	12802	12812	12822	12832	12842	12852	12862	12872	12882	12892	12902	12912	12922	12932	12942	12952	12962	12972	12982	12992	13002	13012	13022	13032	13042	13052	13062	13072	13082	13092	13102	13112	13122	13132	13142	13152	13162	13172	13182	13192	13202	13212	13222	13232	13242	13252	13262	13272	13282	13292	13302	13312	13322	13332	13342	13352	13362	13372	13382	13392	13402	13412	13422	13432	13442	13452	13462	13472	13482	13492	13502	13
------	-----	-----	----	------	-----	-----	------	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	----

The input cards as shown, in sequence, are:

(I) Title Card

Notes: For input of any descriptive title

Format: (20A4)

(II) Namelist UNIFID input

Notes: For input of aerodynamic control parameters appropriate to the case.

Format: In accordance with the input variables whether real or integer.

Test Case:

ICASE = 3, complete missile, body and wing

NTRAN(1) = 1, (2) = 1, no intermediate coordinate system for wing and body.

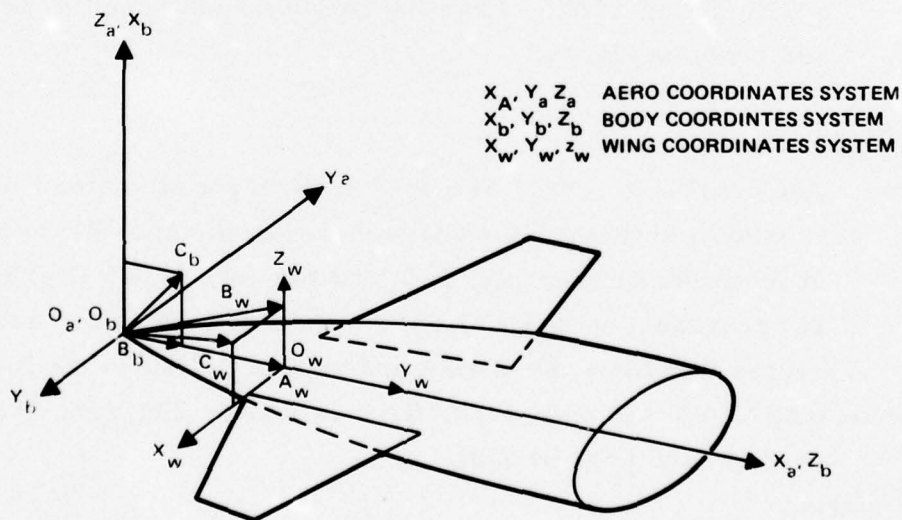
NBPFL = 24, number of points of input for body profile.

NWPI(1) = 30, number of points of input for wing surface, both upper and lower, given at same locations.

NWING = 1, one wing section.

ARB = 5.0, angle of attack of missile.

XMACH = 2.01, flow Mach number.



The above sketch shows the geometry of the complete missile with separate coordinate systems for body and wings. For body profile input, the radius RB and axial distance XB are given based on the cylindrical coordinate system oriented as shown. For wing plane form and surface contour input, XWI, YWI and ZWI representing the wing surface $Z = f(x, y)$ are specified with ZWI as the height of wing surface. They can be given in either rectangular, cylindrical or spherical coordinate systems as desired. For the test case, we have for the body profile

$$XB(1) = 0.0, 0.5233, 1.1667, \dots$$

$$RB(1) = 0.0, 0.1655, 0.3333, \dots$$

For the wing surface, the wing plans are given as

$$XWI(1, 1) = -1.665, -1.665, -11.995, -11.995,$$

$$YWI(1, 1) = 0.0, 8.89, 14.05, 12.05,$$

For the first four points. The surface coordinates are

$$XWI(5, 1) = -1.665, -1.665, -1.665, -3.731, \dots$$

$$YWI(5, 1) = 2.2225, 4.4450, 6.6675, 2.410, \dots$$

$$ZWI(5, 1) = 0.1594, 0.1731, 0.1044, 0.0, \dots$$

$$ZWI(5, 2) = -0.1594, -0.1731, -0.1044, 0.0, \dots$$

where

ZWI(i, 1) and ZWI(i, 2) are the height of wing contour for upper and lower surfaces.

(III) Coordinate Card

Notes: The coordinate cards are needed for input of vectors A, B and C used in defining the relation between the coordinate systems of the finite element (X, Y, Z) and the aero codes (X_a, Y_a, Z_a). In accordance with NASTRAN, vector A defines the origin, vector B defines the Z axis and vector C defines the X-Z plane.

Format: NASTRAN bulk data deck, first card (A8, 2I8, 6F8.2) and second card (A8, 3F8.2).

Test Case:

Two sets of coordinate cards are required, one for the body and one for the wing. The body finite element coordinate system has its origin coincident with the aero code and its Z axis coincident with the X axis of the aero code as shown in the sketch. Hence,

the vector A has component (0.0, 0.0, 0.0), vector B has component (1.0, 0.0, 0.0) and vector C has component (1.0, 0.0, 1.0).

The finite element coordinate system for the wing as shown in the sketch requires the input of vector A with component (15.59, 0.0, 0.0), vector B (15.59, 0.0, 1.0) and vector C (15.59, -1.0, 1.0).

(IV) Finite Element Cards

Notes: The finite element and grid point cards as generated by BING and PING are used for defining element coordinates. They must be divided into two separate groups with the grid point card preceding the element card. A card specifies that the numbers of grid card and element card in a form 2I10 must be placed before them.

Format: For grid and element number card (2I10), grid and finite element cards must be the same as generated by BING or PING.

Test Case:

As shown in the input listing, first set of finite element grid point and element cards are that of the body and the subsequent two sets are for the upper and lower wing surfaces.

4.4 OUTPUT PRINTOUT OF TEST CASES

4.4.1 Body Only Case

FINAL TEST, BODY ALONE, NSWC CARD INPUT

ICASE = 2,

IPUNCH = 0,

POLAR = 0.0

$$\text{STD} = \begin{matrix} 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, \\ 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, & 0.1\text{E}+01, \end{matrix}$$
[illegible]

=	0.0,	0.1655E+00,	0.3333E+00,	0.4694E+00,	0.6079E+00,	0.7376E+00,	0.8585E+00,
RB	0.10745E+01,	0.11696E+01,	0.12563E+01,	0.13346E+01,	0.14045E+01,	0.14661E+01,	0.15194E+01,
	0.15643E+01,	0.16013E+01,	0.16299E+01,	0.16503E+01,	0.16626E+01,	0.16667E+01,	0.16667E+01,
	0.16667E+01,	0.16667E+01,	0.0,	0.0,	0.0,	0.0,	0.0,
	0.0,	0.0,	0.0,	0.0,	0.0,	0.0,	0.0,
	0.0,	0.0,	0.0,	0.0,	0.0,	0.0,	0.0,





















NUMPI = 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,

IFORM = 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,

THICK = 0.1E+01,

DIMED

XVI

XMACH = 0.201E+01,
 PINF = 0.147E+02,
 DADEG = 0.0,
 ARB = 0.5E+01,
 ARW = 0.0,
 ARN = 0.0, 0.0,
 SEND
 EXIT INTAPE

DESCRIPTION OF CASE REQUESTED

SYMMETRICAL CONFIGURATION - PANELS LOCATED ON BOTH SIDES OF X-Z PLANE(SYM = 1.)

CASE = 2. CALCULATE CL, GIVEN SHAPE
 CPCALC = 0. LINEAR CP
 POLAR = 1. POLARS REQUESTED
 THICK = 0. WING THICKNESS PRESSURES NOT TO BE ADDED
 VOUT = 0. VELOCITY COMPONENTS NOT TO BE PRINTED
 MACH NUMBER = 2.0100

POINT ABOUT WHICH THE MOMENTS ARE TO BE COMPUTED

X-COORDINATE = 0.0000
 Z-COORDINATE = 0.0000

REFERENCE CHORD LENGTH = 1.0000

WING REFERENCE AREA = 1.0000

WING SEMI-SPAN = 1.0000

BODY REFERENCE AREA = 8.7469

HEIGHT OF WING PLANE ABOVE BODY AXIS = 0.0000

INCLINATION OF BODY AXIS WITH RESPECT TO DEFINING AXIS = 0.0000 DEG.

ANGLE OF ATTACK WITH RESPECT TO BODY AXIS = 5.0000 DEG.

PRESSURES, FORCES AND MOMENTS ON BODY

CD = .06332 CL = .13074 CM = -.73702

BODY PRESSURE COEFFICIENTS(CP)

THETA(DEG.)	0.0000	30.0000	60.0000	90.0000	120.0000	150.0000	180.0000
0.0000	.12638	.13607	.16616	.21578	.27524	.32501	.34454
1.7300	.11196	.12129	.15040	.19876	.25703	.30596	.32520
1.4600	.08963	.09797	.12453	.16979	.22539	.27265	.29134
2.1900	.08156	.08911	.11368	.15656	.21022	.25633	.27465
2.9200	.06710	.07400	.09689	.13771	.18955	.23448	.25241
3.6500	.05376	.05992	.08089	.11935	.16914	.21278	.23027
4.3800	.04049	.04587	.06482	.10079	.14842	.19067	.20769
5.1100	.02795	.03250	.04931	.08266	.12800	.16878	.18531
5.8400	.01576	.01944	.03401	.06459	.10749	.14671	.16272
6.5700	.00414	.00691	.01912	.04677	.08710	.12467	.14011
7.3000	-.01976	-.01824	-.00931	.01422	.05081	.08588	.10047
8.0300	-.04166	-.04303	-.04159	-.02744	.00080	.03041	.04313
8.7600	-.04718	-.05153	-.05788	-.03347	-.03395	-.01008	.00068
9.4900	-.02317	-.02981	-.04214	-.04519	-.03229	-.01275	-.00346
10.2200	-.00714	-.01505	-.03072	-.03808	-.02821	-.01244	-.00413
10.9500	.00291	-.00354	-.02270	-.03210	-.02531	-.01006	-.00231
11.6800	.00802	-.00052	-.01798	-.02795	-.02190	-.00730	.00019
12.4100	.01049	.00208	-.01512	-.02491	-.01887	-.00442	.00299
13.1400	.01146	.00324	-.01348	-.02279	-.01645	-.00189	.00553
13.8700	.01175	.00372	-.01254	-.02133	-.01462	.00011	.00759
14.6000	.01184	.00395	-.01195	-.02032	-.01330	.00161	.00913
15.3300	.01195	.00417	-.01148	-.01956	-.01230	.00274	.01030
16.0600	.01213	.00441	-.01108	-.01899	-.01159	.00354	.01112
16.7900	.01236	.00467	-.01074	-.01855	-.01107	.00410	.01170
17.5200	.01263	.00495	-.01043	-.01821	-.01071	.00447	.01207
18.2500	.01329	.00562	-.00973	-.01747	-.00993	.00526	.01287

AERODYNAMIC PRESSURE ON THE BODY - - CENTROID OF FINITE ELEMENT AS GENERATED BY NSWC CODE IN THE
SAME LOCAL COORDINATE SYSTEM

ELEMENT	X	THETA	PRESSURE	ELEMENT	X	THETA	PRESSURE
90	.844E+01	.280E+03	.480E+00	95	.908E+01	.200E+03	.322E+01
100	.844E+01	.130E+03	.305E+01	105	.909E+01	.498E+02	.157E+00
110	.104E+02	.340E+03	-.541E+00				

.....END OF COMPUTATIONS

4.4.2 Wing Only Case

FINAL TEST CASE, WING ONLY, NASA MEMO 10 - 15 - 58L



MCDONNELL DOUGLAS

53

1 AND 2 INDICATE WING PANEL LEADING-EDGE POINTS, 3 AND 4 INDICATE TRAILING-EDGE POINTS

[illegible]

WING PANEL CENTROID AND CONTROL POINT COORDINATES

PANEL	X C	Y C	Z C	X CP	Y CP	Z CP	AREA	THETA- DIED	ALPHA- CAMBER	CHORD
1	17.1727	2.66907	0.00000	17.54218	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
2	17.59430	2.66907	0.00000	18.36421	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
3	18.81633	2.66907	0.00000	19.18624	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
4	19.63836	2.66907	0.00000	20.00827	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
5	20.46039	2.66907	0.00000	20.83030	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
6	21.28242	2.66907	0.00000	21.65233	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
7	22.10445	2.66907	0.00000	22.47436	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
8	22.92648	2.66907	0.00000	23.29639	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
9	23.74851	2.66907	0.00000	24.11842	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
10	24.57053	2.66907	0.00000	24.94045	2.66907	0.00000	1.69433	0.00000	0.00000	-8.2203
11	19.50375	4.72923	0.00000	19.81483	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
12	20.19137	4.72923	0.00000	20.49945	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
13	20.87599	4.72923	0.00000	21.18407	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
14	21.56061	4.72923	0.00000	21.86868	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
15	22.24523	4.72923	0.00000	22.55330	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
16	22.92984	4.72923	0.00000	23.23792	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
17	23.61446	4.72923	0.00000	23.92254	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
18	24.29908	4.72923	0.00000	24.60716	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
19	24.98370	4.72923	0.00000	25.29178	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
20	25.66832	4.72923	0.00000	25.97640	4.72923	0.00000	1.40963	0.00000	0.00000	-6.8462
21	21.83788	6.78643	0.00000	22.08421	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
22	22.38288	6.78643	0.00000	22.63162	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
23	22.93269	6.78643	0.00000	23.17902	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
24	23.48010	6.78643	0.00000	23.72643	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
25	24.02750	6.78643	0.00000	24.27383	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
26	24.57491	6.78643	0.00000	24.82124	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
27	25.12231	6.78643	0.00000	25.36865	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
28	25.66972	6.78643	0.00000	25.91605	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
29	26.21713	6.78643	0.00000	26.46346	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
30	26.76453	6.78643	0.00000	27.01087	6.78643	0.00000	1.12494	0.00000	0.00000	-5.4741
31	24.16235	8.83767	0.00000	24.34701	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
32	24.57284	8.83767	0.00000	24.75760	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
33	24.98343	8.83767	0.00000	25.16820	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
34	25.39402	8.83767	0.00000	25.57879	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
35	25.80461	8.83767	0.00000	25.98938	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
36	26.21520	8.83767	0.00000	26.39997	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
37	26.62579	8.83767	0.00000	26.81056	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
38	27.03638	8.83767	0.00000	27.22115	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
39	27.44697	8.83767	0.00000	27.63174	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
40	27.85757	8.83767	0.00000	28.04233	8.83767	0.00000	1.12494	0.00000	0.00000	-5.4741
41	26.46947	10.87377	0.00000	26.59113	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
42	26.74426	10.87377	0.00000	26.86791	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
43	27.01904	10.87377	0.00000	27.14270	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
44	27.29383	10.87377	0.00000	27.41748	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
45	27.56861	10.87377	0.00000	27.69227	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
46	27.84340	10.87377	0.00000	27.96705	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
47	28.11818	10.87377	0.00000	28.24184	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
48	28.39297	10.87377	0.00000	28.51662	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
49	28.66775	10.87377	0.00000	28.79140	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741
50	28.94254	10.87377	0.00000	29.06619	10.87377	0.00000	1.12494	0.00000	0.00000	-5.4741

EXIT INTAPE

EXIT EVAL

EXIT EVAL

DESCRIPTION OF CASE REQUESTED

SYMMETRICAL CONFIGURATION - PANELS LOCATED ON BOTH SIDES OF X-Z PLANE (SYM = 1.)

CASE = 2. CALCULATE CL, GIVEN SHAPE

CPCALC = 0. LINEAR CP

POLAR = 1. POLARS REQUESTED

THICK = 1. WING THICKNESS PRESSURES TO BE ADDED

VOUT = 0. VELOCITY COMPONENTS NOT TO BE PRINTED

MACH NUMBER = 2.0100

POINT ABOUT WHICH THE MOMENTS ARE TO BE COMPUTED

X-COORDINATE = 0.0000

Z-COORDINATE = 0.0000

REFERENCE CHORD LENGTH = 1.0000

WING REFERENCE AREA = 56.2468

WING SEMI-SPAN = 1.0000

INCLINATION OF BODY AXIS WITH RESPECT TO DEFINING AXIS = 0.0000 DEG.

ANGLE OF ATTACK WITH RESPECT TO BODY AXIS = 0.0000 DEG.

PRESSURES, FORCES AND MOMENTS ON WING

CD = .01754 CL = .19380 CM = -4.59133

SECTION CD DISTRIBUTION

SPANWISE STATION	1	2	3	4	5
	.01050	.01691	.02166	.02333	.02350

SECTION CL DISTRIBUTION

SPANWISE STATION	1	2	3	4	5
	.11439	.17955	.23880	.26761	.26936

UPPER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.09520	-.12815	-.17064	-.14518	-.12249
2	-.07904	-.13419	-.11030	-.14825	-.12256
3	-.05805	-.13073	-.07121	-.13368	-.12905
4	-.04222	-.12393	-.10727	-.13756	-.13233
5	-.03439	-.10357	-.12046	-.11620	-.13393
6	-.03220	-.05241	-.12325	-.10530	-.13493
7	-.03326	-.00498	-.11868	-.10919	-.13808
8	-.03514	-.00839	-.10627	-.12152	-.14236
9	-.03455	-.01576	-.09297	-.12344	-.14301
10	-.01433	-.02802	-.08548	-.12382	-.13603

LOWER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	.16372	.14111	.09872	.12419	.14687
2	.11627	.13300	.15903	.12112	.14680
3	.08835	.12128	.19793	.11568	.14031
4	.06937	.09609	.16030	.13179	.13703
5	.05316	.08154	.14241	.13512	.13543
6	.04206	.10496	.12825	.16388	.13443
7	.03523	.13944	.11376	.15948	.13128
8	.03126	.10728	.10433	.14578	.12700
9	.03263	.08573	.09522	.14115	.12634
10	.05348	.06691	.08151	.13575	.13331

WING PANEL PRESSURE DIFFERENCE(CL)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	.25893	.26926	.26936	.26936	.26936
2	.19531	.26720	.26935	.26936	.26936
3	.14640	.25201	.26914	.26936	.26936
4	.11159	.22002	.26758	.26936	.26936
5	.08755	.18711	.26287	.26933	.26936
6	.07426	.15737	.25149	.26918	.26936
7	.06849	.13245	.23244	.26867	.26936
8	.06640	.11367	.21060	.26730	.26936
9	.06718	.10149	.18819	.26459	.26933
10	.06781	.09493	.16699	.25957	.26933

UPPER SURFACE WING PANEL SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.06507	-.08307	-.11057	-.09407	-.07937
2	-.06492	-.09497	-.08042	-.09327	-.07942
3	-.06487	-.10477	-.05247	-.09252	-.07957
4	-.06487	-.11022	-.05787	-.09182	-.07982
5	-.06497	-.11137	-.06387	-.09112	-.08012
6	-.06517	-.08062	-.06882	-.09042	-.08047
7	-.06537	-.05182	-.07357	-.08977	-.08092
8	-.06567	-.05552	-.08097	-.08837	-.08147
9	-.06607	-.06117	-.09112	-.08727	-.08207
10	-.05832	-.06887	-.10052	-.08727	-.08267

LOWER SURFACE WING PANEL SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.10947	-.09147	-.06397	-.08047	-.09517
2	-.10962	-.07957	-.09412	-.08127	-.09312
3	-.10967	-.06977	-.12207	-.08202	-.09497
4	-.10967	-.06432	-.11667	-.08272	-.09472
5	-.10957	-.06317	-.11067	-.08342	-.09442
6	-.10937	-.09392	-.10572	-.08412	-.09407
7	-.10917	-.12272	-.10097	-.08477	-.09362
8	-.10887	-.11902	-.09357	-.08617	-.09307
9	-.10847	-.11337	-.08342	-.08727	-.09247
10	-.11622	-.10567	-.07402	-.08727	-.09187

WING CAMBER SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.08727	-.08727	-.08727	-.08727	-.08727
2	-.08727	-.08727	-.08727	-.08727	-.08727
3	-.08727	-.08727	-.08727	-.08727	-.08727
4	-.08727	-.08727	-.08727	-.08727	-.08727
5	-.08727	-.08727	-.08727	-.08727	-.08727
6	-.08727	-.08727	-.08727	-.08727	-.08727
7	-.08727	-.08727	-.08727	-.08727	-.08727
8	-.08727	-.08727	-.08727	-.08727	-.08727
9	-.08727	-.08727	-.08727	-.08727	-.08727
10	-.08727	-.08727	-.08727	-.08727	-.08727

WING CHORD LENGTHS(C)

8.22030	6.84619	5.47406	4.10591	2.74785
---------	---------	---------	---------	---------

PRESSURE AT CONTROL POINT - UPPER SURFACE X Y PRESSURE

17.5422	2.6691	-.3958E+01
18.3642	2.6691	-.3286E+01
19.1862	2.6691	-.2413E+01
20.0083	2.6691	-.1755E+01
20.8303	2.6691	-.1430E+01
21.6523	2.6691	-.1339E+01
22.4744	2.6691	-.1383E+01
23.2964	2.6691	-.1461E+01

24.1184	2.6691	-1436E+01
24.9404	2.6691	-5957E+00
19.8148	4.7292	-5327E+01
20.4994	4.7292	-5579E+01
21.1841	4.7292	-5435E+01
21.8687	4.7292	-5152E+01
22.5253	4.7292	-4589E+01
23.2379	4.7292	-2179E+01
23.9225	4.7292	-2902E+00
24.6072	4.7292	-2657E+00
25.2918	4.7292	-6554E+00
25.9764	4.7292	-1165E+01
22.0342	6.7864	-7094E+01
22.6316	6.7864	-4585E+01
23.1790	6.7864	-2960E+01
23.7564	6.7864	-4460E+01
24.2738	6.7864	-5124E+01
24.8212	6.7864	-5124E+01
25.3686	6.7864	-4934E+01
25.9161	6.7864	-4413E+01
26.4635	6.7864	-3865E+01
27.0109	6.7864	-3553E+01
24.3470	8.8377	-6035E+01
24.7576	8.8377	-6163E+01
25.1682	8.8377	-6399E+01
25.5788	8.8377	-5719E+01
25.9894	8.8377	-4831E+01
26.4000	8.8377	-4377E+01
26.8106	8.8377	-4539E+01
27.2211	8.8377	-5052E+01
27.6317	8.8377	-5132E+01
28.0423	8.8377	-5147E+01
28.5931	10.8738	-5092E+01
26.8679	10.8738	-5095E+01
27.1427	10.8738	-5365E+01
27.4175	10.8738	-5501E+01
27.6923	10.8738	-5568E+01
27.9671	10.8738	-5610E+01
28.2418	10.8738	-5741E+01
28.5166	10.8738	-5918E+01
28.7914	10.8738	-5945E+01
29.0662	10.8738	-5655E+01

PRESSURE AT CONTROL POINT - LOWER SURFACE
X Y PRESSURE

17.5422	2.6691	-6806E+01
18.3662	2.6691	-4834E+01
19.1862	2.6691	-3673E+01
20.0083	2.6691	-2884E+01
20.8303	2.6691	-210E+01
21.6523	2.6691	-1749E+01
22.4744	2.6691	-165E+01
23.2964	2.6691	-1300E+01
24.1184	2.6691	-1356E+01
24.9404	2.6691	-223E+01
19.8148	4.7292	-586E+01
20.4994	4.7292	-529E+01
21.1841	4.7292	-5042E+01
21.8687	4.7292	-3995E+01
22.5533	4.7292	-3390E+01
23.2379	4.7292	-4364E+01
23.9225	4.7292	-5797E+01



24.6072	4.7292	.4460E+01
25.2918	4.7292	.3564E+01
25.9764	4.7292	.2782E+01
22.0842	6.7864	.4104E+01
22.6316	6.7864	.6612E+01
23.1790	6.7864	.8228E+01
23.7264	6.7864	.6664E+01
24.2738	6.7864	.5921E+01
24.8212	6.7864	.5332E+01
25.3686	6.7864	.4729E+01
25.9161	6.7864	.4337E+01
26.4635	6.7864	.3958E+01
27.0109	6.7864	.3589E+01
24.3470	8.8377	.5163E+01
24.7576	8.8377	.5035E+01
25.1682	8.8377	.4809E+01
25.5788	8.8377	.5479E+01
25.9894	8.8377	.6366E+01
26.4000	8.8377	.6813E+01
26.8106	8.8377	.6630E+01
27.2211	8.8377	.6061E+01
27.6317	8.8377	.5868E+01
28.0423	8.8377	.5643E+01
26.5931	10.8738	.6106E+01
26.8679	10.8738	.6103E+01
27.1427	10.8738	.5833E+01
27.4175	10.8738	.5697E+01
27.6923	10.8738	.5630E+01
27.9671	10.8738	.5589E+01
28.2418	10.8738	.5457E+01
28.5166	10.8738	.5280E+01
28.7914	10.8738	.5252E+01
29.0662	10.8738	.5542E+01

AERODYNAMIC PRESSURE ON THE WING - - CENTROID OF FINITE ELEMENT AS GENERATED BY NSWC CODE

TOTAL NUMBER OF WINGS 1

WING NO. 1

PRESSURE LOAD ON THE UPPER SURFACE OF WING

ELEMENT	X	Y	PRESSURE	ELEMENT	X	Y	PRESSURE
500	.178E+02	-.267E+01	.377E+01	501	.200E+02	-.473E+01	.539E+01
502	.222E+02	-.679E+01	.640E+01	503	.245E+02	-.884E+01	.606E+01
504	.267E+02	-.109E+02	.508E+01	515	.240E+02	-.267E+01	.149E+01
516	.522E+02	-.473E+01	.586E+00	517	.264E+02	-.679E+01	.396E+01
518	.275E+02	-.884E+01	.513E+01	519	.287E+02	-.109E+02	.596E+01

PRESSURE LOAD ON THE LOWER SURFACE OF WING

ELEMENT	X	Y	PRESSURE	ELEMENT	X	Y	PRESSURE
525	.178E+02	-.267E+01	-.625E+01	526	.200E+02	-.473E+01	-.577E+01
527	.222E+02	-.679E+01	-.476E+01	528	.245E+02	-.884E+01	-.513E+01
529	.267E+02	-.109E+02	-.612E+01	540	.240E+02	-.267E+01	-.129E+01
541	.522E+02	-.473E+01	-.372E+01	542	.264E+02	-.679E+01	-.405E+01
543	.275E+02	-.884E+01	-.590E+01	544	.287E+02	-.109E+02	-.523E+01

.....END OF COMPUTATIONS

4.4.3 Complete Missile Case

FINAL TEST CASE, COMPLETE MISSILE, NASA MEMO 10 - 15 - 58L

SUNIFID

ICASE = 3,
 NTRANS = 1, 1, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,
 IPUNCH = 0,
 IRW = 0,
 POLAR = 0.0,
 ISOLID = 0,
 SID = 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01, 0.1E+01,
 NBPFL = 24,
 XB = 0.0, 0.5833E+00, 0.11667E+01, 0.175E+01, 0.2333E+01, 0.2916E+01, 0.35E+01, 0.40833E+01, 0.46667E+01, 0.525E+01, 0.5833E+01, 0.64167E+01, 0.7E+01, 0.75833E+01, 0.81667E+01, 0.875E+01, 0.9333E+01, 0.99167E+01, 0.105E+02, 0.110533E+02, 0.116667E+02, 0.1225E+02, 0.12833E+02, 0.134167E+02, 0.14E+02, 0.145833E+02, 0.151667E+02, 0.1575E+02, 0.16333E+02, 0.169167E+02, 0.175E+02, 0.180833E+02, 0.186667E+02, 0.1925E+02, 0.19833E+02, 0.204167E+02, 0.21E+02, 0.215833E+02, 0.221667E+02, 0.2275E+02, 0.23333E+02, 0.239167E+02, 0.245E+02, 0.250833E+02, 0.256667E+02, 0.2625E+02, 0.26833E+02, 0.274167E+02, 0.28E+02, 0.285833E+02, 0.291667E+02, 0.2975E+02, 0.30333E+02, 0.309167E+02, 0.315E+02, 0.320833E+02, 0.326667E+02, 0.3325E+02, 0.33833E+02, 0.344167E+02, 0.35E+02, 0.355833E+02, 0.361667E+02, 0.3675E+02, 0.37333E+02, 0.379167E+02, 0.385E+02, 0.390833E+02, 0.396667E+02, 0.4025E+02, 0.40833E+02, 0.414167E+02, 0.42E+02, 0.425833E+02, 0.431667E+02, 0.4375E+02, 0.44333E+02, 0.449167E+02, 0.455E+02, 0.460833E+02, 0.466667E+02, 0.4725E+02, 0.47833E+02, 0.484167E+02, 0.49E+02, 0.495833E+02, 0.501667E+02, 0.5075E+02, 0.51333E+02, 0.519167E+02, 0.525E+02, 0.530833E+02, 0.536667E+02, 0.5425E+02, 0.54833E+02, 0.554167E+02, 0.56E+02, 0.565833E+02, 0.571667E+02, 0.5775E+02, 0.58333E+02, 0.589167E+02, 0.595E+02, 0.600833E+02, 0.606667E+02, 0.6125E+02, 0.61833E+02, 0.624167E+02, 0.63E+02, 0.635833E+02, 0.641667E+02, 0.6475E+02, 0.65333E+02, 0.659167E+02, 0.665E+02, 0.670833E+02, 0.676667E+02, 0.6825E+02, 0.68833E+02, 0.694167E+02, 0.7E+02, 0.705833E+02, 0.711667E+02, 0.7175E+02, 0.72333E+02, 0.729167E+02, 0.735E+02, 0.740833E+02, 0.746667E+02, 0.7525E+02, 0.75833E+02, 0.764167E+02, 0.77E+02, 0.775833E+02, 0.781667E+02, 0.7875E+02, 0.79333E+02, 0.799167E+02, 0.805E+02, 0.810833E+02, 0.816667E+02, 0.8225E+02, 0.82833E+02, 0.834167E+02, 0.84E+02, 0.845833E+02, 0.851667E+02, 0.8575E+02, 0.86333E+02, 0.869167E+02, 0.875E+02, 0.880833E+02, 0.886667E+02, 0.8925E+02, 0.89833E+02, 0.904167E+02, 0.91E+02, 0.915833E+02, 0.921667E+02, 0.9275E+02, 0.93333E+02, 0.939167E+02, 0.945E+02, 0.950833E+02, 0.956667E+02, 0.9625E+02, 0.96833E+02, 0.974167E+02, 0.98E+02, 0.985833E+02, 0.991667E+02, 0.9975E+02, 1.00333E+02, 1.009167E+02, 1.015E+02, 1.020833E+02, 1.026667E+02, 1.0325E+02, 1.03833E+02, 1.044167E+02, 1.05E+02, 1.055833E+02, 1.061667E+02, 1.0675E+02, 1.07333E+02, 1.079167E+02, 1.085E+02, 1.090833E+02, 1.096667E+02, 1.1025E+02, 1.10833E+02, 1.114167E+02, 1.12E+02, 1.125833E+02, 1.131667E+02, 1.1375E+02, 1.14333E+02, 1.149167E+02, 1.155E+02, 1.160833E+02, 1.166667E+02, 1.1725E+02, 1.17833E+02, 1.184167E+02, 1.19E+02, 1.195833E+02, 1.201667E+02, 1.2075E+02, 1.21333E+02, 1.219167E+02, 1.225E+02, 1.230833E+02, 1.236667E+02, 1.2425E+02, 1.24833E+02, 1.254167E+02, 1.26E+02, 1.265833E+02, 1.271667E+02, 1.2775E+02, 1.28333E+02, 1.289167E+02, 1.295E+02, 1.300833E+02, 1.306667E+02, 1.3125E+02, 1.31833E+02, 1.324167E+02, 1.33E+02, 1.335833E+02, 1.341667E+02, 1.3475E+02, 1.35333E+02, 1.359167E+02, 1.365E+02, 1.370833E+02, 1.376667E+02, 1.3825E+02, 1.38833E+02, 1.394167E+02, 1.4E+02, 1.405833E+02, 1.411667E+02, 1.4175E+02, 1.42333E+02, 1.429167E+02, 1.435E+02, 1.440833E+02, 1.446667E+02, 1.4525E+02, 1.45833E+02, 1.464167E+02, 1.47E+02, 1.475833E+02, 1.481667E+02, 1.4875E+02, 1.49333E+02, 1.499167E+02, 1.505E+02, 1.510833E+02, 1.516667E+02, 1.5225E+02, 1.52833E+02, 1.534167E+02, 1.54E+02, 1.545833E+02, 1.551667E+02, 1.5575E+02, 1.56333E+02, 1.569167E+02, 1.575E+02, 1.580833E+02, 1.586667E+02, 1.5925E+02, 1.59833E+02, 1.604167E+02, 1.61E+02, 1.615833E+02, 1.621667E+02, 1.6275E+02, 1.63333E+02, 1.639167E+02, 1.645E+02, 1.650833E+02, 1.656667E+02, 1.6625E+02, 1.66833E+02, 1.674167E+02, 1.68E+02, 1.685833E+02, 1.691667E+02, 1.6975E+02, 1.70333E+02, 1.709167E+02, 1.715E+02, 1.720833E+02, 1.726667E+02, 1.7325E+02, 1.73833E+02, 1.744167E+02, 1.75E+02, 1.755833E+02, 1.761667E+02, 1.7675E+02, 1.77333E+02, 1.779167E+02, 1.785E+02, 1.790833E+02, 1.796667E+02, 1.8025E+02, 1.80833E+02, 1.814167E+02, 1.82E+02, 1.825833E+02, 1.831667E+02, 1.8375E+02, 1.84333E+02, 1.849167E+02, 1.855E+02, 1.860833E+02, 1.866667E+02, 1.8725E+02, 1.87833E+02, 1.884167E+02, 1.89E+02, 1.895833E+02, 1.901667E+02, 1.9075E+02, 1.91333E+02, 1.919167E+02, 1.925E+02, 1.930833E+02, 1.936667E+02, 1.9425E+02, 1.94833E+02, 1.954167E+02, 1.96E+02, 1.965833E+02, 1.971667E+02, 1.9775E+02, 1.98333E+02, 1.989167E+02, 1.995E+02, 2.000833E+02, 2.006667E+02, 2.0125E+02, 2.01833E+02, 2.024167E+02, 2.03E+02, 2.035833E+02, 2.041667E+02, 2.0475E+02, 2.05333E+02, 2.059167E+02, 2.065E+02, 2.070833E+02, 2.076667E+02, 2.0825E+02, 2.08833E+02, 2.094167E+02, 2.1E+02, 2.105833E+02, 2.111667E+02, 2.1175E+02, 2.12333E+02, 2.129167E+02, 2.135E+02, 2.140833E+02, 2.146667E+02, 2.1525E+02, 2.15833E+02, 2.164167E+02, 2.17E+02, 2.175833E+02, 2.181667E+02, 2.1875E+02, 2.19333E+02, 2.199167E+02, 2.205E+02, 2.210833E+02, 2.216667E+02, 2.2225E+02, 2.22833E+02, 2.234167E+02, 2.24E+02, 2.245833E+02, 2.251667E+02, 2.2575E+02, 2.26333E+02, 2.269167E+02, 2.275E+02, 2.280833E+02, 2.286667E+02, 2.2925E+02, 2.29833E+02, 2.304167E+02, 2.31E+02, 2.315833E+02, 2.321667E+02, 2.3275E+02, 2.33333E+02, 2.339167E+02, 2.345E+02, 2.350833E+02, 2.356667E+02, 2.3625E+02, 2.36833E+02, 2.374167E+02, 2.38E+02, 2.385833E+02, 2.391667E+02, 2.3975E+02, 2.40333E+02, 2.409167E+02, 2.415E+02, 2.420833E+02, 2.426667E+02, 2.4325E+02, 2.43833E+02, 2.444167E+02, 2.45E+02, 2.455833E+02, 2.461667E+02, 2.4675E+02, 2.47333E+02, 2.479167E+02, 2.485E+02, 2.490833E+02, 2.496667E+02, 2.5025E+02, 2.50833E+02, 2.514167E+02, 2.52E+02, 2.525833E+02, 2.531667E+02, 2.5375E+02, 2.54333E+02, 2.549167E+02, 2.555E+02, 2.560833E+02, 2.566667E+02, 2.5725E+02, 2.57833E+02, 2.584167E+02, 2.59E+02, 2.595833E+02, 2.601667E+02, 2.6075E+02, 2.61333E+02, 2.619167E+02, 2.625E+02, 2.630833E+02, 2.636667E+02, 2.6425E+02, 2.64833E+02, 2.654167E+02, 2.66E+02, 2.665833E+02, 2.671667E+02, 2.6775E+02, 2.68333E+02, 2.689167E+02, 2.695E+02, 2.700833E+02, 2.706667E+02, 2.7125E+02, 2.71833E+02, 2.724167E+02, 2.73E+02, 2.735833E+02, 2.741667E+02, 2.7475E+02, 2.75333E+02, 2.759167E+02, 2.765E+02, 2.770833E+02, 2.776667E+02, 2.7825E+02, 2.78833E+02, 2.794167E+02, 2.8E+02, 2.805833E+02, 2.811667E+02, 2.8175E+02, 2.82333E+02, 2.829167E+02, 2.835E+02, 2.840833E+02, 2.846667E+02, 2.8525E+02, 2.85833E+02, 2.864167E+02, 2.87E+02, 2.875833E+02, 2.881667E+02, 2.8875E+02, 2.89333E+02, 2.899167E+02, 2.905E+02, 2.910833E+02, 2.916667E+02, 2.9225E+02, 2.92833E+02, 2.934167E+02, 2.94E+02, 2.945833E+02, 2.951667E+02, 2.9575E+02, 2.96333E+02, 2.969167E+02, 2.975E+02, 2.980833E+02, 2.986667E+02, 2.9925E+02, 2.99833E+02, 3.004167E+02, 3.01E+02, 3.015833E+02, 3.021667E+02, 3.0275E+02, 3.03333E+02, 3.039167E+02, 3.045E+02, 3.050833E+02, 3.056667E+02, 3.0625E+02, 3.06833E+02, 3.074167E+02, 3.08E+02, 3.085833E+02, 3.091667E+02, 3.0975E+02, 3.10333E+02, 3.109167E+02, 3.115E+02, 3.120833E+02, 3.126667E+02, 3.1325E+02, 3.13833E+02, 3.144167E+02, 3.15E+02, 3.155833E+02, 3.161667E+02, 3.1675E+02, 3.17333E+02, 3.179167E+02, 3.185E+02, 3.190833E+02, 3.196667E+02, 3.2025E+02, 3.20833E+02, 3.214167E+02, 3.22E+02, 3.225833E+02, 3.231667E+02, 3.2375E+02, 3.24333E+02, 3.249167E+02, 3.255E+02, 3.260833E+02, 3.266667E+02, 3.2725E+02, 3.27833E+02, 3.284167E+02, 3.29E+02, 3.295833E+02, 3.301667E+02, 3.3075E+02, 3.31333E+02, 3.319167E+02, 3.325E+02, 3.330833E+02, 3.336667E+02, 3.3425E+02, 3.34833E+02, 3.354167E+02, 3.36E+02, 3.365833E+02, 3.371667E+02, 3.3775E+02, 3.38333E+02, 3.389167E+02, 3.395E+02, 3.400833E+02, 3.406667E+02, 3.4125E+02, 3.41833E+02, 3.424167E+02, 3.43E+02, 3.435833E+02, 3.441667E+02, 3.4475E+02, 3.45333E+02, 3.459167E+02, 3.465E+02, 3.470833E+02, 3.476667E+02, 3.4825E+02, 3.48833E+02, 3.494167E+02, 3.5E+02, 3.505833E+02, 3.511667E+02, 3.5175E+02, 3.52333E+02, 3.529167E+02, 3.535E+02, 3.540833E+02, 3.546667E+02, 3.5525E+02, 3.55833E+02, 3.564167E+02, 3.57E+02, 3.575833E+02, 3.581667E+02, 3.5875E+02, 3.59333E+02, 3.599167E+02, 3.605E+02, 3.610833E+02, 3.616667E+02, 3.6225E+02, 3.62833E+02, 3.634167E+02, 3.64E+02, 3.645833E+02, 3.651667E+02, 3.6575E+02, 3.66333E+02, 3.669167E+02, 3.675E+02, 3.680833E+02, 3.686667E+02, 3.6925E+02, 3.69833E+02, 3.704167E+02, 3.71E+02, 3.715833E+02, 3.721667E+02, 3.7275E+02, 3.73333E+02, 3.739167E+02, 3.745E+02, 3.750833E+02, 3.756667E+02, 3.7625E+02, 3.76833E+02, 3.774167E+02, 3.78E+02, 3.785833E+02, 3.791667E+02, 3.7975E+02, 3.80333E+02, 3.809167E+02, 3.815E+02, 3.820833E+02, 3.826667E+02, 3.8325E+02, 3.83833E+02, 3.844167E+02, 3.85E+02, 3.855833E+02, 3.861667E+02, 3.8675E+02, 3.87333E+02, 3.879167E+02, 3.885E+02, 3.890833E+02, 3.896667E+02, 3.9025E+02, 3.90833E+02, 3.914167E+02, 3.92E+02, 3.925833E+02, 3.931667E+02, 3.9375E+02, 3.94333E+02, 3.949167E+02, 3.955E+02, 3.960833E+02, 3.966667E+02, 3.9725E+02, 3.97833E+02, 3.984167E+02, 3.99E+02, 3.995833E+02, 4.001667E+02, 4.0075E+02, 4.01333E+02, 4.019167E+02, 4.025E+02, 4.030833E+02, 4.036667E+02, 4.0425E+02, 4.04833E+02, 4.054167E+02, 4.06E+02, 4.065833E+02, 4.071667E+02, 4.0775E+02, 4.08333E+02, 4.089167E+02, 4.095E+02, 4.100833E+02, 4.106667E+02, 4.1125E+02, 4.11833E+02, 4.124167E+02, 4.13E+02, 4.135833E+02, 4.141667E+02, 4.1475E+02, 4.15333E+02, 4.159167E+02, 4.165E+02, 4.170833E+02, 4.176667E+02, 4.1825E+02, 4.18833E+02, 4.194167E+02, 4.2E+02, 4.205833E+02, 4.211667E+02, 4.2175E+02, 4.22333E+02, 4.229167E+02, 4.235E+02, 4.240833E+02, 4.246667E+02, 4.2525E+02, 4.25833E+02, 4.264167E+02, 4.27E+02, 4.275833E+02, 4.281667E+02, 4.2875E+02, 4.29333E+02, 4.299167E+02, 4.305E+02, 4.310833E+02, 4.316667E+02, 4.3225E+02, 4.32833E+02, 4.334167E+02, 4.34E+02, 4.345833E+02, 4.351667E+02, 4.3575E+02, 4.36333E+02, 4.369167E+02, 4.375E+02, 4.380833E+02, 4.386667E+02, 4.3925E+02, 4.39833E+02, 4.404167E+02, 4.41E+02, 4.415833E+02, 4.421667E+02, 4.4275E+02, 4.43333E+02, 4.439167E+02, 4.445E+02, 4.450833E+02, 4.456667E+02, 4.4625E+02, 4.46833E+02, 4.474167E+02, 4.48E+02, 4.485833E+02, 4.491667E+02, 4.4975E+02, 4.50333E+02, 4.509167E+02, 4.515E+02, 4.520833E+02, 4.526667E+02, 4.5325E+02, 4.53833E+02, 4.544167E+02, 4.55E+02, 4.555833E+02, 4.561667E+02, 4.5675E+02, 4.57333E+02, 4.579167E+02, 4.585E+02, 4.590833E+02, 4.596667E+02, 4.6025E+02, 4.60833E+02, 4.614167E+02, 4.62E+02, 4.625833E+02, 4.631667E+02, 4.6375E+02, 4.64333E+02, 4.649167E+02, 4.655E+02, 4.660833E+02, 4.666667E+02, 4.6725E+02, 4.67833E+02, 4.684167E+02, 4.69E+02, 4.695833E+02, 4.701667E+02, 4.7075E+02, 4.71333E+02, 4.719167E+02, 4.725E+02, 4.730833E+02, 4.736667E+02, 4.7425E+02, 4.74833E+02, 4.754167E+02, 4.76E+02, 4.765833E+02, 4.771667E+02, 4.7775E+02, 4.78333E+02, 4.789167E+02, 4.795E+02, 4.800833E+02, 4.806667E+02, 4.8125E+02, 4.81833E+02, 4.824167E+02, 4.83E+02, 4.835833E+02, 4.841667E+02, 4.8475E+02, 4.85333E+02, 4.859167E+02, 4.865E+02, 4.870833E+02, 4.876667E+02, 4.8825E+02, 4.88833E+02, 4.894167E+02, 4.9E+02, 4.905833E+02, 4.911667E+02, 4.9175E+02, 4.92333E+02, 4.929167E+02, 4.935E+02, 4.940833E+02, 4.946667E+02, 4.9525E+02, 4.95833E+02, 4.964167E+02, 4.97E+02, 4.975833E+02, 4.981667E+02, 4.9875E+02, 4.99333E+02, 4.999167E+02, 5.005E+02, 5.010833E+02, 5.016667E+02, 5.0225E+02, 5.02833E+02, 5.034167E+02, 5.04E+02, 5.045833E+02, 5.051667E+02, 5.0575E+02, 5.06333E+02, 5.069167E+02, 5.075E+02, 5.080833E+02, 5.086667E+02, 5.0925E+02, 5.09833E+02, 5.104167E+02, 5.11E+02, 5.115833E+02, 5.121667E+02, 5.1275E+02, 5.13333E+02, 5.139167E+02, 5.145E+02, 5.150833E+02, 5.156667E+02, 5.1625E+02, 5.16833E+02, 5.174167E+02, 5.18E+02, 5.185833E+02, 5.191667E+02, 5.1975E+02, 5.20333E+02, 5.209167E+02, 5.215E+02, 5.220833E+02, 5.226667E+02, 5.2325E+02, 5.23833E+02, 5.244167E+02, 5.25E+02, 5.255833E+02, 5.261667E+02, 5.2675E+02, 5.27333E+02, 5.279167E+02, 5.285E+02, 5.290833E+02, 5.296667E+02, 5.3025E+02, 5.30833E+02, 5.314167E+02, 5.32E+02, 5.325833E+02, 5.331667E+02, 5.3375E+02, 5.34333E+02, 5.349167E+02, 5.355E+02, 5.360833E+02, 5.366667E+02, 5.3725E+02, 5.37833E+02, 5.384167E+02, 5.39E+02, 5.395833E+02, 5.401667E+02, 5.4075E+02, 5.41333E+02, 5.419167E+02, 5.425E+02, 5.430833E+02,

BODY PANEL CORNER POINT LOCATIONS EXPRESSED IN THE AERO COORDINATE SYSTEM
1 AND 2 INDICATE BODY PANEL LEADING-EDGE POINTS, 3 AND 4 INDICATE TRAILING-EDGE POINTS

PANEL NO	PARTS	X ₁	Y ₁	Z ₁	X ₂	Y ₂	Z ₂	X ₃	Y ₃	Z ₃	X ₄	Y ₄	Z ₄
1	1	14.70100	0.00000	1.66500	14.70100	.83250	1.44193	15.59000	0.00000	1.66500	15.59000	.83250	1.44193
2	1	15.59000	0.00000	1.66500	15.59000	.83250	1.44193	17.36800	0.00000	1.66500	17.36800	.83250	1.44193
3	1	17.36800	0.00000	1.66500	17.36800	.83250	1.44193	18.25700	0.00000	1.66500	18.25700	.83250	1.44193
4	1	18.25700	0.00000	1.66500	18.25700	.83250	1.44193	19.14600	0.00000	1.66500	19.14600	.83250	1.44193
5	1	19.14600	0.00000	1.66500	19.14600	.83250	1.44193	20.03500	0.00000	1.66500	20.03500	.83250	1.44193
6	1	20.03500	0.00000	1.66500	20.03500	.83250	1.44193	20.92400	0.00000	1.66500	20.92400	.83250	1.44193
7	1	20.92400	0.00000	1.66500	20.92400	.83250	1.44193	21.81300	0.00000	1.66500	21.81300	.83250	1.44193
8	1	21.81300	0.00000	1.66500	21.81300	.83250	1.44193	22.70200	0.00000	1.66500	22.70200	.83250	1.44193
9	1	22.70200	0.00000	1.66500	22.70200	.83250	1.44193	23.59100	0.00000	1.66500	23.59100	.83250	1.44193
10	1	23.59100	0.00000	1.66500	23.59100	.83250	1.44193	24.48000	0.00000	1.66500	24.48000	.83250	1.44193
11	1	24.48000	0.00000	1.66500	24.48000	.83250	1.44193	27.48500	0.00000	1.66500	27.48500	.83250	1.44193
12	1	27.48500	0.00000	1.66500	27.48500	.83250	1.44193	30.49000	0.00000	1.66500	30.49000	.83250	1.44193
13	1	30.49000	0.00000	1.66500	30.49000	.83250	1.44193	33.49500	0.00000	1.66500	33.49500	.83250	1.44193
14	1	33.49500	0.00000	1.66500	33.49500	.83250	1.44193	36.50000	0.00000	1.66500	36.50000	.83250	1.44193
15	1	36.50000	0.00000	1.66500	36.50000	.83250	1.44193	39.50500	0.00000	1.66500	39.50500	.83250	1.44193
16	1	39.50500	0.00000	1.66500	39.50500	.83250	1.44193	42.51000	0.00000	1.66500	42.51000	.83250	1.44193
17	1	42.51000	0.00000	1.66500	42.51000	.83250	1.44193	45.51500	0.00000	1.66500	45.51500	.83250	1.44193
18	1	45.51500	0.00000	1.66500	45.51500	.83250	1.44193	48.52000	0.00000	1.66500	48.52000	.83250	1.44193
19	1	48.52000	0.00000	1.66500	48.52000	.83250	1.44193	51.52500	0.00000	1.66500	51.52500	.83250	1.44193
20	1	51.52500	0.00000	1.66500	51.52500	.83250	1.44193	54.53000	0.00000	1.66500	54.53000	.83250	1.44193
21	1	54.53000	0.00000	1.66500	54.53000	.83250	1.44193	57.53500	0.00000	1.66500	57.53500	.83250	1.44193
22	1	57.53500	0.00000	1.66500	57.53500	.83250	1.44193	60.54000	0.00000	1.66500	60.54000	.83250	1.44193
23	1	60.54000	0.00000	1.66500	60.54000	.83250	1.44193	63.54500	0.00000	1.66500	63.54500	.83250	1.44193
24	1	63.54500	0.00000	1.66500	63.54500	.83250	1.44193	66.55000	0.00000	1.66500	66.55000	.83250	1.44193
25	1	66.55000	0.00000	1.66500	66.55000	.83250	1.44193	69.55500	0.00000	1.66500	69.55500	.83250	1.44193
26	1	69.55500	0.00000	1.66500	69.55500	.83250	1.44193	72.56000	0.00000	1.66500	72.56000	.83250	1.44193
27	1	72.56000	0.00000	1.66500	72.56000	.83250	1.44193	75.56500	0.00000	1.66500	75.56500	.83250	1.44193
28	1	75.56500	0.00000	1.66500	75.56500	.83250	1.44193	78.57000	0.00000	1.66500	78.57000	.83250	1.44193
29	1	78.57000	0.00000	1.66500	78.57000	.83250	1.44193	81.57500	0.00000	1.66500	81.57500	.83250	1.44193
30	1	81.57500	0.00000	1.66500	81.57500	.83250	1.44193	84.58000	0.00000	1.66500	84.58000	.83250	1.44193
31	1	84.58000	0.00000	1.66500	84.58000	.83250	1.44193	87.58500	0.00000	1.66500	87.58500	.83250	1.44193
32	1	87.58500	0.00000	1.66500	87.58500	.83250	1.44193	90.59000	0.00000	1.66500	90.59000	.83250	1.44193
33	1	90.59000	0.00000	1.66500	90.59000	.83250	1.44193	93.59500	0.00000	1.66500	93.59500	.83250	1.44193
34	1	93.59500	0.00000	1.66500	93.59500	.83250	1.44193	96.60000	0.00000	1.66500	96.60000	.83250	1.44193
35	1	96.60000	0.00000	1.66500	96.60000	.83250	1.44193	99.60500	0.00000	1.66500	99.60500	.83250	1.44193
36	1	99.60500	0.00000	1.66500	99.60500	.83250	1.44193	102.61000	0.00000	1.66500	102.61000	.83250	1.44193
37	1	102.61000	0.00000	1.66500	102.61000	.83250	1.44193	105.61500	0.00000	1.66500	105.61500	.83250	1.44193
38	1	105.61500	0.00000	1.66500	105.61500	.83250	1.44193	108.62000	0.00000	1.66500	108.62000	.83250	1.44193
39	1	108.62000	0.00000	1.66500	108.62000	.83250	1.44193	111.62500	0.00000	1.66500	111.62500	.83250	1.44193
40	1	111.62500	0.00000	1.66500	111.62500	.83250	1.44193	114.63000	0.00000	1.66500	114.63000	.83250	1.44193
41	1	114.63000	0.00000	1.66500	114.63000	.83250	1.44193	117.63500	0.00000	1.66500	117.63500	.83250	1.44193
42	1	117.63500	0.00000	1.66500	117.63500	.83250	1.44193	120.64000	0.00000	1.66500	120.64000	.83250	1.44193
43	1	120.64000	0.00000	1.66500	120.64000	.83250	1.44193	123.64500	0.00000	1.66500	123.64500	.83250	1.44193
44	1	123.64500	0.00000	1.66500	123.64500	.83250	1.44193	126.65000	0.00000	1.66500	126.65000	.83250	1.44193
45	1	126.65000	0.00000	1.66500	126.65000	.83250	1.44193	129.65500	0.00000	1.66500	129.65500	.83250	1.44193
46	1	129.65500	0.00000	1.66500	129.65500	.83250	1.44193	132.66000	0.00000	1.66500	132.66000	.83250	1.44193
47	1	132.66000	0.00000	1.66500	132.66000	.83250	1.44193	135.66500	0.00000	1.66500	135.66500	.83250	1.44193
48	1	135.66500	0.00000	1.66500	135.66500	.83250	1.44193	138.67000	0.00000	1.66500	138.67000	.83250	1.44193
49	1	138.67000	0.00000	1.66500	138.67000	.83250	1.44193	141.67500	0.00000	1.66500	141.67500	.83250	1.44193
50	1	141.67500	0.00000	1.66500	141.67500	.83250	1.44193	144.68000	0.00000	1.66500	144.68000	.83250	1.44193
51	1	144.68000	0.00000	1.66500	144.68000	.83250	1.44193	147.68500	0.00000	1.66500	147.68500	.83250	1.44193
52	1	147.68500	0.00000	1.66500	147.68500	.83250	1.44193	150.69000	0.00000	1.66500	150.69000	.83250	1.44193
53	1	150.69000	0.00000	1.66500	150.69000	.83250	1.44193	153.69500	0.00000	1.66500	153.69500	.83250	1.44193
54	1	153.69500	0.00000	1.66500	153.69500	.83250	1.44193	156.70000	0.00000	1.66500	156.70000	.83250	1.44193
55	1	156.70000	0.00000	1.66500	156.70000	.83250	1.44193	159.70500	0.00000	1.66500	159.70500	.83250	1.44193
56	1	159.70500	0.00000	1.66500	159.70500	.83250	1.44193	162.71000	0.00000	1.66500	162.71000	.83250	1.44193
57	1	162.71000	0.00000	1.66500	162.71000	.83250	1.44193	165.71500	0.00000	1.66500	165.71500	.83250	1.44193
58	1	165.71500	0.00000	1.66500	165.71500	.83250	1.44193	168.72000	0.00000	1.66500	168.72000	.83250	1.44193

59	1	17.36800	1.44193	83250	-1.44193	18.25700	1.44193	83250	-1.44193	18.25700	1.44193	83250	-1.44193
60	1	18.25700	1.44193	83250	-1.44193	19.14600	1.44193	83250	-1.44193	19.14600	1.44193	83250	-1.44193
61	1	19.14600	1.44193	83250	-1.44193	20.03500	1.44193	83250	-1.44193	20.03500	1.44193	83250	-1.44193
62	1	20.03500	1.44193	83250	-1.44193	20.92400	1.44193	83250	-1.44193	20.92400	1.44193	83250	-1.44193
63	1	20.92400	1.44193	83250	-1.44193	21.81300	1.44193	83250	-1.44193	21.81300	1.44193	83250	-1.44193
64	1	21.81300	1.44193	83250	-1.44193	22.70200	1.44193	83250	-1.44193	22.70200	1.44193	83250	-1.44193
65	1	22.70200	1.44193	83250	-1.44193	23.59100	1.44193	83250	-1.44193	23.59100	1.44193	83250	-1.44193
66	1	23.59100	1.44193	83250	-1.44193	24.48000	1.44193	83250	-1.44193	24.48000	1.44193	83250	-1.44193
67	1	24.48000	1.44193	83250	-1.44193	25.36900	1.44193	83250	-1.44193	25.36900	1.44193	83250	-1.44193
68	1	25.36900	1.44193	83250	-1.44193	26.25800	1.44193	83250	-1.44193	26.25800	1.44193	83250	-1.44193
69	1	26.25800	1.44193	83250	-1.44193	27.14700	1.44193	83250	-1.44193	27.14700	1.44193	83250	-1.44193
70	1	27.14700	1.44193	83250	-1.44193	28.03600	1.44193	83250	-1.44193	28.03600	1.44193	83250	-1.44193
71	1	28.03600	1.44193	83250	-1.44193	28.92500	1.44193	83250	-1.44193	28.92500	1.44193	83250	-1.44193
72	1	28.92500	1.44193	83250	-1.44193	29.81400	1.44193	83250	-1.44193	29.81400	1.44193	83250	-1.44193
73	1	29.81400	1.44193	83250	-1.44193	30.70300	1.44193	83250	-1.44193	30.70300	1.44193	83250	-1.44193
74	1	30.70300	1.44193	83250	-1.44193	31.59200	1.44193	83250	-1.44193	31.59200	1.44193	83250	-1.44193
75	1	31.59200	1.44193	83250	-1.44193	32.48100	1.44193	83250	-1.44193	32.48100	1.44193	83250	-1.44193
76	1	32.48100	1.44193	83250	-1.44193	33.37000	1.44193	83250	-1.44193	33.37000	1.44193	83250	-1.44193
77	1	33.37000	1.44193	83250	-1.44193	34.25900	1.44193	83250	-1.44193	34.25900	1.44193	83250	-1.44193
78	1	34.25900	1.44193	83250	-1.44193	35.14800	1.44193	83250	-1.44193	35.14800	1.44193	83250	-1.44193
79	1	35.14800	1.44193	83250	-1.44193	36.03700	1.44193	83250	-1.44193	36.03700	1.44193	83250	-1.44193
80	1	36.03700	1.44193	83250	-1.44193	36.92600	1.44193	83250	-1.44193	36.92600	1.44193	83250	-1.44193
81	1	36.92600	1.44193	83250	-1.44193	37.81500	1.44193	83250	-1.44193	37.81500	1.44193	83250	-1.44193
82	1	37.81500	1.44193	83250	-1.44193	38.70400	1.44193	83250	-1.44193	38.70400	1.44193	83250	-1.44193
83	1	38.70400	1.44193	83250	-1.44193	39.59300	1.44193	83250	-1.44193	39.59300	1.44193	83250	-1.44193
84	1	39.59300	1.44193	83250	-1.44193	40.48200	1.44193	83250	-1.44193	40.48200	1.44193	83250	-1.44193

BODY PANEL CENTROID AND CONTROL POINT LOCATIONS EXPRESSED IN THE AERO COORDINATE SYSTEM

PANEL	X _C	Y _C	Z _C	X _{CP}	Y _{CP}	Z _{CP}	AREA	THETA- INCLIN	ALPHA- INCLIN	CHORD
1	15.14550	.41625	1.55347	15.54555	.41625	1.55347	76620	-26180	0.00000	.88900
2	16.49000	.41625	1.55347	17.27910	.41625	1.55347	1.53240	-26180	0.00000	1.77800
3	17.81250	.41625	1.55347	18.21255	.41625	1.55347	76620	-26180	0.00000	.88900
4	18.70150	.41625	1.55347	19.10155	.41625	1.55347	76620	-26180	0.00000	.88900
5	19.59050	.41625	1.55347	19.99055	.41625	1.55347	76620	-26180	0.00000	.88900
6	20.47950	.41625	1.55347	20.87955	.41625	1.55347	76620	-26180	0.00000	.88900
7	21.36850	.41625	1.55347	21.76855	.41625	1.55347	76620	-26180	0.00000	.88900
8	22.25750	.41625	1.55347	22.65755	.41625	1.55347	76620	-26180	0.00000	.88900
9	23.14650	.41625	1.55347	23.54655	.41625	1.55347	76620	-26180	0.00000	.88900
10	24.03550	.41625	1.55347	24.43555	.41625	1.55347	76620	-26180	0.00000	.88900
11	24.92450	.41625	1.55347	25.32455	.41625	1.55347	2.58991	-26180	0.00000	3.00500
12	25.81350	.41625	1.55347	26.21355	.41625	1.55347	2.58991	-26180	0.00000	3.00500
13	26.70250	.41625	1.55347	27.10255	.41625	1.55347	2.58991	-26180	0.00000	3.00500
14	27.59150	.41625	1.55347	27.99155	.41625	1.55347	2.58991	-26180	0.00000	3.00500
15	28.48050	.41625	1.55347	28.88055	.41625	1.55347	76620	-78540	0.00000	.88900
16	29.36950	.41625	1.55347	29.76955	.41625	1.55347	1.53240	-78540	0.00000	1.77800
17	30.25850	.41625	1.55347	30.65855	.41625	1.55347	76620	-78540	0.00000	.88900
18	31.14750	.41625	1.55347	31.54755	.41625	1.55347	76620	-78540	0.00000	.88900
19	32.03650	.41625	1.55347	32.43655	.41625	1.55347	76620	-78540	0.00000	.88900
20	32.92550	.41625	1.55347	33.32555	.41625	1.55347	76620	-78540	0.00000	.88900
21	33.81450	.41625	1.55347	34.21455	.41625	1.55347	76620	-78540	0.00000	.88900
22	34.70350	.41625	1.55347	35.10355	.41625	1.55347	76620	-78540	0.00000	.88900
23	35.59250	.41625	1.55347	35.99255	.41625	1.55347	76620	-78540	0.00000	.88900
24	36.48150	.41625	1.55347	36.88155	.41625	1.55347	76620	-78540	0.00000	.88900
25	37.37050	.41625	1.55347	37.77055	.41625	1.55347	76620	-78540	0.00000	.88900
26	38.25950	.41625	1.55347	38.65955	.41625	1.55347	2.58991	-78540	0.00000	3.00500
27	39.14850	.41625	1.55347	39.54855	.41625	1.55347	2.58991	-78540	0.00000	3.00500
28	40.03750	.41625	1.55347	40.43755	.41625	1.55347	2.58991	-78540	0.00000	3.00500
29	40.92650	.41625	1.55347	41.32655	.41625	1.55347	2.58991	-78540	0.00000	3.00500
30	41.81550	.41625	1.55347	42.21555	.41625	1.55347	1.53240	-130900	0.00000	1.77800
31	42.70450	.41625	1.55347	43.10455	.41625	1.55347	76620	-130900	0.00000	.88900
32	43.59350	.41625	1.55347	43.99355	.41625	1.55347	76620	-130900	0.00000	.88900
33	44.48250	.41625	1.55347	44.88255	.41625	1.55347	76620	-130900	0.00000	.88900
34	45.37150	.41625	1.55347	45.77155	.41625	1.55347	76620	-130900	0.00000	.88900
35	46.26050	.41625	1.55347	46.66055	.41625	1.55347	76620	-130900	0.00000	.88900
36	47.14950	.41625	1.55347	47.54955	.41625	1.55347	76620	-130900	0.00000	.88900
37	48.03850	.41625	1.55347	48.43855	.41625	1.55347	76620	-130900	0.00000	.88900
38	48.92750	.41625	1.55347	49.32755	.41625	1.55347	76620	-130900	0.00000	.88900
39	49.81650	.41625	1.55347	50.21655	.41625	1.55347	76620	-130900	0.00000	.88900
40	50.70550	.41625	1.55347	51.10555	.41625	1.55347	76620	-130900	0.00000	.88900
41	51.59450	.41625	1.55347	51.99455	.41625	1.55347	76620	-130900	0.00000	.88900
42	52.48350	.41625	1.55347	52.88355	.41625	1.55347	76620	-130900	0.00000	.88900
43	53.37250	.41625	1.55347	53.77255	.41625	1.55347	76620	-130900	0.00000	.88900
44	54.26150	.41625	1.55347	54.66155	.41625	1.55347	76620	-130900	0.00000	.88900
45	55.15050	.41625	1.55347	55.55055	.41625	1.55347	76620	-130900	0.00000	.88900
46	56.03950	.41625	1.55347	56.43955	.41625	1.55347	76620	-130900	0.00000	.88900
47	56.92850	.41625	1.55347	57.32855	.41625	1.55347	76620	-130900	0.00000	.88900
48	57.81750	.41625	1.55347	58.21755	.41625	1.55347	76620	-130900	0.00000	.88900
49	58.70650	.41625	1.55347	59.10655	.41625	1.55347	76620	-130900	0.00000	.88900
50	59.59550	.41625	1.55347	60.00000	.41625	1.55347	76620	-130900	0.00000	.88900
51	60.48450	.41625	1.55347	60.88455	.41625	1.55347	76620	-130900	0.00000	.88900
52	61.37350	.41625	1.55347	61.77355	.41625	1.55347	76620	-130900	0.00000	.88900
53	62.26250	.41625	1.55347	62.66255	.41625	1.55347	76620	-130900	0.00000	.88900
54	63.15150	.41625	1.55347	63.55155	.41625	1.55347	76620	-130900	0.00000	.88900
55	64.04050	.41625	1.55347	64.44055	.41625	1.55347	76620	-130900	0.00000	.88900
56	64.92950	.41625	1.55347	65.32955	.41625	1.55347	76620	-130900	0.00000	.88900
57	65.81850	.41625	1.55347	66.21855	.41625	1.55347	76620	-130900	0.00000	.88900
58	66.70750	.41625	1.55347	67.10755	.41625	1.55347	76620	-130900	0.00000	.88900
59	67.59650	.41625	1.55347	67.99655	.41625	1.55347	76620	-130900	0.00000	.88900
60	68.48550	.41625	1.55347	68.88555	.41625	1.55347	76620	-130900	0.00000	.88900
61	69.37450	.41625	1.55347	69.77455	.41625	1.55347	76620	-130900	0.00000	.88900
62	70.26350	.41625	1.55347	70.66355	.41625	1.55347	76620	-130900	0.00000	.88900
63	71.15250	.41625	1.55347	71.55255	.41625	1.55347	76620	-130900	0.00000	.88900
64	72.04150	.41625	1.55347	72.44155	.41625	1.55347	76620	-130900	0.00000	.88900
65	72.93050	.41625	1.55347	73.33055	.41625	1.55347	76620	-130900	0.00000	.88900
66	73.81950	.41625	1.55347	74.21955	.41625	1.55347	76620	-130900	0.00000	.88900
67	74.70850	.41625	1.55347	75.10855	.41625	1.55347	76620	-130900	0.00000	.88900
68	75.59750	.41625	1.55347	75.99755	.41625	1.55347	76620	-130900	0.00000	.88900
69	76.48650	.41625	1.55347	76.88655	.41625	1.55347	76620	-130900	0.00000	.88900
70	77.37550	.41625	1.55347	77.77555	.41625	1.55347	76620	-130900	0.00000	.88900
71	78.26450	.41625	1.55347	78.66455	.41625	1.55347	76620	-130900	0.00000	.88900
72	79.15350	.41625	1.55347	79.55355	.41625	1.55347	76620	-130900	0.00000	.88900
73	80.04250	.41625	1.55347	80.44255	.41625	1.55347	76620	-130900	0.00000	.88900
74	80.93150	.41625	1.55347	81.33155	.41625	1.55347	76620	-130900	0.00000	.88900
75	81.82050	.41625	1.55347	82.22055	.41625	1.55347	76620	-130900	0.00000	.88900
76	82.70950	.41625	1.55347	83.10955	.41625	1.55347	76620	-130900	0.00000	.88900
77	83.59850	.41625	1.55347	83.99855	.41625	1.55347	76620	-130900	0.00000	.88900
78	84.48750	.41625	1.55347	84.88755	.41625	1.55347	76620	-130900	0.00000	.88900
79	85.37650	.41625	1.55347	85.77655	.41625	1.55347	76620	-130900	0.00000	.88900
80	86.26550	.41625	1.55347	86.66555	.41625	1.55347	76620	-130900	0.00000	.88900
81	87.15450	.41625	1.55347	87.55455	.41625	1.55347	76620	-130900	0.00000	.88900
82	88.04350	.41625	1.55347	88.44355	.41625	1.55347	76620	-130900	0.00000	.88900
83	88.93250	.41625	1.55347	89.33255	.41625	1.55347	76620	-130900	0.00000	.88900
84	89.82150	.41625	1.55347	90.22155	.41625	1.55347	76620	-130900	0.00000	.88900
85	90.71050	.41625	1.55347	91.11055	.41625	1.55347	76620	-130900	0.00000	.88900
86	91.59950	.41625	1.55347	91.99955	.41625	1.55347	76620	-130900	0.00000	.88900
87	92.48850	.41625	1.55347	92.88855	.41625	1.55347	76620	-130900	0.00000	.88900
88	93.37750	.41625	1.55347	93.77755	.41625	1.55347	76620	-130900	0.00000	.88900
89	94.26650	.41625	1.55347	94.66655	.41625	1.55347	76620	-130900	0.00000	.88900
90	95.15550	.41625	1.55347	95.55555	.41625	1.55347	76620	-130900	0.00000	.88900
91	96.04450	.41625	1.55347	96.44455	.41625	1.55347	76620	-130900	0.00000	.88900
92	96.93350	.41625	1.55347	97.33355	.41625	1.55347	76620	-130900	0.00000	.88900
93	97.82250	.41625	1.55347	98.22255	.41625	1.55347	76620	-130900	0.00000	.88900
94	98.71150	.41625	1.55347	99.11155	.41625	1.55347	76620	-130900	0.00000	.88900
95	99.60050	.41625	1.55347	100.00000	.41625	1.55347	76620	-130900	0.00000	.88900
96	100.48950	.41625	1.55347	100.88955	.41625	1.55347	76620	-130900	0.00000	.88900
97	101.37850	.41625	1.55347	101.77855	.41625	1.55347	76620	-130900	0.00000	.88900
98	102.26750	.41625	1.5534							

WING PANEL CORNER POINT LOCATIONS EXPRESSED IN THE AERO COORDINATE SYSTEM
1 AND 2 INDICATE WING PANEL LEADING-EDGE POINTS, 3 AND 4 INDICATE TRAILING-EDGE POINTS

PANEL NO	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4
WING NO.	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4
1	15.59000	1.66500	0.00000	18.00000	3.73100	0.00000	16.47900	1.66500	0.00000	18.75120	0.00000	18.75120	3.73100	0.00000	18.75120	0.00000	3.73100	0.00000	18.75120	0.00000
2	16.47900	1.66500	0.00000	18.75120	3.73100	0.00000	17.36800	1.66500	0.00000	19.50240	0.00000	19.50240	3.73100	0.00000	19.50240	0.00000	3.73100	0.00000	19.50240	0.00000
3	17.36800	1.66500	0.00000	19.50240	3.73100	0.00000	18.25700	1.66500	0.00000	20.25360	0.00000	20.25360	3.73100	0.00000	20.25360	0.00000	3.73100	0.00000	20.25360	0.00000
4	18.25700	1.66500	0.00000	20.25360	3.73100	0.00000	19.14600	1.66500	0.00000	21.00480	0.00000	21.00480	3.73100	0.00000	21.00480	0.00000	3.73100	0.00000	21.00480	0.00000
5	19.14600	1.66500	0.00000	21.00480	3.73100	0.00000	20.03500	1.66500	0.00000	21.75600	0.00000	21.75600	3.73100	0.00000	21.75600	0.00000	3.73100	0.00000	21.75600	0.00000
6	20.03500	1.66500	0.00000	21.75600	3.73100	0.00000	20.92400	1.66500	0.00000	22.50720	0.00000	22.50720	3.73100	0.00000	22.50720	0.00000	3.73100	0.00000	22.50720	0.00000
7	20.92400	1.66500	0.00000	22.50720	3.73100	0.00000	21.81300	1.66500	0.00000	23.25840	0.00000	23.25840	3.73100	0.00000	23.25840	0.00000	3.73100	0.00000	23.25840	0.00000
8	21.81300	1.66500	0.00000	23.25840	3.73100	0.00000	22.70200	1.66500	0.00000	24.00960	0.00000	24.00960	3.73100	0.00000	24.00960	0.00000	3.73100	0.00000	24.00960	0.00000
9	22.70200	1.66500	0.00000	24.00960	3.73100	0.00000	23.59100	1.66500	0.00000	24.76080	0.00000	24.76080	3.73100	0.00000	24.76080	0.00000	3.73100	0.00000	24.76080	0.00000
10	23.59100	1.66500	0.00000	24.76080	3.73100	0.00000	23.48000	1.66500	0.00000	25.51200	0.00000	25.51200	3.73100	0.00000	25.51200	0.00000	3.73100	0.00000	25.51200	0.00000
11	24.48000	1.66500	0.00000	25.51200	3.73100	0.00000	24.36800	1.66500	0.00000	26.26320	0.00000	26.26320	3.73100	0.00000	26.26320	0.00000	3.73100	0.00000	26.26320	0.00000
12	25.36800	1.66500	0.00000	26.26320	3.73100	0.00000	25.25700	1.66500	0.00000	27.01440	0.00000	27.01440	3.73100	0.00000	27.01440	0.00000	3.73100	0.00000	27.01440	0.00000
13	26.25700	1.66500	0.00000	27.01440	3.73100	0.00000	26.14600	1.66500	0.00000	27.76560	0.00000	27.76560	3.73100	0.00000	27.76560	0.00000	3.73100	0.00000	27.76560	0.00000
14	27.14600	1.66500	0.00000	27.76560	3.73100	0.00000	27.03500	1.66500	0.00000	28.51680	0.00000	28.51680	3.73100	0.00000	28.51680	0.00000	3.73100	0.00000	28.51680	0.00000
15	28.03500	1.66500	0.00000	28.51680	3.73100	0.00000	27.92400	1.66500	0.00000	29.26800	0.00000	29.26800	3.73100	0.00000	29.26800	0.00000	3.73100	0.00000	29.26800	0.00000
16	28.92400	1.66500	0.00000	29.26800	3.73100	0.00000	28.81300	1.66500	0.00000	30.01920	0.00000	30.01920	3.73100	0.00000	30.01920	0.00000	3.73100	0.00000	30.01920	0.00000
17	29.81300	1.66500	0.00000	30.01920	3.73100	0.00000	29.70200	1.66500	0.00000	30.77040	0.00000	30.77040	3.73100	0.00000	30.77040	0.00000	3.73100	0.00000	30.77040	0.00000
18	30.70200	1.66500	0.00000	30.77040	3.73100	0.00000	30.59100	1.66500	0.00000	31.52160	0.00000	31.52160	3.73100	0.00000	31.52160	0.00000	3.73100	0.00000	31.52160	0.00000
19	31.59100	1.66500	0.00000	31.52160	3.73100	0.00000	31.48000	1.66500	0.00000	32.27280	0.00000	32.27280	3.73100	0.00000	32.27280	0.00000	3.73100	0.00000	32.27280	0.00000
20	32.48000	1.66500	0.00000	32.27280	3.73100	0.00000	32.36800	1.66500	0.00000	33.02400	0.00000	33.02400	3.73100	0.00000	33.02400	0.00000	3.73100	0.00000	33.02400	0.00000
21	33.36800	1.66500	0.00000	33.02400	3.73100	0.00000	33.25700	1.66500	0.00000	33.77520	0.00000	33.77520	3.73100	0.00000	33.77520	0.00000	3.73100	0.00000	33.77520	0.00000
22	34.25700	1.66500	0.00000	33.77520	3.73100	0.00000	34.14600	1.66500	0.00000	34.52640	0.00000	34.52640	3.73100	0.00000	34.52640	0.00000	3.73100	0.00000	34.52640	0.00000
23	35.14600	1.66500	0.00000	34.52640	3.73100	0.00000	35.03500	1.66500	0.00000	35.30720	0.00000	35.30720	3.73100	0.00000	35.30720	0.00000	3.73100	0.00000	35.30720	0.00000
24	36.03500	1.66500	0.00000	35.30720	3.73100	0.00000	35.92400	1.66500	0.00000	36.17840	0.00000	36.17840	3.73100	0.00000	36.17840	0.00000	3.73100	0.00000	36.17840	0.00000
25	36.92400	1.66500	0.00000	36.17840	3.73100	0.00000	36.81300	1.66500	0.00000	36.92960	0.00000	36.92960	3.73100	0.00000	36.92960	0.00000	3.73100	0.00000	36.92960	0.00000
26	37.81300	1.66500	0.00000	36.92960	3.73100	0.00000	37.70200	1.66500	0.00000	37.64080	0.00000	37.64080	3.73100	0.00000	37.64080	0.00000	3.73100	0.00000	37.64080	0.00000
27	38.70200	1.66500	0.00000	37.70200	3.73100	0.00000	38.59100	1.66500	0.00000	38.57920	0.00000	38.57920	3.73100	0.00000	38.57920	0.00000	3.73100	0.00000	38.57920	0.00000
28	39.59100	1.66500	0.00000	38.59100	3.73100	0.00000	39.48000	1.66500	0.00000	39.46720	0.00000	39.46720	3.73100	0.00000	39.46720	0.00000	3.73100	0.00000	39.46720	0.00000
29	40.48000	1.66500	0.00000	39.48000	3.73100	0.00000	40.36800	1.66500	0.00000	40.35440	0.00000	40.35440	3.73100	0.00000	40.35440	0.00000	3.73100	0.00000	40.35440	0.00000
30	41.36800	1.66500	0.00000	40.36800	3.73100	0.00000	41.25700	1.66500	0.00000	41.24320	0.00000	41.24320	3.73100	0.00000	41.24320	0.00000	3.73100	0.00000	41.24320	0.00000
31	42.25700	1.66500	0.00000	41.25700	3.73100	0.00000	42.14600	1.66500	0.00000	42.13200	0.00000	42.13200	3.73100	0.00000	42.13200	0.00000	3.73100	0.00000	42.13200	0.00000
32	43.14600	1.66500	0.00000	42.14600	3.73100	0.00000	43.03500	1.66500	0.00000	43.02080	0.00000	43.02080	3.73100	0.00000	43.02080	0.00000	3.73100	0.00000	43.02080	0.00000
33	44.03500	1.66500	0.00000	43.03500	3.73100	0.00000	43.92400	1.66500	0.00000	43.90960	0.00000	43.90960	3.73100	0.00000	43.90960	0.00000	3.73100	0.00000	43.90960	0.00000
34	44.92400	1.66500	0.00000	43.92400	3.73100	0.00000	44.81300	1.66500	0.00000	44.79920	0.00000	44.79920	3.73100	0.00000	44.79920	0.00000	3.73100	0.00000	44.79920	0.00000
35	45.81300	1.66500	0.00000	44.81300	3.73100	0.00000	45.70200	1.66500	0.00000	45.68720	0.00000	45.68720	3.73100	0.00000	45.68720	0.00000	3.73100	0.00000	45.68720	0.00000
36	46.70200	1.66500	0.00000	45.70200	3.73100	0.00000	46.59100	1.66500	0.00000	46.57600	0.00000	46.57600	3.73100	0.00000	46.57600	0.00000	3.73100	0.00000	46.57600	0.00000
37	47.59100	1.66500	0.00000	46.59100	3.73100	0.00000	47.48000	1.66500	0.00000	47.46400	0.00000	47.46400	3.73100	0.00000	47.46400	0.00000	3.73100	0.00000	47.46400	0.00000
38	48.48000	1.66500	0.00000	47.48000	3.73100	0.00000	48.36800	1.66500	0.00000	48.35200	0.00000	48.35200	3.73100	0.00000	48.35200	0.00000	3.73100	0.00000	48.35200	0.00000
39	49.36800	1.66500	0.00000	48.36800	3.73100	0.00000	49.25700	1.66500	0.00000	49.24240	0.00000	49.24240	3.73100	0.00000	49.24240	0.00000	3.73100	0.00000	49.24240	0.00000
40	50.25700	1.66500	0.00000	49.25700	3.73100	0.00000	50.14600	1.66500	0.00000	50.13120	0.00000	50.13120	3.73100	0.00000	50.13120	0.00000	3.73100	0.00000	50.13120	0.00000
41	51.14600	1.66500	0.00000	50.14600	3.73100	0.00000	51.03500	1.66500	0.00000	51.02000	0.00000	51.02000	3.73100	0.00000	51.02000	0.00000	3.73100	0.00000	51.02000	0.00000
42	52.03500	1.66500	0.00000	51.03500	3.73100	0.00000	51.92400	1.66500	0.00000	51.90800	0.00000	51.90800	3.73100	0.00000	51.90800	0.00000	3.73100	0.00000	51.90800	0.00000
43	52.92400	1.66500	0.00000	51.92400	3.73100	0.00000	52.81300	1.66500	0.00000	52.79600	0.00000	52.79600	3.73100	0.00000	52.79600	0.00000	3.73100	0.00000	52.79600	0.00000
44	53.81300	1.66500	0.00000	52.81300	3.73100	0.00000	53.70200	1.66500	0.00000	53.68320	0.00000	53.68320	3.73100	0.00000	53.68320	0.00000	3.73100	0.00000	53.68320	0.00000
45	54.70200	1.66500	0.00000	53.70200	3.73100	0.00000	54.59100	1.66500	0.00000	54.57040	0.00000	54.57040	3.73100	0.00000	54.57040	0.00000	3.73100	0.00000	54.57040	0.00000
46	55.59100	1.66500	0.00000	54.59100	3.73100	0.00000	55.48000	1.66500	0.00000	55.45760	0.00000	55.45760	3.73100	0.00000	55.45760	0.00000	3.73100	0.00000	55.45760	0.00000
47	56.48000	1.66500	0.00000																	

WING PANEL CENTROID AND CONTROL POINT LOCATIONS EXPRESSED IN THE AERO COORDINATE SYSTEM

PANEL	X C	Y C	Z C	X CP	Y CP	Z CP	AREA	THETA- DINED	ALPHA- CAMBER	CHORD
1	17.17227	2.66907	0.00000	17.54218	2.66907	0.00000	1.69433	0.00000	0.00000	.87203
2	17.99430	2.66907	0.00000	18.36421	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
3	18.81633	2.66907	0.00000	19.18624	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
4	19.63836	2.66907	0.00000	20.00827	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
5	20.46039	2.66907	0.00000	20.83030	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
6	21.28242	2.66907	0.00000	21.65233	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
7	22.10445	2.66907	0.00000	22.47436	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
8	22.92648	2.66907	0.00000	23.29639	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
9	23.74851	2.66907	0.00000	24.11842	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
10	24.57053	2.66907	0.00000	24.94045	2.66907	0.00000	1.69433	0.00000	0.00000	.82203
11	19.50675	4.72923	0.00000	19.81483	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
12	20.13137	4.72923	0.00000	20.49945	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
13	20.35599	4.72923	0.00000	21.18407	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
14	21.56061	4.72923	0.00000	21.86868	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
15	22.24523	4.72923	0.00000	22.55330	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
16	22.92984	4.72923	0.00000	23.23792	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
17	23.61446	4.72923	0.00000	23.92254	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
18	24.29908	4.72923	0.00000	24.60716	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
19	24.98370	4.72923	0.00000	25.29178	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
20	25.66832	4.72923	0.00000	25.97640	4.72923	0.00000	1.40963	0.00000	0.00000	.68462
21	21.83788	6.78643	0.00000	22.08421	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
22	22.35288	6.78643	0.00000	22.63162	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
23	22.92629	6.78643	0.00000	23.17902	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
24	23.48010	6.78643	0.00000	23.72643	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
25	24.03750	6.78643	0.00000	24.27383	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
26	24.57491	6.78643	0.00000	24.82124	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
27	25.12231	6.78643	0.00000	25.36865	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
28	25.66972	6.78643	0.00000	25.91605	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
29	26.21713	6.78643	0.00000	26.46346	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
30	26.76453	6.78643	0.00000	27.01087	6.78643	0.00000	1.12494	0.00000	0.00000	.54741
31	24.16225	8.83767	0.00000	24.75760	8.83767	0.00000	.84024	0.00000	0.00000	.41059
32	24.51284	8.83767	0.00000	25.15820	8.83767	0.00000	.84024	0.00000	0.00000	.41059
33	24.93433	8.83767	0.00000	25.55879	8.83767	0.00000	.84024	0.00000	0.00000	.41059
34	25.37402	8.83767	0.00000	25.95938	8.83767	0.00000	.84024	0.00000	0.00000	.41059
35	25.80461	8.83767	0.00000	26.35997	8.83767	0.00000	.84024	0.00000	0.00000	.41059
36	26.21520	8.83767	0.00000	26.75997	8.83767	0.00000	.84024	0.00000	0.00000	.41059
37	26.62579	8.83767	0.00000	27.15956	8.83767	0.00000	.84024	0.00000	0.00000	.41059
38	27.03638	8.83767	0.00000	27.55915	8.83767	0.00000	.84024	0.00000	0.00000	.41059
39	27.44697	8.83767	0.00000	27.95874	8.83767	0.00000	.84024	0.00000	0.00000	.41059
40	27.85757	10.87377	0.00000	28.35833	10.87377	0.00000	.55555	0.00000	0.00000	.27478
41	28.26816	10.87377	0.00000	28.75792	10.87377	0.00000	.55555	0.00000	0.00000	.27478
42	28.67875	10.87377	0.00000	29.15751	10.87377	0.00000	.55555	0.00000	0.00000	.27478
43	29.08934	10.87377	0.00000	29.55710	10.87377	0.00000	.55555	0.00000	0.00000	.27478
44	29.49993	10.87377	0.00000	29.95669	10.87377	0.00000	.55555	0.00000	0.00000	.27478
45	29.91052	10.87377	0.00000	30.35628	10.87377	0.00000	.55555	0.00000	0.00000	.27478
46	30.32111	10.87377	0.00000	30.75587	10.87377	0.00000	.55555	0.00000	0.00000	.27478
47	30.73170	10.87377	0.00000	31.15546	10.87377	0.00000	.55555	0.00000	0.00000	.27478
48	31.14229	10.87377	0.00000	31.55505	10.87377	0.00000	.55555	0.00000	0.00000	.27478
49	31.55288	10.87377	0.00000	31.95464	10.87377	0.00000	.55555	0.00000	0.00000	.27478
50	31.96347	10.87377	0.00000	32.35423	10.87377	0.00000	.55555	0.00000	0.00000	.27478

EXIT INTAPE

EXIT EVAL

EXIT EVAL

DESCRIPTION OF CASE REQUESTED

SYMMETRICAL CONFIGURATION - PANELS LOCATED ON BOTH SIDES OF X-Z PLANE (SYM = 1.)

CASE = 2. CALCULATE CL, GIVEN SHAPE

CPCALC = 0. LINEAR CP

POLAR = 1. POLARS REQUESTED

THICK = 1. WING THICKNESS PRESSURES TO BE ADDED

VOUT = 0. VELOCITY COMPONENTS NOT TO BE PRINTED

MACH NUMBER = 2.0100

POINT ABOUT WHICH THE MOMENTS ARE TO BE COMPUTED

X-COORDINATE = 0.0000

Z-COORDINATE = 0.0000

REFERENCE CHORD LENGTH = 1.0000

WING REFERENCE AREA = 56.2468

WING SEMI-SPAN = 1.0000

HEIGHT OF WING PLANE ABOVE BODY AXIS = 0.0000

INCLINATION OF BODY AXIS WITH RESPECT TO DEFINING AXIS = 0.0000 DEG.

ANGLE OF ATTACK WITH RESPECT TO BODY AXIS = 5.0000 DEG.

PRESSURES, FORCES, AND MOMENTS ON ISOLATED BODY

CD = .00985 CL = .02033 CM = -.11461

BODY PRESSURE COEFFICIENTS(CP)

THETA(DEG.)	0.0000	30.0000	60.0000	90.0000	120.0000	150.0000	180.0000
0.0000	.12638	.13607	.16616	.21578	.27524	.32501	.34454
1.3300	.11196	.12129	.15040	.19876	.25703	.30596	.32520
2.6600	.08963	.09797	.12453	.16979	.22539	.27265	.29134
3.9900	.08156	.08911	.11368	.15656	.21022	.25633	.27465
5.3200	.06710	.07400	.09689	.13771	.18955	.23448	.25241
6.6500	.05376	.05992	.08089	.11935	.16914	.21278	.23027
7.9800	.04049	.04587	.06482	.10079	.14842	.19067	.20769
9.3100	.02795	.03250	.04931	.08266	.12800	.16878	.18531
10.6400	.01576	.01944	.03401	.06459	.10749	.14671	.16272
11.9700	.00414	.00691	.01912	.04637	.08710	.12667	.14011
13.3000	-.01976	-.01824	-.00931	-.01422	-.03081	-.05888	-.10047
14.6300	-.04166	-.04303	-.04159	-.02744	-.00080	-.03041	-.04313
15.9600	-.04718	-.05153	-.05788	-.05347	-.03395	-.01008	-.00068
17.2900	-.03317	-.02981	-.02214	-.04519	-.03329	-.01375	-.00346
18.6200	-.00714	-.01505	-.03072	-.03808	-.02921	-.01244	-.00413
19.9500	.00291	-.00354	-.02270	-.03210	-.02531	-.01006	-.00231
21.2800	.00802	-.00052	-.01798	-.02795	-.02190	-.00730	-.00019
22.6100	.01049	.00208	-.01512	-.02491	-.01887	-.00442	.00299
23.9400	.01146	.00324	-.01348	-.02279	-.01645	-.00189	.00553
25.2700	.01175	.00372	-.01254	-.02133	-.01462	.00011	.00759
26.6000	.01184	.00395	-.01195	-.02032	-.01330	.00161	.00913
27.9300	.01195	.00417	-.01148	-.01936	-.01230	.00274	.01030
29.2600	.01213	.00441	-.01108	-.01899	-.01159	.00354	.01112
30.5900	.01236	.00467	-.01074	-.01855	-.01107	.00410	.01170
31.9200	.01263	.00495	-.01043	-.01821	-.01071	.00447	.01207
33.2500	.01329	.00562	-.00973	-.01747	-.00993	.00526	.01287

INCREMENTAL PRESSURES, FORCES, AND MOMENTS ON BODY PANELS DUE TO WING

CD = .00391 CL = .04487 CM = -1.08710

BODY PANEL PRESSURE COEFFICIENT (CP)

THETA (DEG.)	15.0000	45.0000	75.0000	105.0000	135.0000	165.0000
ROW NO.						
1	-0.00000	-0.00000	-0.00000	-0.00000	-0.00000	-0.00000
2	-.00043	-.00167	-.08854	-.10290	-.00194	-.00049
3	-.00010	-.03029	-.10842	-.12602	-.03531	-.00013
4	-.00323	-.05372	-.09385	-.11178	-.06733	-.00371
5	-.01864	-.06848	-.08109	-.09836	-.08034	-.02180
6	-.03965	-.06519	-.07267	-.08979	-.07846	-.04632
7	-.05621	-.05846	-.06123	-.07839	-.07198	-.06682
8	-.06354	-.05818	-.05944	-.07266	-.07282	-.07624
9	-.06840	-.05375	-.06076	-.06500	-.06955	-.08325
10	-.06681	-.06076	-.06991	-.06527	-.06918	-.08299
11	-.07271	-.05738	-.03344	-.00491	-.04445	-.07658
12	-.05496	-.02850	-.00645	-.00591	-.02307	-.03984
13	-.01835	-.00944	-.00372	-.00713	-.01996	-.01979
14	-.00382	-.00108	-.00320	-.00215	-.00438	-.00843

BODY PANEL SLOPE (DR/DX)

THETA (DEG.)	15.0000	45.0000	75.0000	105.0000	135.0000	165.0000
ROW NO.						
1	-.08521	-.06262	-.02350	-.02167	-.06079	-.08338
2	-.08509	-.06251	-.02339	-.02178	-.06090	-.08349
3	-.08482	-.06224	-.02312	-.02206	-.06118	-.08376
4	-.08458	-.06199	-.02287	-.02230	-.06142	-.08401
5	-.08439	-.06160	-.02268	-.02249	-.06161	-.08420
6	-.08420	-.06161	-.02249	-.02268	-.06180	-.08439
7	-.08408	-.06149	-.02237	-.02280	-.06192	-.08451
8	-.08396	-.06138	-.02226	-.02292	-.06204	-.08462
9	-.08390	-.06131	-.02219	-.02298	-.06210	-.08469
10	-.08385	-.06126	-.02214	-.02303	-.06215	-.08473
11	-.08396	-.06138	-.02226	-.02292	-.06204	-.08462
12	-.08416	-.06158	-.02246	-.02271	-.06183	-.08442
13	-.08437	-.06178	-.02266	-.02251	-.06163	-.08422
14	-.08459	-.06201	-.02289	-.02229	-.06141	-.08399

PRESSURES, FORCES, AND MOMENTS ON WING PANELS IN PRESENCE OF BODY

CD = .02268 CL = .25441 CM = -5.93827

SECTION CD DISTRIBUTION

SPANWISE STATION	1	2	3	4	5
	.01821	.02259	.02586	.02629	.02466

SECTION CL DISTRIBUTION

SPANWISE STATION	1	2	3	4	5
	.20894	.24837	.28822	.29282	.28191

UPPER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.18718	-.15204	-.18585	-.19518	-.14959
2	-.15988	-.17569	-.17826	-.18388	-.15129
3	-.12633	-.18300	-.17832	-.17304	-.16301
4	-.11276	-.17666	-.18335	-.17651	-.16914
5	-.08966	-.15922	-.15723	-.17379	-.16907
6	-.08231	-.14686	-.12687	-.16909	-.16889
7	-.08209	-.12585	-.13803	-.16496	-.16705
8	-.07656	-.07986	-.14025	-.15503	-.16503
9	-.07950	-.03800	-.13214	-.14806	-.16475
10	-.07877	-.04064	-.12008	-.14484	-.16630

LOWER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	.20593	.16504	.10942	.09080	.13103
2	.16103	.15584	.11964	.10271	.12951
3	.12764	.14942	.12413	.11481	.11827
4	.11462	.12657	.12540	.11275	.11271
5	.09035	.10926	.15681	.17333	.11337
6	.07812	.09359	.18636	.12458	.11415
7	.07302	.07873	.15989	.13181	.11664
8	.05902	.09938	.13703	.14529	.11945
9	.05905	.12564	.12259	.15548	.12059
10	.05353	.11186	.11156	.15948	.12001

WING PANEL PRESSURE DIFFERENCE(CL)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	.39311	.31708	.29527	.28598	.28042
2	.32091	.33153	.29791	.28659	.28081
3	.25597	.33541	.30245	.28785	.28127
4	.22738	.30323	.30875	.28926	.28185
5	.18001	.26848	.31403	.29111	.28244
6	.16043	.24046	.31323	.29367	.28303
7	.15511	.20457	.29792	.24677	.28369
8	.13558	.17924	.27727	.30032	.28447
9	.13855	.16364	.25473	.30354	.28534
10	.13230	.15250	.23163	.30433	.28631

UPPER SURFACE WING PANEL SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.07227	-.07472	-.10342	-.11082	-.08727
2	-.07227	-.08667	-.10882	-.10527	-.08727
3	-.07227	-.09772	-.11137	-.09967	-.08727
4	-.07232	-.10507	-.11147	-.09932	-.08727
5	-.07247	-.10937	-.08947	-.09867	-.08727
6	-.07272	-.11107	-.06797	-.09807	-.08727
7	-.07307	-.11067	-.07042	-.09752	-.08727
8	-.07347	-.08622	-.07427	-.09697	-.08727
9	-.07387	-.06237	-.07742	-.09642	-.08727
10	-.07432	-.06497	-.08252	-.09592	-.08727

LOWER SURFACE WING PANEL SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.10227	-.09982	-.07112	-.06372	-.08727
2	-.10227	-.08787	-.06572	-.06927	-.08727
3	-.10227	-.07682	-.06317	-.07487	-.08727
4	-.10222	-.06947	-.06307	-.07522	-.08727
5	-.10207	-.06517	-.08507	-.07587	-.08727
6	-.10182	-.06347	-.10657	-.07647	-.08727
7	-.10147	-.06387	-.10412	-.07702	-.08727
8	-.10107	-.08832	-.10027	-.07757	-.08727
9	-.10067	-.11217	-.09712	-.07812	-.08727
10	-.10022	-.10957	-.09202	-.07862	-.08727

WING CAMBER SLOPE(DZ/DX)

SPANWISE STATION CHORDWISE STATION	1	2	3	4	5
1	-.08727	-.08727	-.08727	-.08727	-.08727
2	-.08727	-.08727	-.08727	-.08727	-.08727
3	-.08727	-.08727	-.08727	-.08727	-.08727
4	-.08727	-.08727	-.08727	-.08727	-.08727
5	-.08727	-.08727	-.08727	-.08727	-.08727
6	-.08727	-.08727	-.08727	-.08727	-.08727
7	-.08727	-.08727	-.08727	-.08727	-.08727
8	-.08727	-.08727	-.08727	-.08727	-.08727
9	-.08727	-.08727	-.08727	-.08727	-.08727
10	-.08727	-.08727	-.08727	-.08727	-.08727

WING CHORD LENGTHS(C)	8.22030	6.84619	5.47406	4.10591	2.74785
-----------------------	---------	---------	---------	---------	---------

FORCES AND MOMENTS ON WING-BODY COMBINATION

CD = .03644 CL = .31961 CM = -7.13999

BODY PRESSURE COEFFICIENTS (CP), INCLUDING THE EFFECT OF WING

THETA (DEG)	0.0000	30.0000	60.0000	90.0000	120.0000	150.0000	180.0000
0.0000	.12638	.13607	.16616	.21578	.27524	.32501	.34454
1.0000	.11196	.12129	.15040	.19876	.25703	.30596	.32520
2.0000	.08963	.09797	.12453	.16979	.22539	.27265	.29134
3.0000	.08156	.08911	.11368	.15656	.21022	.25633	.27465
4.0000	.06710	.07400	.09689	.13771	.18955	.23448	.25241
5.0000	.05376	.05992	.08089	.11935	.16914	.21278	.23027
6.0000	.04049	.04587	.06482	.10079	.14842	.19067	.20769
7.0000	.02795	.03250	.04931	.08266	.12800	.16878	.18531
8.0000	.01576	.01944	.03401	.06459	.10749	.14671	.16272
9.0000	.00414	.00691	.01912	.04677	.08710	.12467	.14011
10.0000	-.01976	-.01824	-.00931	-.01422	-.05081	-.08588	-.10047
11.0000	-.04166	-.04303	-.04159	-.02744	-.00800	-.03041	-.04313
12.0000	-.04718	-.05153	-.05188	-.03347	-.03595	-.01008	-.00068
13.0000	-.02317	-.02981	-.04214	-.04519	-.03229	-.01275	-.00346
14.0000	-.00714	-.01505	-.03072	-.03808	-.02921	-.01244	-.00413
15.0000	.00305	.03023	.03075	.03376	.01702	.01744	.00148
16.0000	.00323	.03347	.03900	.02858	.00086	.02940	.00684
17.0000	.00133	.03776	.04576	.02512	.01412	.03968	.01477
18.0000	-.00116	.04142	.04992	.02311	.02218	.04709	.02128
19.0000	-.00299	.04319	.05103	.02211	.02337	.05102	.02575
20.0000	-.00340	.04239	.04924	.02168	.02459	.05142	.02795
21.0000	-.00210	.03892	.04509	.02149	.02103	.04873	.02803
22.0000	.00082	.03317	.03942	.02143	.01570	.04361	.02628
23.0000	.00503	.02581	.03302	.02148	.00944	.03685	.02319
24.0000	.01014	.01751	.02851	.02170	.00280	.02913	.01920
25.0000	.01329	.00562	-.00973	-.01747	-.00993	.00526	.01287

AERODYNAMIC PRESSURE ON THE BODY - - CENTROID OF FINITE ELEMENT AS GENERATED BY NSWC CODE IN THE
SAME LOCAL COORDINATE SYSTEM

ELEMENT	X	THETA	PRESSURE	ELEMENT	X	THETA	PRESSURE
90	.844E+01	.280E+03	.428E+00	95	.908E+01	.200E+03	.338E+01
100	.844E+01	.130E+03	.322E+01	105	.908E+01	.498E+02	-.401E-01
110	.104E+02	.340E+03	-.721E+00				

PRESSURE AT CONTROL POINT - UPPER SURFACE
X Y PRESSURE

17.5422	2.6691	-.7782E+01
18.3642	2.5691	-.6647E+01
19.1862	2.6691	-.5252E+01
20.0083	2.6691	-.4685E+01
20.8303	2.6691	-.3727E+01
21.6523	2.6691	-.3422E+01
22.4744	2.6691	-.3413E+01
23.2964	2.6691	-.3183E+01
24.1184	2.6691	-.3305E+01
24.9404	2.6691	-.3275E+01
19.8148	4.7292	-.6321E+01
20.4994	4.7292	-.7304E+01
21.1841	4.7292	-.7608E+01
21.8687	4.7292	-.7344E+01
22.5533	4.7292	-.6619E+01
23.2379	4.7292	-.6106E+01
23.9225	4.7292	-.5232E+01
24.6072	4.7292	-.3320E+01
25.2918	4.7292	-.1580E+01
25.9764	4.7292	-.1690E+01
22.0842	6.7864	-.7726E+01
22.6316	6.7864	-.7411E+01
23.1790	6.7864	-.7413E+01
23.7264	6.7864	-.7622E+01
24.2738	6.7864	-.6536E+01
24.8212	6.7864	-.5274E+01
25.3686	6.7864	-.3738E+01
25.9161	6.7864	-.5830E+01
26.4635	6.7864	-.5493E+01
27.0109	6.7864	-.4992E+01
24.3470	8.8377	-.8114E+01
24.7576	8.8377	-.7644E+01
25.1682	8.8377	-.7194E+01
25.5788	8.8377	-.7338E+01
25.9894	8.8377	-.7225E+01
26.4000	8.8377	-.7030E+01
26.8106	8.8377	-.6858E+01
27.2211	8.8377	-.6445E+01
27.6317	8.8377	-.6155E+01
28.0423	8.8377	-.6022E+01
26.5931	10.8738	-.6219E+01
26.8679	10.8738	-.6290E+01
27.1427	10.8738	-.6777E+01
27.4175	10.8738	-.7032E+01
27.6923	10.8738	-.7029E+01
27.9671	10.8738	-.7021E+01

PRESSURE AT CONTROL POINT - X		Y		LOWER SURFACE PRESSURE	
28.2418	10.8738	-	.6945E+01		
28.5166	10.8738	-	.6861E+01		
28.7914	10.8738	-	.6849E+01		
29.0662	10.8738	-	.6913E+01		
17.5422	2.6691		.8561E+01		
18.3642	2.6691		.6094E+01		
19.1862	2.6691		.5306E+01		
20.0083	2.6691		.4765E+01		
20.8303	2.6691		.3756E+01		
21.6523	2.6691		.3248E+01		
22.4744	2.6691		.3036E+01		
23.2964	2.6691		.2454E+01		
24.1184	2.6691		.2455E+01		
24.9404	2.6691		.2225E+01		
19.8148	4.7292		.6861E+01		
20.4994	4.7292		.6479E+01		
21.1841	4.7292		.6212E+01		
21.8687	4.7292		.5622E+01		
22.5533	4.7292		.4542E+01		
23.2379	4.7292		.3891E+01		
23.9225	4.7292		.3273E+01		
24.6072	4.7292		.4132E+01		
25.2918	4.7292		.5223E+01		
25.9764	4.7292		.4650E+01		
22.0842	6.7864		.4549E+01		
22.6316	6.7864		.4974E+01		
23.1790	6.7864		.5161E+01		
23.7264	6.7864		.5213E+01		
24.2738	6.7864		.6519E+01		
24.8212	6.7864		.7748E+01		
25.3686	6.7864		.6647E+01		
25.9161	6.7864		.5697E+01		
26.4635	6.7864		.5096E+01		
27.0109	6.7864		.4638E+01		
27.5583	8.8377		.3775E+01		
28.1057	8.8377		.4270E+01		
28.6531	8.8377		.4773E+01		
29.1999	8.8377		.4687E+01		
29.7467	8.8377		.4878E+01		
30.2935	8.8377		.5179E+01		
30.8403	8.8377		.5480E+01		
31.3871	8.8377		.6040E+01		
31.9339	8.8377		.6646E+01		
32.4807	8.8377		.6650E+01		
33.0275	10.8738		.5447E+01		
33.5743	10.8738		.5384E+01		
34.1211	10.8738		.4917E+01		
34.6679	10.8738		.4866E+01		
35.2147	10.8738		.4713E+01		
35.7615	10.8738		.4745E+01		
36.3083	10.8738		.4849E+01		
36.8551	10.8738		.4966E+01		
37.4019	10.8738		.5013E+01		
37.9487	10.8738		.4989E+01		

AERODYNAMIC PRESSURE ON THE WING -- CENTROID OF FINITE ELEMENT AS GENERATED BY NSWC CODE IN THE
SAME LOCAL COORDINATE SYSTEM

TOTAL NUMBER OF WINGS 1

WING NO. 1

PRESSURE LOAD ON THE UPPER SURFACE OF WING

ELEMENT	X	Y	PRESSURE	ELEMENT	X	Y	PRESSURE
500	.178E+02	-.267E+01	-.747E+01	501	.200E+02	-.473E+01	-.658E+01
502	.222E+02	-.679E+01	-.762E+01	503	.245E+02	-.84E+01	-.799E+01
504	.267E+02	-.109E+02	-.621E+01	515	.240E+02	-.267E+01	-.528E+01
516	.252E+02	-.473E+01	-.181E+01	517	.264E+02	-.679E+01	-.558E+01
518	.275E+02	-.884E+01	-.620E+01	519	.287E+02	-.109E+02	-.684E+01

PRESSURE LOAD ON THE LOWER SURFACE OF WING

ELEMENT	X	Y	PRESSURE	ELEMENT	X	Y	PRESSURE
525	.178E+02	-.267E+01	-.804E+01	526	.200E+02	-.473E+01	-.673E+01
527	.222E+02	-.679E+01	-.644E+01	528	.245E+02	-.84E+01	-.390E+01
529	.267E+02	-.109E+02	-.546E+01	540	.240E+02	-.267E+01	-.245E+01
541	.252E+02	-.473E+01	-.511E+01	542	.264E+02	-.679E+01	-.520E+01
543	.275E+02	-.884E+01	-.640E+01	544	.287E+02	-.109E+02	-.501E+01

.....END OF COMPUTATIONS

Section 5

CONCLUSIONS AND RECOMMENDATIONS

The MDAC aerodynamic code has been modified extensively to provide pressure loads on a missile or its components at the centroid of finite elements as specified. The input preparation has been greatly simplified to reduce the effort necessary. In particular, wing parameters such as camber, thickness slope and twist are generated automatically from the wing surface description. Body panel slopes are generated from input by spline interpolation from given profiles. Coordinate systems for the description of finite elements for both body and wing can be different from that used for aerodynamic calculations. Outputs are produced as computer printout and punched cards in the format of NASTRAN bulk data.

The computer program as developed thus provides a unique link between the aerodynamic analysis of a missile at subsonic or supersonic speed and the analysis of its structural response under the aerodynamic load. It reduces considerably the effort required for generating the pressure load at the desired position when used in combination with the NSWC computer code PING or BING. It may be used for analyzing either the component such as wing, body or tail or the complete missile as the situation demands.

The computer code as developed represents a versatile tool for missile analysis. Nevertheless, its range of utilization can be extended with additional effort. It is recommended that the following tasks be considered for future development.

- Interpolation of experimental data for structural analysis: When the measured pressure distributions over a given missile are available from experiment, it is suggested that the present code be used to interpolate the pressure loads and generate the loading at specified centroids of finite elements as input to NASTRAN for analysis. This can be accomplished by incorporating additional

capabilities for inputting test data, performing coordinate transform, interpolating the pressure and generating loads at centroids of elements in punch card form.

- **Missile attitude generalization:** The present MDAC aero code calculates the aerodynamic loads and missile with a restriction on its attitude. Only the angle of attack given in the pitch plane is considered at the present. For missile attitudes expressed in terms of roll and yaw, modification of the code will be necessary. This addition will in many ways expand the utilization of the code for practical cases of structural analysis of a missile at various attitudes during its flight.
- **Aerodynamic loads at high supersonic speed:** With the continuing changes in systems requirements as well as improvements in missile technology, the cruising speed of missiles may well be in the high supersonic range of operation. Based on the linear theory the present MDAC aero code is limited to low supersonic speeds ($M_\infty \leq 2.5$). For realistic structural analysis of missiles at high supersonic speeds appropriate methods are available for calculating the aerodynamic loads. In view of the current needs of NSWC, it is felt that relatively exact methods (finite difference or method of characteristics) may not be satisfactory in terms of computational effort required. It is suggested that a combination of methods (e. g., second order shock expansion, tangent cone and wedge and Newtonian impact, etc.) be used for analyzing and computing the aerodynamic loads on a missile at high supersonic speed. In References 9 through 12 the above methods are described in some detail and their applications and limitations are discussed.

Section 6
REFERENCES

1. R. H. MacNeal (Editor). The NASTRAN User's Manual, NASA SP-221(01), 1972.
2. H. Ashley and W. P. Rodden. Wing-Body Aerodynamic Interaction. Annual Review of Fluid Mechanics, 1972, Vol 4, P 431-472.
3. F. A. Woodward. Analysis and Design of Wing-Body Combinations at Subsonic and Supersonic Speeds. Journal of Aircraft, 1968, Vol 5, No. 6, P 528-534.
4. P. C. Huang and J. P. Matra, Jr. Planform Input Generating (PING), A NASTRAN Preprocessor for Lifting Surface-Theoretical Development, User's Manual, and Program Listing. NOLTR-73-199, Naval Ordnance Laboratory, White Oak, Silver Spring, Maryland, December 1973.
5. P. C. Huang and J. P. Matra, Jr. Missile Body Input Generator (BING), A NASTRAN Preprocessor; Theoretical Development, User's Manual, and Program Listing. NSWC-NOL-TR-75-9, Naval Surface Weapons Center, White Oak, Silver Spring, Maryland, March 1975.
6. R. L. Harder and R. N. Desmarais. Interpolation Using Surface Splines. Journal of Aircraft, 1972, Vol 9. No. 2, P 189-191.
7. H. W. Carlson. Pressure Distributions at Mach Number 2.05 on a Series of Highly Swept Arrow Wings Employing Various Degrees of Twist and Camber. NASA TN D-1264, Langley Research Center, Langley Station, Hampton, Virginia, May 1962.
8. Gapcynski, John P. and G. J. Landrum. Tabulated Data for a Pressure Distribution Investigation at Mach Number 2.01 of a 45° Sweptback-Wing Airplane Model at Combined Angles of Attack and Sideslip. NASA memo 10-15-58L, November 1958, Langley Research Center, Langley Field, Virginia.
9. Hayes, W. D. and R. F. Probstein. Hypersonic Flow Theory, Vol 1, Inviscid Flows, Second Edition (1966). Academic Press, New York.
10. Savin, R. C. Application of the Generalized Shock-Expansion Method to Include Bodies of Revolution Traveling at High Supersonic Speeds, NACA TN 3345, April 1955.
11. Syvertson, C. A. and D. H. Dennis. A Second-Order Shock-Expansion Method Applicable to Bodies of Revolution Near Zero Lift. NACA Report 1328, 1957.
12. Van Dyke, M. D. Second-Order Slender-Body Theory-Axisymmetric Flow. NASA TR R-47, 1959.

Appendix A
PROGRAM LISTING



PRECEDING PAGE NOT FILMED
BLANK


```

CDECK WOODWARD
OVERLAY(WOOD,0,0)
PROGRAM WOODWARD(INPUT=200,OUTPUT=200,TAPE5=INPUT,TAPE6=OUTPUT,
1 TAPE1=200,TAPE2=100,TAPE3=200,TAPE4=100,TAPE8=100,
2 TAPE9=100,TAPE11=200,TAPE12,PUNCH=200)
***** SUBSONIC / SUPERSONIC INFLUENCE COEFFICIENT PROGRAM *****
***** AERODYNAMIC COMPUTER CODE FOR ANALYSIS OF MISSILE WING,
***** BODY, OR COMBINATIONS. IT IS BASED ON THE WOODWARD
***** PROGRAM DEVELOPED FOR COMPUTING THE PRESSURE LOADS ON
***** MISSILE. IT READS IN THE GEOMETRY OF MISSILE COMPONENTS
***** AND THE FINITE ELEMENT DESCRIPTION FROM NSVC'S PING OR
***** BING AS INPUT, COMPUTES PRESSURE LOAD AND INTERPOLATES,
***** USING SURFACE FIT, FOR PRESSURE ON THE CENTROID OF EACH
***** ELEMENT. FOR INFORMATION CONTACT KENNETH K. WANG
***** MCDONNELL-DOUGLAS
***** HUNTINGTON BEACH, CA. WOOD1070
*****
COMMON / MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NEODY, NWING, XMACH,
1 SYM, KACE, NPOLAR, IFX
COMMON / BODYSP / DRDX(51), DZDX(51)
COMMON / INPUT T / LIN
COMMON / DSX5 / XS1, XS2, DS1, DS2
COMMON / TRANS / IOWR10, IOWR60, IOWR70
COMMON / ENDJOB / JOSEND
COMMON / CORTN / NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)

INITIALIZE
LA=1
LB=2
LC=3
LD=4
LE=5
LF=6
LI=7
LN=11
REXIND1
REXIND2
REXIND3
REXIND4
REXIND8
REXIND9
REXIND11

READ IN CASE SPECIFICATIONS
CALL OVERLAY(4HWANG, 2, 0)
NPOLAR = 0
IRW = 0 , DATA ARE NOT SAVED ON TAPE
IRW = 1 , DATA ARE SAVED ON TAPE 12 FOR RESTART
IRW = 2 , RESTART RUN, BYPASS ALL AERO CALCULATIONS
IF ( IRW -LT. 2 ) GO TO 100
CALL OVERLAY(4HWANG, 7, 0)
GO TO 1100
100 CONTINUE

```

WOOD1000
WOOD1010
WOOD1020
WOOD1030
WOOD1040

WOOD1120
WOOD1130

WOOD1140
WOOD1150
WOOD1160

WOOD1290
WOOD1300
WOOD1310
WOOD1320
WOOD1330
WOOD1340
WOOD1350
WOOD1360
WOOD1370
WOOD1380
WOOD1390
WOOD1400
WOOD1410
WOOD1420
WOOD1430
WOOD1440
WOOD1450

AD-A048 840

MCDONNELL DOUGLAS ASTRONAUTICS CO HUNTINGTON BEACH CALIF F/G 1/1
AERODYNAMIC COMPUTER CODE FOR COMPUTING PRESSURE LOADING ON COM--ETC(U)
JAN 78 K K WANG
MDC-67215

UNCLASSIFIED

NL

2 OF 3

ADA048840




```

C      IOVR70 = 4
C      CALL OVERLAY(4HWANG, 7, 0, 6HRECALL )
C
C      GO TO 3000
C
C      BODY ALONE, KACE = 2
C      1070 CONTINUE
C      GO TO 3000
C
C      WING - BODY COMBINATION, KACE = 3
C      2000 CONTINUE
C      IOVR70 = 2
C      CALL OVERLAY(4HWANG, 7, 0, 6HRECALL )
C      CALL OVERLAY(4HWOOD, 4, 0, 6HRECALL )
C
C      IOVR70 = 3
C      CALL OVERLAY(4HWANG, 7, 0, 6HRECALL )
C      CALL OVERLAY(4HWOOD, 5, 0, 6HRECALL )
C
C      IOVR70 = 4
C      CALL OVERLAY(4HWANG, 7, 0, 6HRECALL )
C
C      3000 CONTINUE
C      IOVR60 = 1
C      CALL OVERLAY(4HWOOD, 6, 0, 6HRECALL )
C
C      IOVR70 = 0
C      CALL OVERLAY(4HWANG, 7, 0, 6HRECALL )

```

AER01760
AER01770
AER01780
AER01790

```

C      END
C      SUBROUTINE FOR EOF (IT)
C
C      ..... WRITES E.F. ON A TAPE TO INDICATE THE END OF A DATA SET .....
C
C      INTEGER EOF
C      DATA EOF /4HE.F./
C
C      WRITE (IT) EOF
C
C      RETURN
C
C      END
C
C      SUBROUTINE FSF (NF, NTAPE, IRR)
C
C      ..... READS A TAPE UNTIL IT HAS READ THE CHARACTERS E.F. ....
C
C      INTEGER TW
C      INTEGER EOF
C      DATA EOF /4HE.F./

```

FORE1000
FORE1010
FORE1020
FORE1030
FORE1040
FORE1050
FORE1060
FORE1070
FORE1080
FORE1090
FORE1100
FORE1110
FORE1120
FORE1130
FORE1140

FSF 1000
FSF 1010
FSF 1020
FSF 1030
FSF 1040
FSF 1050
FSF 1060
FSF 1070
FSF 1080
FSF 1090

```

C
IRR = 0
K = 0
DO 1000 I = 1, 10000
  RE/>(NTAPE) TW
  IF (TW - NE. EOF) GO TO 1000
  K = K + 1
  IF (K .GE. NF) RETURN
1000 CONTINUE
  IRR = NF - K
C -----
C RETURN
C -----
C END
CDECK FUNCTION INTURP(IDIC,NDIC,LI,LO)
C .....
C READ AND WRITE A COMMAND CARD,SEE IF COMMAND (IN THE
C FIRST WORD) IS IN THE DICTIONARY.
C .....
C INTEGER IDIC(1), COM(20), ICOM
C EQUIVALENCE (COM(1),ICOM)
C
C IDIC (INSTEAD OF DIC) IS USED AS AN ARGUMENT
C SO THAT A FIXED-POINT COMPARISON CAN BE MADE
C
C READ (LI,1040)COM
C IF (LO)1010,1010,1000
1000 WRITE (LO,1050)COM
1010 DO 1020 INTERP=1,NDIC
  IF (IDIC(INTERP) .EQ. ICOM) GO TO 1030
1020 CONTINUE
C
  INTERP=0
1030 INTURP=INTERP
C -----
C RETURN
C -----
C 1040 FORMAT(20A4)
1050 FORMAT(11H0,20A4)
CDECK,CGOP
OVERLAY(WOOD,1,0)
PROGRAM CGOP
COMMON/ MAIN / LA,NTAPEB,NTAPEEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1 NTAPED,NEODY,NWING,XMACH,SYM,KACE,NPOLAR,IRW
COMMON /TRANSFR/ IOVR10,IOVR60,IOVR70
200 CALL PANEL
C
END
CDECK PANEL
SUBROUTINE PANEL
C
COMMON/ MAIN / LA,NTAPEB,NTAPEEC,NTAPED,LE,LF,LI,LO,NEODY,NWING,
1 XMACH,SYM,KACE,NPOLAR,IRW
COMMON /XWING/ XH(13,11),YH(11),ZH(11)
COMMON/DSX5 / XES1,XES2,XSB1,DSB2
DIMENSION XB(51),RB(51),ZD(51),THETA(11),X(51),Y(11),Z(11),BC(10),

```

```

FSF 1100
FSF 1110
FSF 1120
FSF 1130
FSF 1140
FSF 1150
FSF 1160
FSF 1170
FSF 1180
FSF 1190
FSF 1200
FSF 1210
FSF 1220
FSF 1230
INTU1000
INTU1010
INTU1020
INTU1030
INTU1040
INTU1050
INTU1060
INTU1070
INTU1080
00000100
INTU1100
INTU1110
INTU1120
INTU1130
INTU1140
INTU1150
INTU1160
INTU1170
INTU1180
INTU1190
INTU1200
INTU1210
INTU1220
INTU1230
INTU1240
INTU1250
INTU1260
INTU1270
INTU1280

```

```

1 XBAR(50), YBAR(10), ZBAR(10), XC(50), THET(11), CHORD(50), AREA(50,10),
2 KX(10), ZER(110,10), XER(110,10), YBR(110,10), CN(110,10), THETW(10),
3 ARX(110,10), XCN(110,10)

```

```

C
REWIND NTAPEC
XCPT = 0.95
I=1
Z0=0.
ON=1.

```

```

10 IF ( NBODY ) 100, 100, 10
   READ (LI,1010) BODYS, BTHET, PLANE, RP
   NEDYS=BODYS
   NTHET=BTHET
   NPLANE=PLANE

```

```

   NXLE=0
   READ (LI,1010) ( XB(N), N=1,NBODYS)
   READ (LI,1010) ( RB(N), N=1,NBODYS)
   READ (LI,1010) ( ZD(N), N=1,NBODYS)
   READ (LI,1010) ( THETA(N), N=1,NTHET )
   READ (LI,1010) XBS1, XBS2, DSB1, DSB2

```

```

DO 15 N=1,NTHET
15 THETA(N)=THETA(N)/57.2957795
   IF (PLANE) 300,300,20

```

```

C
C
C BODY-WING CASE, REQUIRES PANELED BODY

```

```

20 CONTINUE
   READ (LI,1010) ( X(N), N=1,NPLANE)
   ALPHA=0
   NPLN1=NPLANE-1
   NROW=NTHET-1
   IF (RP) 22,22,28

```

```

C
C
C NON-CIRCULAR BODY

```

```

22 CONTINUE
   READ (LI,1010) ( Y(N), N=1,NTHET)
   READ (LI,1010) ( Z(N), N=1,NTHET)
   GO TO 35

```

```

C
C
C CIRCULAR BODY

```

```

28 DO 30 N=1,NTHET
   Y(N)=RP*SIN(THETA(N))
30 Z(N)=RP*COS(THETA(N))
35 DO 40 N=1,NROW
   YEAR(N)=(Y(N)+Y(N+1))/2.
   ZBAR(N)=(Z(N)+Z(N+1))/2.
40 BC(N)=SQR((Y(N+1)-Y(N))*2+(Z(N+1)-Z(N))*2)
   DO 50 N=1,NPLN1
   XBAR(N)=(X(N+1)+X(N))/2.
   CHORD(N)=X(N+1)-X(N)
50 XC(N)=X(N)+XCPT*CHORD(N)
   DO 60 N=1,NROW
60 THEI(N)=ATAN2((Z(N+1)-Z(N)),(Y(N+1)-Y(N)))
   WRITE(LO,900)
   WRITE(LO,910)
   NP=0

```

```

DO 70 N=1,NROW
DO 70 N=1,NPLN1
NP=NP+1
WRITE(LO,920) NP, X(M), Y(N), Z(N), X(M), Y(N+1), Z(N+1),
1 X(N+1), Y(N), Z(N), X(N+1), Z(N+1)
70 WRITE (NTAPE) NP, X(M), Y(N), Z(N), X(M), Y(N+1), Z(N+1),
1 X(N+1), Y(N), Z(N), X(N+1), Z(N+1)

```



```

WRITE(LO,940)
WRITE(LO,950)
NP=0
DO 80 N=1,NROW
DO 80 M=1,NPLN1
NP=NP+1
AREA(N)=CHORD(M)*BC(N)
WRITE(LO,960) NP,XEAR(M),YBAR(N),ZBAR(N),XC(M),YBAR(N),ZBAR(N),
1AREAM(N),THET(N),ZO,CHORD(M)
80 WRITE(NTAPEC) NP,XEAR(M),YBAR(N),ZBAR(N),XC(M),YBAR(N),ZBAR(N),
1AREAM(N),THET(N),ZO,CHORD(M)
WRITE(NTAPEC) NPLN1,XCPT
NEODY=NP
IF(NWING)500,500,120
100 IF(NWING)500,500,110
C
C      BODY ONLY OR BODY-WING CASE
C
110 CONTINUE
NEODY=0
PLANE=0.
120 NP=0
WRITE(LO,970)
WRITE(LO,980)
DO 200 L=1,NWING
CALL WINGP(NB,NC,YO,ZA,DIH)
THETW(L)=DIH
WRITE(LO,1020) L,YO,ZA,DIH
NB1=NB-1
NC1=NC-1
KW(L)=NB1*NC1
DO 150 N=1,NB1
DO 150 M=1,NC1
NP=NP+1
WRITE(NTAPEC) NP,I,XW(M,N),YW(N),ZW(N),XW(M,N+1),YW(N+1),ZW(N+1),
1XW(M+1,N),YW(N),ZW(N),XW(M+1,N+1),YW(N+1),ZW(N+1),
WRITE(LO,920) NP,I,XW(M,N),YW(N),ZW(N),XW(M,N+1),YW(N+1),ZW(N+1),
1XW(M+1,N),YW(N),ZW(N),XW(M+1,N+1),YW(N+1),ZW(N+1),
K=N*(N-1)*NC1
CR=XW(M+1,N)-XW(M,N)
CT=XW(M+1,N+1)-XW(M,N+1)
RY=(1.+CT/(CR-CT))/5.0
RY1=1.0-RY
XWL=RY*XW(M,N+1)+RY1*XW(M,N)
XWT=RY*XW(M+1,N+1)+RY1*XW(M+1,N)
CW(K,L)=XWT-XWL
YDUM=SQRT((YW(N+1)-YW(N))**2+(ZW(N+1)-ZW(N))**2)
ARW(K,L)=YDUM*.5*(CR+CT)
XER(K,L)=(XWL+XWT)/2.
YER(K,L)=(YW(N+1)+RY+YW(N)+RY1
ZER(K,L)=ZW(N+1)+RY+ZW(N)+RY1
XCW(K,L)=XCPT+XWT*(1.0-XCPT)*XWL
150 CONTINUE
WRITE(LO,990)
WRITE(LO,1000)
NP=0
DO 250 L=1,NWING
KL=XW(L)
DO 250 K=1,KL
NP=NP+1
WRITE(LO,960) NP,XER(K,L),YER(K,L),ZER(K,L),XCW(K,L),YBR(K,L),
1ZER(K,L),ARW(K,L),THETW(L),ZO,CW(K,L)
250 WRITE(NTAPEC) NP,XER(K,L),YER(K,L),ZER(K,L),XCW(K,L),YBR(K,L),
1ZER(K,L),ARW(K,L),THETW(L),ZO,CW(K,L)
NWIN=NP

```

```

WRITE (NTAPEC) NC1, XCPT *
IF (PLANE.GT.0.) WRITE(NTAPEC) NTHET
IF (PLANE.GT.0.) WRITE(NTAPEC) (THETA(N), N=1, NTHET)
1 (PLANE) 500,500,400
300 NEDDY=-1
REWIND NTAPED
WRITE(NTAPEB) NDUM,NDUM,NDUM,NTHET
WRITE(NTAPEB) (THETA(N), N=1, NTHET)
REWIND NTAPED
400
REWIND NTAPED
WRITE (NTAPEB) ON,ON,ZO,ZA,DSB1,DSB2
WRITE (NTAPEB) NBODY$ ,NILE
WRITE (NTAPEB) (XB(N),RB(N),ZD(N),N=1,NBODYS)
500
REWIND NTAPED
NPAPEL=NWING*NBODY
RETURN
900 FORMAT (1H1,9X,'BODY PANEL CORNER POINT LOCATIONS EXPRESSED IN *,
A
186H1 AND 2 INDICATE BODY PANEL LEADING-EDGE POINTS, 3 AND 4 INDICA
2TE TRAILING-EDGE POINTS)
910 FORMAT (1H0,5X,5HPANEL, 4(8X,1HX,8X,1HY,8X,1HZ)/
15X,2HNO,2X,5HPARTS,6X,
2 3(1H1,8X),3(1H2,8X),3(1H3,8X),3(1H4,8X)/)
920 FORMAT (1H 3X,13,3X,11,3X,12F9.5)
930 FORMAT (1H 13X,12F9.5)
940 FORMAT (1H1,9X,'BODY PANEL CENTROID AND CONTROL POINT LOCATIONS*,
1
= EXPRESSED IN THE AERO COORDINATE SYSTEM*)
950 FORMAT (1H0,5HPANEL,6X,2(1HX,8X,1HY,8X,1HZ,8X),5X,4HAREA,9X,
16HTHETA-2X,6HALPHA-5X,5HCHORD/13X,3(1HC,8X),3(2HCP,7X),
21X,6HINCIN,5X,5HINCID//)
960 FORMAT (1H 1X,13,3X,11,3X,12F9.5)
970 FORMAT (1H1,9X,'WING PANEL CORNER POINT LOCATIONS EXPRESSED IN *,
A
186H1 AND 2 INDICATE WING PANEL LEADING-EDGE POINTS, 3 AND 4 INDICA
2TE TRAILING-EDGE POINTS)
980 FORMAT (1H0,5X,5HPANEL, 4(8X,1HX,8X,1HY,8X,1HZ)/
15X,2HNO,2X,5HPARTS,6X,
2 3(1H1,8X),3(1H2,8X),3(1H3,8X),3(1H4,8X)/)
990 FORMAT (1H1,9X,'WING PANEL CENTROID AND CONTROL POINT LOCATIONS*,
A
=EXPRESSED IN THE AERO COORDINATE SYSTEM*)
1000 FORMAT (1H0,1X,5HPANEL,6X,2(1HX,8X,1HY,8X,1HZ,8X),5X,4HAREA,12X,
16HTHETA-2X,6HALPHA-5X,5HCHORD/14X,3(1HC,8X),3(2HCP,7X),
220X,5HSHED,4X,6HCAMBER,4X//)
1010 FORMAT(7F10.0)
1020 FORMAT(1H0,4X,9HWING NO.,12,5X,9H YPIVOT =,F10.3,5X,9H ZPIVOT =,
1F10.3,5X,16H WING DIBEDRAL =,F10.3,1X,7HRADIANS,1X//)
END
CDECK
WINGP
SUBROUTINE WINGP(NB,NC,YO,ZA,DIH)
COMMON/MAIN / LA,NTAPEB,NTAPEC,NTAPEB,LE,LI,LI,LO,NBODY,NWING,
1 XWACH,SYM,KACE,NPOLAR,IRW
COMMON /XYWING/ XY(13,11),YW(11),ZW(11)
DIMENSION XW(12),DY(11)
READ (LI,1010) X0,Y0,CR,A,B,C
READ (LI,1010) XNB,XNC,CASE,ZA
NB=XNB
NC=XNC
NCA=CASE
PERCT = 0.1
CRR = CR - X0
DCR = (1.0 - PERCT) * CRR / (XNC - 2.0)
XW(1)=X0
XW(2) = XW(1) + PERCT* CRR

```

C

```

DO 145 M=3,NC
  XM(M) = XM(M-1) + DCR
145 CONTINUE
  BY = B - YO
  DBY=BY/(XNB-1.)
  YM(1)=YO
  DO 165 N=2,NB
    YM(N) = YM(N-1) + DBY
165 CONTINUE
  SLE=(A-XO)/(B-YO)
  STE=(C-CR)/(B-YO)
  IF(SLE-STE)210,230,210
210 CONTINUE
  DX = (C-A) / (CR - XO)
  DO 215 N=1,NC
    XY(N,NB) = A + DX*( XM(M) - XO )
215 CONTINUE
  DO 220 N=1,NB
    NY(N)=(YM(N)-YO)/(B-YO)
  DO 220 M=1,NC
    XY(M,N) = XM(M) + ( XY(M,NB) - XM(M) ) * DY(N)
220 CONTINUE
  GO TO 250
230 DO 240 N=1,NB
  DO 240 M=1,NC
    DY(N)=YM(N)-YO
  DO 240 M=1,NC
    XY(M,N) = XM(M) + SLE*DY(N)
240 CONTINUE
250 CONTINUE
  CALL WROTAT(NB,YO,ZA,DIH)
  RETURN
1010 FORMAT(7F10.0)

CDECK WROTAT
SUBROUTINE WROTAT(NB,YO,ZA,WNGDIH)
COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, MWING, XMACH,
1 SYM, KACE, NPOLAR, IRW
COMMON /XYWING/ XY(13,11),YW(11),ZW(11)
DIMENSION DYPIVT(11)
WNGDIH=0.
READ (11,1020) PIVOT, WNGDIH
YPIVT=YO
ZPIVT=ZA
C PIVOT, DIHEDRAL INDICATOR
C YPIVT, ZPIVT, PIVOT POINT
C WNGDIH, DIHEDRAL ANGLE
DO 50 I=1,NB
50 ZW(I)=ZA
IF(PIVT.EQ.0.0)RETURN
DO 100 I=1,NB
DYPIVT(I)=YW(I)-YPIVT
100 CONTINUE
WNGDIH=WNGDIH/57.2957795
COSDIH=COS(WNGDIH)
SINDIH=SIN(WNGDIH)
DO 200 I=1,NB
YW(I)=YPIVT+COSDIH*DYPIVT(I)
ZW(I)=ZPIVT+SINDIH*DYPIVT(I)
200 CONTINUE
1020 FORMAT (7F10.4)
RETURN
END
CDECK,PRELIM
OVERLAY (NANG,2,0)
PROGRAM PRELIM

```



```

C C C C
      READ INPUT, WRITE ON TAPE 11 FOR SUBSEQUENT COMPUTATION
COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, NHING, XMACHN,
1  SYMM, KACE, NPOLAR, IPN
COMMON/ BODYSP/ DRDX(51) DZDX(51)
COMMON/DEFAU / BODY, BODYS, BTHET, CPCALC, UCASE, NRUN, DADEG, ARB,
1  PLANE, POLAR, RP, XNACEL, SYM, THICK, WING, XMACH,
2  XNEB, XNCC, PINF, IPUNCH, SID(20), CKASE, ARM
COMMON/ BODY2 / NEFL, NEODYS, NTHET, XB(51), RB(51), ZD(51),
1  THETA(11), RPP, XSPANL(20)
COMMON/ NACEL / NACELP, XN(51,2), RN(51,2), ZN(51,2), ARN(2)
COMMON/ CORTN/ NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
COMMON/ INPUT / TX(4, 100)
COMMON/ POINTP/ TY(6), TYP(4), TYP(4)
COMMON/ POINTS / NPTS, NVAR
COMMON/ WINGFM/ XHI(30,20), YHI(30,20), ZHI(30,20), NWPI(20), NCHORD,
1  NSPAN, ISOLID, NPLANE, ICAMBR, ITWIST, ITTHICK, IFORM(10)
2  PIVOT(10), DIHED(10)
INTEGER TITLE(20)
DIMENSION NEC(2, 6)
DATA NEC / 4, 9, 4, 6, 3, 7, 3, 6, 3, 4, 2, 5 /
C
NAMELIST/ UNIFID / ICASE, NTRANS, IPUNCH, IRW, POLAR, ISOLID, SID,
1  NEPFL, XB, RB, ZD, RP, NWPI,
2  NHING, IFORM, PIVOT, THICK, DIHED, XWI, YWI, ZWI,
3  XNACEL, NACELP, XN, RN, ZN,
4  XMACH, PINF, DADEG, ARB, ARW, ARM
C C C C
      READ IN DESCRIPTIVE TITLE
READ (5,1000) TITLE
WRITE (6,1010) TITLE
C C C C
      SET DEFAULT VALUES
CALL DEFAULT
C C C C
      READ NAMELIST INPUT FOR UNIFIED COMPUTER CODE
READ (5, UNIFID )
WRITE (6, UNIFID )
C
NSTR = NHING - 2
IF ( NHING .LE. 2 ) GO TO 30
XNEB = FLOAT( NEC(1, NSTR) )
XNCC = FLOAT( NEC(2, NSTR) )
CONTINUE
XNE = XNEB
XNC = XNCC
NB = XNEB
NC = XNC
NEODY = 0
NCHORD = NC
NSPAN = NB
30
C C C C
      FIRST RUN IRW .LT. 2
      RESTART RUN IRW = 2
C C C C
      IF ( IRW .EQ. 2 ) GO TO 500
C C C C
      READ IN COORDINATE SYSTEM SPECIFICATION FOR BODY AND WING AND
      COMPUTE TRANSFORMATION MATRICES.

```

```

C      IF ( ICASE .NE. 1 ) NBODY = 1
      ANACEL = ABS( XNACEL )
      NACELS = IFIX(ANACEL)
      NW2 = 0
      IF ( ICASE .EQ. 2 ) GO TO 45
      DO 40 I=1,NWING
      NCORD = 1
      IF ( IFORM(I) .EQ. 1 ) NCORD = 2
      NW2 = NW2 + NCORD
40    CONTINUE
45    CONTINUE
      NS = NBODY + NW2 + NACELS
      DO 50 I=1,NS
      NSYM = I
      CALL CORDTR
50    CONTINUE
      IF ( ICASE .EQ. 2 ) GO TO 70
      TRANSFORM WING COORDINATES TO THAT OF AERO
      NSYM = NBODY
      DO 60 I = 1,NWING
      NSYM = NSYM + 1
      NW = 2 * I - 1
      CALL WTRANS( NW, I )
      CALL CORTAN( NW, I )
      IF ( IFORM(I) .NE. 1 ) GO TO 60
      NSYM = NSYM + 1
      NW = NW + 1
      CALL WTRANS( NW, I )
      CALL CORTAN( NW, I )
60    CONTINUE
      IF ( NACELS .EQ. 0 ) GO TO 70
      TRANSFORM THE NACEL AXIS XN TO THAT OF THE BODY AXIS
      DO 51 K = 1, NACELS
      NSYM = 1 + NW2 + K
      NT = NTRANS( NSYM )
      DO 51 ITRAN = 1, NT
      DO 51 J = 1, NACELP
      XN(J) = XN(J) + VA( 1, ITRAN, NSYM )
51    CONTINUE
70    CONTINUE
      PREPARE INPUTS AND WRITE ON TAPE 11 FOR AERO CODE
      ICASE = 1, WING ONLY
      ICASE = 2, BODY ONLY
      ICASE = 3, COMPLETE MISSILE
      GO TO ( 100, 200, 300 ), ICASE
      WING ONLY CASE
100  CONTINUE
      KACE = 1
      CALL WINGIN
      GO TO 500
200  CONTINUE

```

```

C
C
C      BODY ONLY CASE
      KACE = 2
      NBODY = 1
      XNACEL = 0.0
      NHING = 0.0
      PLANE = 0.0
      CALL BODYIN
      GO TO 500

C
C      300 CONTINUE
      COMPLETE MISSILE CASE
C
C
C      KACE = 3
      CALL BANWIN
C
C      500 CONTINUE
C
C      1000 FORMAT(20A4)
      1010 FORMAT(1H1,20A4)
      1020 FORMAT(7F10.0)
C
C
C      END
CDECK, BODYPN
      SUBROUTINE BODYPN
C
C
C
C      PANEL BODY SECTION TO CORRESPONDING WITH THE WING PANEL FOR
      AERODYNAMIC COMPUTATIONS
      COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, NHING, XMACH,
      1 SYM, KACE, NPOLAR, IRW
      1 COMMON/ BODY2 / NEPEL, NBOBYS, NTHET, XB(51), RB(51), ZD(51),
      1 THETA(11), RP, XN(20)
      COMMON/CORTRN/ NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
      COMMON/DEFAU / BODY, BODYS, BTHT, CPCALC, WCASE, NRUN, DADG, ARB
      1 PLANE, POLAR, RPP, XNACEL, SYMM, THICK, WING, XMACHH, XNB
      2 XNC, PINE, IPUNCH, CBASE, ARW
      COMMON/WINGFM/ XWI(30,20), YWI(30,20), ZWI(30,20), NWPI(20), NCHORD,
      1 NSPAN, ISOLID, NPLANE, ICAMBR, ITWIST, ITHICK, IFORM(10)
      2 , PIVOT(10), DIH(10)
      PERCT = 0.1
      NC = XNC
C
C
C      DETERMINE BODY PANEL RADIUS RP
      YMIN = YWI( 1,1)
      NW2 = 2 * NHING
      XMIN = XWI( 1,1)
      XMAX = XWI( 2,1)
      IF ( NHING .EQ. 1 ) GO TO 305
      DO 200 I=1,NW2,2
      YMIN = AMIN1( YWI(1,1), YMIN )
      200 CONTINUE
C
      DO 300 I=1,NW2,2
      XMIN = AMIN1( XWI(1,1), XMIN )
      XMAX = AMAX1( XWI(2,1), XMAX )
      300 CONTINUE
C

```



```

ICAMER = 1
TX(3,1) = ZD(1)
100 CONTINUE
C
NVAR = 3
IF ( ICAMER .EQ. 0 ) NVAR = 2
CALL SPLIT
C
FOR IMPROVED ACCURACY, FIRST 20 PERCENT OF BODY IS DIVIDED INTO
10 EQUAL SECTIONS, THE REMAINING PART IS DIVIDED INTO 15 EQUAL
SECTIONS.
C
N1 = 11
XLAST = XB(NPTS)
BODY1 = NEODYS - 1
DX = XLAST * 0.2 / 10.0
DO 200 I=1,N1
AI = I - 1
TY(1) = DX * AI
XB(1) = TY(1)
CALL POINT(1)
RE(1) = TY(2)
IF ( ICAMER .EQ. 0 ) GO TO 200
ZD(1) = TY(3)
200 CONTINUE
C
XS1 = N1 - 1
N2 = N1 + 1
DX = ( XLAST - XB(N1) ) / ( BODY1 - XS1 )
DO 250 I=N2, NEODYS
XB(I) = XB(I-1) + DX
TY(1) = XB(I)
CALL POINT(1)
RE(I) = TY(2)
IF ( ICAMER .EQ. 0 ) GO TO 250
ZL(I) = TY(3)
250 CONTINUE
C
CALCULATE THE SLOPE AND CAMBER OF BODY AT POINT MIDWAY BETWEEN
STATION.
C
DO 275 I=2, NEODYS
TY(1) = ( XB(I-1) + XB(I) ) * 0.5
CALL POINT(1)
DRDX(I-1) = TY(2) / TY(1)
IF ( ICAMER .EQ. 0 ) GO TO 275
DZDX(I-1) = TY(3) / TY(1)
275 CONTINUE
NEB1 = NEODYS - 1
DRDX(NBODYS) = (RE(NBODYS) - RE(NB1)) / ( XB(NBODYS) - XB(NB1) )
C
TY(1) = XB(1)
CALL POINT(1)
DSB1 = TY(2) / TY(1)
TY(1) = XB(51)
CALL POINT(1)
DSE2 = TY(2) / TY(1)
C
GENERATE THETA
DTH = 180.0 / FLOAT( NTHET - 1 )
DO 300 I=1,NTHET
AI = I - 1
THETA(I) = DTH * AI
300 CONTINUE
C

```



```

C
DO 100 ITRAN = 1, NTN
  READ (5,901) ID, ICHECK, NM, (VA(1,ITRAN,NSYM), I=1,3), (VB(1,ITRAN)
  1 I=1,3)
  READ (5,902) (VC(I, ITRAN), I=1,3)
  IF (ITRAN .GT. 1) GO TO 50
  IF (ICORD(1) .EQ. ICHECK) ISYM( NSYM ) = 0
  IF (ICORD(2) .EQ. ICHECK) ISYM( NSYM ) = 1
  IF (ICORD(3) .EQ. ICHECK) ISYM( NSYM ) = 2
C
50 CONTINUE
  CALL TRANS( VA(1,ITRAN,NSYM), VB(1,ITRAN), VC(1,ITRAN), BTM(1,
  1 ITRAN, NSYM) )
  100 CONTINUE
C
901 FORMAT ( A5, A1, 2X, I8, 8X, 6F8.2 )
902 FORMAT ( 8X, 3F8.2 )
C
RETURN
END
CDECK, BODYIN
SUBROUTINE BODYIN
C
COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, NHING, XMACHN,
1 SYMM, KACE, NPOLAR, IRW
COMMON/ BODY2 / NBPEL, NBODYS, NTHET, XB(51), RB(51), ZD(51),
1 THETA(11), RPP, XBPANL(20)
COMMON/ BODYSP / DRDX(51), DZDX(51)
COMMON/ CORTN / NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
COMMON/ DEFAU / BODY, BODYS, BTHET, CPCALC, NCASE, NRUN, DADeg, ARB,
1 PLANE, POLAR, RP, XNACEL, SYM THICK, WING, XMACH,
2 XNB, XNC, PINF, IPUNCH, SID(20), CKASE, ARW
COMMON/ WINGFM / XUI(30,20), YUI(30,20), ZUI(30,20), NUPI(20),
1 NCHORD, NSPAN, ISOLID, NPLANE, ICAMBR, ITWIST, ITHICK,
2 IFORM(10), PIVOT(10), DIH(10)
C
NBODY = 1
NBODYS = IFIX( BODYS )
NSYM = 1
NTHET = IFIX( BTHET )
NHING = 0
PLANE = 0.0
THKOMP = 1.0
WING = 0.0
SOLID = 0.0
THICK = 0.0
PUNCH = FLOAT( IPUNCH )
C
      READ IN BODY PROFILE AND COMPUTE BODY RADIUS DISTRIBUTION AT
      OPTIMUM LOCATIONS.
C
  CALL BODYPF( XB, RB, ZD, THETA, NBPEL, NTHET, NBODYS, XBS1, XBS2,
  1 DSRT, DSB2 )
  BODYS = FLOAT( NBODYS )
C
      WRITE ON TAPE 11 FOR AERODYNAMIC ANALYSIS.
C
      REXIND 11
      WRITE (11,1020) BODYS, BTHET, PLANE, RP
      WRITE (11,1020) ( XB(N), N=1, NBODYS )
      WRITE (11,1020) ( RB(N), N=1, NBODYS )

```

```

WRITE ( 11,1020) ( ZD(N), N=1,NBODYS)
WRITE ( 11,1020) ( THETA(N), N=1,NTHET)
WRITE ( 11,1020) XBS1,XBS2,DSB1,DSB2
WRITE ( 11,1020) XMACH,SYM,THKOMP
WRITE ( 11,1020) CKASE,CPCALC,POLAR,THICK,XNACEL,PINF,PUNCH,SOLID,
1 WING (SID(K), K=1,20), (IFORM(K), K=1,10)
WRITE ( 11,1020) ARB,DADEG
REWIND 11

C 1020 FORMAT (7F10.4)
C
RETURN
END
CDECK,BANWIN
SUBROUTINE BANWIN
C
COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, NWING, XMACHN,
1 COMMON/ SYMM / KACE, NPOLAR, IRW
COMMON/ BODY2 / NEPFL, NBODYS, NTHET, XB(51), RB(51), ZD(51),
1 THETA(11), RPP, XBPANL(20)
COMMON/ BODYSP / DRDX(51), DZDX(51)
COMMON/ NACEL / NACELP, XN(51,2), RN(51,2), ZN(51,2), ARN(2)
COMMON/ CONTRN / NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
COMMON/ DEFAU / BODY, BODYS, BTHET, CPCALC, WCASE, NRUN, DADEG, ARB,
1 PLANE, POLAR, RP, XNACEL, SYM, THICK, WING, XMACH,
2 XNB, XNC, XPINF, IPUNCH, SID(20), CKASE, ARW
COMMON/ WANGLE / ALPHAC(55,10), ALPHAT(55,10), ARNT(55,10)
COMMON/ WINGFM / XWI(30,20), YWI(30,20), ZWI(30,20), NWPI(20), NCHORD,
1 NSPAN, ISOLID, NPLANE, ICAMER, ITWIST, ITHICK, IFORM(10)
2 PIVOT(10), DIH(10)
COMMON/ INPUT / TX(4,100)
COMMON/ POINTP / TY(4), TYP(4), TYP(4)
COMMON/ POINTS / NPTS, NVAR
DIMENSION REPANL(11), ZBPANL(11)

NBODY = 1
NBODYS = IFIX( BODYS )
NC = XNC
NB = XNB
NC1 = NC - 1
NB1 = NB - 1
NEC = NB1-NC1
NECT = NC * NB1
NCOLW = NWING * NC1
NX2 = 2 * NWING
NPLANE = IFIX( PLANE )
NTHET = IFIX( BTHET )
THKOMP = 1.0
WING = FLOAT(NWING)
SOLID = FLOAT(ISOLID)
PUNCH = FLOAT(IPUNCH)

CALL BODYPF( XB, RB, ZD, THETA, NEPFL, NTHET, NBODYS, XBS1, XBS2,
1 DSB1, DSB2 )
BODYS = FLOAT( NBODYS )
C
C
C
CALL BODYPN
C
REWIND 11
WRITE ( 11,1020) BODYS, BTHET, PLANE, RP
WRITE ( 11,1020) ( XB(N), N=1,NBODYS)
WRITE ( 11,1020) ( RB(N), N=1,NBODYS)

```



```

WRITE ( 11,1020) ( ZD(N), N=1,NBODYS)
WRITE ( 11,1020) ( THETA(N), N=1,NTHET)
WRITE ( 11,1020) XBS1,XBS2,DSB1,DSB2
WRITE ( 11,1020) ( XBPANL(N), N=1,NPLANE )
IF ( RP .GT. 0.0 ) GO TO 410
WRITE ( 11,1020) ( REPANL(N), N=1,NTHET )
WRITE ( 11,1020) ( ZBPANL(N), N=1,NTHET )

410 CONTINUE
PERCT = 0.1
DO 450 I = 1, NW2, 2
WRITE ( 11,1020) XWI(1,I),YWI(1,I),XWI(2,I),YWI(2,I),YWI(4,I),
1 XWI(3,I)
WRITE ( 11,1020) XNB, XNC, WCASE, ZWI(1,I)
NW1 = I / 2 + 1
WRITE ( 11,1020) PIVOT(NW1), DIH(NW1)
CALL WINGS( NW1 )
450 CONTINUE
TWIST = FLOAT( ITWIST )
THICK = FLOAT( ITHICK )
WRITE ( 11,1020) XMACH, SYM, THICK
WRITE ( 11,1020) CKASE, CPCALC, POLAR, THICK, XNACEL, PINF, PUNCH,
1 SOLID,WING,(SID(K),K=1,20),(IFORM(K),K=1,10)
C IF ( XNACEL .EQ. 0 ) GO TO 460
CALL XNACEL( XNACEL, NHING )
460 CONTINUE
WRITE ( 11,1020) ARE, DADEG
WRITE ( 11,1020) ARN, TWIST
IF ( ITWIST .EQ. 1 ) WRITE ( 11,1020) ( (ARWT(J,I), J=1,NB1), I=1,
1 NHING )
IF ( ICOMBR .EQ. 1 ) WRITE ( 11,1020) ( ( ALPHAC(I,J), I=1,NBC),
1 J=1,NHING )
IF ( ITHICK .EQ. 1 ) WRITE ( 11,1020) ( ( ALPHAT(I,J), I=1,NBCT),
1 J=1,NHING )
REWIND 11
C 805 FORMAT ( 8F10.3 )
1020 FORMAT ( 7F10.4 )
C
RETURN
END
CDECK,WINGIN
SUBROUTINE WINGIN
C
COMMON/ MAIN / LA, LB, LC, LD, LE, LF, LI, LO, NBODY, NHING, XMACHN,
1 SYMH, KACE, NPOLAR, IRW
COMMON/DEFAU / BODY, BODYS, BTHET, CPCALC, CASE, NRUN, DADEG, ARB,
1 PLANE, POLAR, RP, XNACEL, SYM, THICK, WING, XMACH,
2 XNB, XNC, PINF, IPUNCH, SID(20), CKASE, ARW
COMMON/WANGLE / ALPHAC(55,10), ALPHAT(55,10), ARWT(55,10)
COMMON/WINGFM/ XWI(30,20), YWI(30,20), ZWI(30,20), NWPI(20), NCHORD,
1 NSPAN, ISOLID, NPLANE, ICAMBR, ITWIST, ITHICK, IFORM(10)
2 , PIVOT(10), DIH(10)
C
NBODY = 0
THCOMP = 1.0
NPLANE = IFIX( PLANE )
PUNCH = IFIX( IPUNCH )
SOLID = IFIX( ISOLID )
WING = IFIX( NHING )
C
NC = XNC

```



```

IF ( ALPHAC(K,I)*CDR .GT. 0.01 ) GO TO 415
410 CONTINUE
GO TO 416
415 CONTINUE
ICAMSR = 1
416 CONTINUE
GO TO 500
C 450 CONTINUE
C C C
      FLAT WING SURFACE
ITWIST = 0
ICAMSR = 0
1 CNX = ( YWI(2, NW) - YWI(1, NW)) * (ZWI(3, NW) - ZWI(1, NW)) - ( YWI(3, NW) -
1 CNZ = ( XWI(2, NW) - XWI(1, NW)) * ( YWI(3, NW) - YWI(1, NW)) - ( XWI(3,
1 NX) - XWI(1, NW)) * ( YWI(2, NW) - YWI(1, NW))
ALP = ATAN( - CNX / CNZ )
DO 470 J = 1, NP
  ALPHAT(J,I) = ALP
470 CONTINUE
C 500 CONTINUE
C C C
      REARRANGE ALPHAT TO CORRESPONDING WITH AERO CODE FORMAT
DO 505 K = 1, NB1
  IO = NP - K*NC1 + 1
  IR = NP1 - K*NCH + 1
DO 504 J = 1, NC1
  JO = NP - J - (K-1)*NC1 + 1
  JR = NP1 - J - (K-1)*NCH + 1
  ALPHAT(JR,I) = ALPHAT(JO,I)
504 CONTINUE
  ALPHAT(IR,I) = ALPHAT(IO,I)
505 CONTINUE
C C C C
      SET ITHICK FOR WING
ITHICK = 0
DO 510 K = 1, NP
  IF ( ALPHAT(K,I)*CDR .GT. 0.01 ) GO TO 515
510 CONTINUE
GO TO 516
515 CONTINUE
ITHICK = 1
516 CONTINUE
C C C C
      RETURN
END
CDECK COEFF
      SUBROUTINE COEFF( X, Y, Z, CF, N )
C C C C
      COMPUTES COEFFICIENTS OF INTERPOLATION OF Z AT N POINTS(X,Y)
      DIMENSION X(1), Y(1), Z(1), CF(1), XT(115), YT(115), CFT(115)
      N3 = N + 3
      DO 100 I = 1, N
        XT(I) = X(I)
        YT(I) = Y(I)
        CFT(I) = Z(I)

```

```

100 CONTINUE
C
C   CALL SURFIT( XT, YT, N3, CFT )
C
DO 200 I=1,N3
  CF(I) = CFT(I)
200 CONTINUE
C
  RETURN
END
CDECK INTERP
SUBROUTINE INTERP( N, X, Y, CF, NP, XP, YP, ZP )
C
C   INTERPOLATES AT NP POINTS ( XP, YP )
C
  DIMENSION X(1), Y(1), XF(1), YP(1), ZP(1), CF(1)
C
DO 100 I=1,NP
  SUM = CF(2)
DO 110 J=1,N
  J3 = J + 3
  RI = (XP(I) - X(J))**2 + (YP(I) - Y(J))**2
  IF ( RI .LT. 1.E-9 ) GO TO 110
  SUM = SUM + 2.0*CF(J3)*(1.0+ALOG(RI))*(XP(I)-X(J))
110 CONTINUE
  ZP(I) = SUM
100 CONTINUE
C
  RETURN
END
CDECK WPNAC
SUBROUTINE WPNAC( XI, YI, NC, NB, XC, YC )
C
C   COMPUTE CONTROL POINT ( XC, YC ) OF WING PANELS
C
  DIMENSION XI(1), YI(1), XC(1), YC(1), XY(13,11), XW(13), YW(11),
1    DY(11)
C
  PERCT = 0.1
  XCPT = 0.95
  XW(1) = XI(1)
  XCHORD = XI(2) - XI(1)
  XW(2) = XW(1) + PERCT*XCHORD
  DX = (1.0 - PERCT) * XCHORD / ( NC - 2 )
DO 100 L=3,NC
  XW(L) = XW(L-1) + DX
100 CONTINUE
  BY = YI(4) - YI(1)
  DBY = BY / ( NB - 1 )
  YW(1) = YI(1)
DO 165 N=2,NB
  YW(N) = YW(N-1) + DBY
165 CONTINUE
  SLE = ( XI(4)-XI(1) ) / BY
  STE = ( XI(3)-XI(2) ) / BY
  IF ( SLE-STE ) 210, 230, 210
210 CONTINUE
  DX = ( XI(3) - XI(4) ) / ( XI(2) - XI(1) )
DO 215 M=1,NC
  XY( M, NB ) = XI(4) + DX * ( XW(M) - XI( 1 ) )
215 CONTINUE
DO 220 N=1,N3
  DY(N) = ( YW(N) - YI(1) ) / BY

```

```

DO 220 M=1,NC
XY(M,N) = XM(M) + ( XY(M,NB) - XM(M) ) * DY(N)
220 CONTINUE
GO TO 250
230 CONTINUE
DO 240 N=1,NB
DY(N) = YM(N) - YI(1)
DO 240 M=1,NC
XY(M,N) = XM(M) + SLE* DY(N)
240 CONTINUE
250 CONTINUE
C
C CONTROL POINT COORDINATES ( XC, YC )
C
NC1 = NC-1
NB1 = NB-1
DO 350 N=1,NB1
DO 350 M=1,NC1
K = M + (N-1)*NC1
CT = XY(M+1,N+1) - XY(M,N+1)
CR = XY(M+1,N) - XY(M,N)
RY = ( 1.0 + CT/(CR*CT) )/3.0
RY1 = 1.0 - RY
XWL = RY*XY(M,N+1) + RY1*XY(M,N)
YWL = RY*XY(M+1,N+1) + RY1*XY(M+1,N)
XC(K) = XCPT * XWL + ( 1.0 - XCPT ) * XWL
YC(K) = YW( N+1 ) * RY + YW(N) * RY1
350 CONTINUE
C
C RETURN
C
C END
C
C SUBROUTINE WTWIST( YC, I )
C
C COMPUTES THE WING TWIST ANGLE ARWT
C
COMMON/ANGLE/ ALPHAC(55,10), ALPHAT(55,10), ARWT(55,10)
COMMON/WINGFM/ XWI(30,20), YWI(30,20), ZWI(30,20), NWPI(20), NCHORD,
1 NSPAN, ISOLID, NPLANE, ICAMBR, ITWIST, ITHICK, IFORM(10)
2 PIVOT(10) DIH(10)
C
C DIMENSION YC(1), VX(2), VY(2), VZ(2)
C
C COMPUTES LEADING AND TRAILING EDGE UNIT VECTORS
C
DO 100 J=1,2
J1 = 4
J2 = 1
IF ( J.EQ. 2 ) J1 = 3
IF ( J.EQ. 2 ) J2 = 2
DX = XWI(J1,I) - XWI(J2,I)
DY = YWI(J1,I) - YWI(J2,I)
DZ = ZWI(J1,I) - ZWI(J2,I)
SUML = SQRT( DX**2 + DY**2 + DZ**2 )
VX(J) = DX / SUML
VY(J) = DY / SUML
VZ(J) = DZ / SUML
100 CONTINUE
C
NB1 = NSPAN - 1
NC1 = NCHORD - 1
DO 200 K=1,NB1
K1 = 1 + ( K-1 ) * NCHORD
DY = YC( K1 ) - YWI( 1, I )
XLE = XWI(1,I) + VX(1) * DY / VY(1)

```



```

C      ZI = VA( 3, 1, NSYM ) + VA( 3, 2, NSYM )
C      WRITE (11,1020) XN(1,N), YI, ZI, NBODYS, NTHET, ARN(N)
C      IF ( XNACEL) 100, 300, 200
C 100 CONTINUE
C      IF ( N - 1 ) 300, 200, 300
C 200 CONTINUE
C      WRITE (11,1020) ( XN(L,N), L=1,NBODYS )
C      WRITE (11,1020) ( RN(L,N), L=1,NBODYS )
C      WRITE (11,1020) ( ZN(L,N), L=1,NBODYS )
C      WRITE (11,1020) ( THETA(L), L=1,NTHET )
C      WRITE (11,1020) XN1, XN2, DS1, DS2, (DRDX(J), DZDX(J), J=1,NBODYS)
C 300 CONTINUE
C 1020 FORMAT ( 7F10.4 )
C
C      RETURN
C      END
C      SUBROUTINE TRANS( A, B, C, UNIVEC )
C
C      COMPUTES THE TRANSFORM MATRIX TFM BETWEEN TWO COORDINATE
C      SYSTEMS 1 AND 2. A DEFINE THE ORIGIN, B A POINT ON
C      THE Z AXIS AND C A POINT ON THE X - Z PLANE OF COORDINA-
C      TE SYSTEM 2.
C      THE MATRIX UNIVEC(L,M) HAS THE ROW INDEX L FOR THE UNIT VECTOR
C      I, J, K AND THE COLUMN INDEX M FOR THEIR THREE COMPONENTS IN
C      THE COORDINATE SYSTEM 1.
C
C      DIMENSION A(3), B(3), C(3), UNIVEC(3,3), UNIVCA( 3 ), N1(3), N2(3)
C      DATA N1 / 3, 1, 2 /, N2 / 2, 3, 1 /
C
C      COMPUTE THE UNIT VECTOR I, J, K OF COORDINATE SYSTEM 2 IN TERM
C      OF COORDINATE SYSTEM 1.
C
C      SUM = 0.0
C      SUM1 = 0.0
C      DO 100 I = 1, 3
C      SUM = SUM + ( B(I) - A(I) )**2
C      SUM1 = SUM1 + ( C(I) - A(I) )**2
C 100 CONTINUE
C      AB = SQRT ( SUM )
C      CA = SQRT ( SUM1 )
C
C      UNIT VECTOR K
C      UNIT VECTOR CA
C
C      DO 200 J = 1, 3
C      UNIVEC(3, J) = ( B(J) - A(J) ) / AB
C      UNIVCA( J ) = ( C(J) - A(J) ) / CA
C 200 CONTINUE
C
C      UNIT VECTOR J
C
C      SUM = 0.0
C      DO 300 I = 1, 3
C      I1 = N1(I)
C      I2 = N2(I)
C      UNIVEC(2, I) = UNIVCA(I1)*UNIVEC(3, I2) - UNIVCA( I2 ) * UNIVEC( 3, I1 )
C      SUM = SUM + UNIVEC( 2, I )**2
C 300 CONTINUE
C      SUM = SQRT ( SUM )

```

```

DO 350 I=1,3
UNIVEC(2,I) = UNIVEC(2,I) / SUM
350 CONTINUE
C
C      UNIT VECTOR I
C
SUM = 0.0
DO 400 I = 1, 3
I1 = N1(I)
I2 = N2(I)
UNIVEC( 1, I) = UNIVEC(2, I2) * UNIVEC( 3, I1 ) - UNIVEC( 2, I1 ) *
1 UNIVEC( 3, I2 )
SUM = SUM + UNIVEC( 1, I)**2
400 CONTINUE
SUM = SQRT( SUM )
DO 450 I=1,3
UNIVEC(1,I) = UNIVEC(1,I) / SUM
450 CONTINUE
C
C      RETURN
C      END
CDECK, CUSERT
SUBROUTINE CUBERT
DIMENSION X(3)
COMMON/LOCIN / V(3), L, M, G(4), VMAX, VMIN
COMMON/POINTS/ NPTS, NVAR
L=0
SUM = SQRT( G(1)**2+G(2)**2+G(3)**2+G(4)**2 )
G1 = G(1) / SUM
G2 = G(2) / SUM
G3 = G(3) / SUM
G4 = G(4) / SUM
EQ. 1 G1*X**3 + G2*X**2 + G3*X = 0.
IF ( ABS( G4 ) .LT. 1.E-6) GO TO 4
EQ. 2 G1*X**3 + G2*X**2 + G3*X + G4 = 0.
IF ( ABS( G1 ) .GT. 1.E-6) GO TO 9
EQ. 3 G2*X**2 + G3*X + G4 = 0.
IF ( ABS( G2 ) .GT. 1.E-6) GO TO 7
EQ. 4 G3*X + G4 = 0.
IF ( ABS( G3 ) .GT. 1.E-6) GO TO 5
RETURN
C
C      4 CONTINUE
V(1) = 0.0
L=1
RETURN
C
C      5 CONTINUE
V(1) = - G(4) / G(3)
GO TO 35
C
C      7 CONTINUE
R1 = G(3)**2 - 4.0*G(2)*G(4)
IF ( R1 .GT. 0.0 ) GO TO 107
WRITE (6,901)
901 FORMAT (1H0,NAGATIVE RADICAL RESULTED FROM SOLVING THE QUADRATIC
1 EQUATION G2.X2 + G3.X + G4 = 0*)
RETURN
C
C      107 CONTINUE
R1=SQRT(R1)
V1 = ( -G(3) + R1 ) *0.5 / G(2)
V(1) = V1
IF ( V1 .GT. VMIN .AND. V1 .LT. VMAX ) GO TO 8

```



```

40 CONTINUE
DO 45 I=1,3
VO = X(I) - A1/3.0
X(I) = VO
V(I) = VO
IF ( VO .LT. VMIN .OR. VO .GT. VMAX ) GO TO 50
L=1
RETURN
50 CONTINUE
45 CONTINUE
WRITE (6,904) VMIN, V(1), V(2), V(3), VMAX
904 FORMAT (1H0, 'ALL THREE UNEQUAL ROOTS OUTSIDE OF LIMIT VMIN, VMAX*/
1 1X, 'VMIN =', E14.4, 'X, *V1 =', E14.4, 'X, *V2 =', E14.4, 'X, *V3 =',
2 E14.4, 'X, *VMAX =', E14.4)
C
RETURN
END
CDECK POINT
SUBROUTINE POINT( N )
COMMON/ CURFIT/ B( 4, 4, 100), T(100), SCALEF( 4 )
COMMON/ ENDPT/ XFIRST, XLAST, XSAVE(100)
COMMON/ LOCTN/ V(3), L, M, A(4), VMAX, VMIN
COMMON/ POINTS/ NPTS, NVAR
COMMON/ POINTP/ X(4), XP( 4), XPP( 4)
DIMENSION DX(4)
N1 = NPTS - 1
IF (N.NE.0) GO TO 4
DO 1 I=1,N1
M=I
1 CONTINUE
IF ( V(I) .LE. T(I+1) ) GO TO 2
WRITE(6,100)
100 FORMAT(1H0, '33H ERROR - PARAMETER EXCEEDS LIMITS)
RETURN
2 CONTINUE
DO 300 K=1,3
P = V(K)
DX(K) = 1.E10
IF ( P .LT. VMIN .OR. P .GT. VMAX ) GO TO 300
DX(K) = ABS((((B(1,M))*P + B(1,2,M))*P + B(1,3,M))*P + B(1,4,M))*
1 SCALEF(1) - XIND )
300 CONTINUE
IF ( DX(1) .GT. DX(2) ) GO TO 302
IDENT = 1
IF ( DX(1) .GT. DX(3) ) IDENT = 3
GO TO 305
302 CONTINUE
IDENT = 2
IF ( DX(2) .GT. DX(3) ) IDENT = 3
305 CONTINUE
P = V(IDENT)
DO 3 I=1, NVAR
X(I) = ((B(1,1,M))*P+B(1,2,M))*P+B(1,3,M))*P+B(1,4,M))*SCALEF(1)
XP(I) = ((B(1,1,M))*P+B(1,2,M))*P+B(1,3,M))*SCALEF(1)
3 XPP(I) = ((B(1,1,M))*P+B(1,2,M))*P+B(1,3,M))*SCALEF(1)
C
310 CONTINUE
RETURN
C
4 X(N) = X(N)/SCALEF(N)
DO 5 I=1,N1
M=I

```

```

K = I + 1
IF ( XSAVE(K) .GE. X(N) ) GO TO 6
5 CONTINUE
XIND = X(N) * SCALEF(N)
XFT = XFIRST * SCALEF(1)
XLT = XLAST * SCALEF(1)
WRITE (6,101) XIND, XFT, XLT
101 FORMAT (1H0,*, THE GIVEN VALUE F INDEPENDENT VARIABLE *E12.4,
5X,*, IS OUT OF RANGE TO BE INTERPOLATED *E12.4,5X,E12.4)
1 RETURN
DO 7 I=1,4
6 A(1)=B(N,I,M)
A(4)=A(4)-X(N)
IF ( XFIRST .EQ. X(N) ) GO TO 112
IF ( XLAST .EQ. X(1) ) GO TO 111
VMAX = T(M+1) * 1.0001
VMIN = T(M) * 0.9999
CALL CUBERT
XIND = X(1) * SCALEF(1)
GO TO 103
112 V(1) = 0.0
L=1
GO TO 103
111 V(1) = 1.0
L=1
103 CONTINUE
IF (L.NE.0) GO TO 2
OP = P
WRITE (6,10) OP
10 FORCAT (1X4HOP =,E15.8)
DO 8 J=1,2
K = M + J - 1
B1 = B(N,1,K)
B2 = B(N,2,K)
B3 = B(N,3,K)
B4 = B(N,4,K)
P = T(K)
SUM = B1*P**3 + B2*P**2 + B3*P + B4
DIF = SUM - X(N)
8 WRITE (6,9) K,P,B1,B2,B3,B4,X(N),SUM,DIF
9 FORCAT (1X13,8E15.8)
WRITE (6,102)
102 FORCAT (1H0,32H FAILURE IN CUBE ROOT EXTRACTION)
103 CONTINUE
END
CHECK SPLFIT
SUBROUTINE SPLFIT
REAL L,X,MU
COMMON/CURFIT/ B(4,4,100), T(100), SCALEF(4)
COMMON/ENDPT/ XFIRST, XLAST, XSAVE(100)
COMMON/INPUT / X(4,100)
COMMON/POINTS/ NPTS,NVAR
COMMON/DIMENSION M(4,100), S(100), L(100), MU(100), P(100), Q(100)
1 IF (NPTS.GT.100) NPTS=100
DO 200 I=1, NVAR
DO 200 J=1, NVAR
200 SCALEF(I)=0.
DO 201 I=1, NPTS
DO 201 J=1, NVAR
201 SCALEF(J)=AMAX1(SCALEF(J),ABS(X(J,I)))
DO 101 J=1, NVAR
DO 101 I=1, NPTS
101 IF ( SCALEF(J) .LT. 1.E-10 ) SCALEF(J) = 1.0
DO 202 I=1, NPTS
DO 202 J=1, NVAR

```



```

202 X(I,I)=X(J,I)/SCALEF(J)
DO 203 I=1,NPTS
  XSAVE(I) = X(I,I)
203 CONTINUE
  XFIRST = X(1,1)
  XLAST = X(1,NPTS)
  T(1)=0.
  S(1)=0.
  SUM=0.
  L(1)=-2.
  MU(1)=0.
  MU(NPTS)=0.
  MU(NPTS)=-2.
  D(1)=0.
  D(NPTS)=0.
  P(1)=2.
  Q(1)=1.
  U(1)=0.
  N1=NPTS-1
  DO 2 I=2,NPTS
    SUM1=0.
    DO 1 J=1,NVAR
      1 SUM1=SUM1+(X(J,I)-X(J,I-1))**2
      S(I)=SQRT(SUM1)
      2 T(I)=T(I-1)+S(I)
      DO 3 I=2,NPTS
        S(I)=S(I)/T(NPTS)
        3 T(I)=T(I)/T(NPTS)
        DO 4 I=2,N1
          L(I)=S(I+1)/(S(I)+S(I+1))
          MU(I)=1-L(I)
          P(I)=MU(I)*Q(I-1)+2.
          4 Q(I)=L(I)/P(I)
          P(NPTS)=2.*(1.-Q(N1))
          DO 7 I=1,NVAR
            DO 5 J=2,N1
              DO 6 J=1,N1
                5 U(J)=0.-(X(I,J+1)-X(I,J))/S(J+1)-(X(I,J)-X(I,J-1))/S(J)/(S(J)+
                1 S(J+1))
                6 U(J)=0.-(X(I,J+1)-X(I,J))/S(J+1)-(X(I,J)-X(I,J-1))/S(J)/(S(J)+
                U(NPTS))=MU(NPTS)*U(N1)/P(NPTS)
                M(I,NPTS)=U(NPTS)
                DO 6 J=1,N1
                  K=NPTS-J
                  M(I,K)=Q(K)*M(I,K+1)+U(K)
                  B(I,K)=M(I,K+1)-M(I,K)/(6.*S(K+1))
                  B(I,K)=5.*M(I,K)*T(K+1)-M(I,K+1)*T(K)/S(K+1)
                  B(I,K)=5.*M(I,K+1)*T(K)**2-M(I,K)*T(K+1)*T(K+1)-X(I,K)+
                  1*(M(I,K)-M(I,K+1))*S(K+1)**2/6./S(K+1)
                  6 B(I,K)=M(I,K)*T(K+1)+3-M(I,K+1)*T(K)**3/(6.*S(K+1))+X(I,K)*T
                  1(K+1)-X(I,K+1)*T(K)/S(K+1)+S(K+1)/6.*M(I,K+1)*T(K)*T(K+1)
                7 CONTINUE
              RETURN
            END
  CDECK INVERT
  C SUEROUTINE INVERT (GOTON, A, IA, IPIVOT, INDXR, INDXC, NROWS)
  C .....
  C .....
  C .....
  C .....
  C REAL A(NROWS, NROWS), PIVOT, T
  C INTEGER IPIVOT(IA), INDXR(IA), INDXC(IA)
  C .....
  INVE1010
  INVE1020
  INVE1030
  INVE1040
  INVE1050
  INVE1060
  INVE1070
  INVE1080
  INVE1090

```


1130 FORMAT (29H ERROR THE MATRIX IS SINGULAR)

```

END
CDECK, SUBROUTINE SURFIT( X, Y, N3, B )
C
C   COMPUTES COEFFICIENTS FOR SURFACE SPLINE.
C   N TOTAL NUMBER OF INPUT POINTS, CAN BE RANDOMLY LOCATED.
C   JEQ FOR EQUATION NUMBERING
C   MUK FOR COEFFICIENT NUMBERING
C
C   CF ARE THE COEFFICIENT MATRIX OF EQUATION
C    $W(X,Y) = B(1) + B(2)*X + B(3)*Y + \text{SUM OF } B(I) * R(I)**2 *$ 
C    $\text{LN}(R(I)**2)$ 
C
C   COMMON/REPEAT/ IREP
C   DIMENSION IPIV(115), INXR(115), INXC(115), CF(115,115), TM(115)
C   DIMENSION X(N3), Y(N3), B(N3)
C
C   N4 = 115
C   N2 = N3 - 1
C   N1 = N3 - 2
C   N = N3 - 3
C
C   BYPASS MATRIX INVERSION FOR THE CASE WHERE THE DATA POINTS (X,
C   Y ) ARE IDENTICAL FOR INTERPOLATION
C
101 CONTINUE
DO 100 JEQ = 1, N
  CF( JEQ, 1 ) = 1.0
  CF( JEQ, 2 ) = X( JEQ )
  CF( JEQ, 3 ) = Y( JEQ )
  DO 90 MUK = 1, N
    MUK1 = MUK + 3
    IF ( MUK .EQ. JEQ ) GO TO 90
    RJM = ( X( MUK ) - X( JEQ ) )**2 + ( Y( MUK ) - Y( JEQ ) )**2
    CF( JEQ, MUK1 ) = RJM * ALOG( RJM )
  90 CONTINUE
100 CONTINUE
C
DO 150 K=1,3
  CF( N1, K ) = 0.0
  CF( N2, K ) = 0.0
  CF( N3, K ) = 0.0
150 CONTINUE
DO 200 MUK = 1, N
  MUK1 = MUK + 3
  CF( N1, MUK1 ) = 1.0
  CF( N2, MUK1 ) = X( MUK )
  CF( N3, MUK1 ) = Y( MUK )
200 CONTINUE
C
C
IA = N3
CALL INVERT( GOT, CF, IA, IPIV, INXR, INXC, N4 )
C
250 CONTINUE
B( N1 ) = B( N2 ) = B( N3 ) = 0.0
C
DO 300 I=1, N3
  SUM = 0.0
  DO 290 J=1, N3
    SUM = SUM + CF( I, J ) * B( J )
  290 CONTINUE
  TX( I ) = SUM

```



```

C 300 CONTINUE
C DO 400 I=1,N3
C B(I) = TM(I)
C 400 CONTINUE
C RETURN
C END
CDECK ADATE
C OVERLAY(WOOD,3,0)
C PROGRAM ADATE
C .....
C CONTROL ROUTINE FOR COMPUTING AERODYNAMIC INFLUENCE COEFFICIENTS
C MATRIX AND VELOCITY COMPONENTS
C .....
C COMMON / MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1 COMMON /NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRV
1,CHORD(210)
2,ISYM
3,NPART(210),NPANEL,NROW(2)
4,THETA(210),TAIL,THKORP
5,UC(210)
6,V(210),VPM(210),VV(210),VPM(210)
7,W(210),WPM(210),WM(210),WPM(210)
8,X(210,3,4),XBAR(210),XC(210)
9,Y(210,3,4),YBAR(210),YC(210)
A,Z(210,3,4),ZBAR(210),ZC(210)
C READ IN GEOMETRICAL DATA
C CALL INTAPE
C WRITE(NTAPEO,1040)
C KACE = 1 WING ALONE
C KACE = 2 BODY ALONE
C KACE = 3 WING-BODY COMBINATION
C GO TO (1000,1030,1000),KACE
C COMPUTE VELOCITY COMPONENTS DUE TO WING SOURCES
C THICKNESS CASE
C IF (THKORP .EQ. 0.0) GO TO 1010
1000 NS=NBODY+1
C CALL EVAL(NS,XBAR,1.)
C WRITE(NTAPEO,1050)
C GO TO 1020
1010 CALL FOREOF (NTAPEA)
C CALL FOREOF (NTAPEB)
C COMPUTE VELOCITY COMPONENTS TO WING PANEL SINGULARITIES
C LIFTING CASE
1020 NS=1
C CALL EVAL (NS,XC,0.)
C WRITE(NTAPEO,1050)
1030 REWIND NTAPEC
C REWIND NTAPEA
C REWIND NTAPEB
C .....
C .....
C .....
C 1040 FORMAT(1H0,11HEXIT INTAPE)
C 1050 FORMAT(1H0,9HEXIT EVAL)

```

AMAT11010
 AMAT11020
 AMAT11030
 AMAT11040
 AMAT11050
 AMAT11060
 AMAT11090
 AMAT11100
 AMAT11110
 AMAT11120
 AMAT11130
 AMAT11140
 AMAT11150
 AMAT11160
 AMAT11170
 AMAT11180
 AMAT11190
 AMAT11200
 AMAT11210
 AMAT11220
 AMAT11230
 AMAT11240
 AMAT11250
 AMAT11260
 AMAT11270
 AMAT11280
 AMAT11290
 AMAT11300
 AMAT11310
 AMAT11320
 AMAT11330
 AMAT11340
 AMAT11350
 AMAT11360
 AMAT11370
 AMAT11380
 AMAT11390
 AMAT11400
 AMAT11410
 AMAT11420
 AMAT11430
 AMAT11440
 AMAT11450
 AMAT11460
 AMAT11470
 AMAT11480
 AMAT11490
 AMAT11510
 AMAT11520
 AMAT11530
 AMAT11540
 AMAT11550

```

CDECK EVAL
END SUBROUTINE EVAL (NI, XCPT, THKW)
C
C .....
C COMPUTES AERODYNAMIC INFLUENCE COEFFICIENTS MATRIX AND VELOCITY
C COMPONENTS MATRIX
C .....
C
COMMON / MAIN / NTAPEA, NTAPEB, NTAPEC, NTAPEE, NTAPEF, NTAPEI,
1 COMMON / NTAPEO, NBDY, NKG, XMACH, SYM, KACE, NPOLAR, IRM
COMMON / PANEL / VS2(110), VS2(110), WSS(110)
COMMON / BLOCK / ALPHAS(210), AREA(210), A(210), ALPHAT(110)
1, CHORD(210)
2, ISYM
3, NPART(210), NPANEL, NROW(2)
4, THETA(210), TAIL, THKOMP
5, U(210)
6, V(210), VPX(210), VV(210), VPM(210)
7, W(210), WPM(210), WX(210), WPM(210)
8, X(210, 3, 4), XBAR(210), XC(210)
9, Y(210, 3, 4), YBAR(210), YC(210)
A, Z(210, 3, 4), ZBAR(210), ZC(210)
C
DIMENSION AS(210), EBETAM(4), C(4), CPM(4), CPM(4), Q(4)
1, R(4), RPM(4), RPM(4), UU(210), US(210), VS(210), WS(210)
2, XCPT(210)
C
ASINH(B)=ALOG(B+SQRT(1.+B*B))
ACOSH(E)=2.*ALOG(SQRT(ABS((E+1.)/2.))+SQRT(ABS((E-1.)/2.)))
C
EPS=0.0001
BETA=SQRT(ABS(XMACH**2-1.))
PI=3.1415926
CONSTA=BETA/4.0
CONSTB=CONSTA/PI
CONSTD=BETA/PI
LVSD=THKW
IT=1
C
INFLUENCING PANEL I
C
GO TO (1000, 2580, 1010), KACE
1000 NC=NWING/NROW(1)
NR=NROW(1)
I1=1
I2=NWING
GO TO 1050
1010 IF (THKW) 1020, 1040, 1020
1020 NC=NWING/NROW(2)
NR=NROW(2)
NCT=NI-1
I1=NI
I2=NPANEL
GO 1030 N=1, NBDY
1030 XCPT(N)=XC(N)
GO TO 1060
1040 NC=NBDY/NROW(1)
NR=NROW(1)
I1=1
I2=NBDY
GO 1050 NCT=0
1050 NCT=0
1060 N=1

```

```

00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001220

```

```

C *****
C DO 2530 I=1,12
C *****
1080 IF(LVSD)1090,1130,1090
1090 SL=1.0
      IT=1-I-NI-NR*(N-1)
      IF(IT)1110,1110,1100
1100 N=N+1
      LVSD=1
      GO TO 1140
1110 LVSD=-1
      NCT=NCT+1
      GO TO 1140
1120 SL=-1.0
      LVSD=1
      GO TO 1140
1130 NCT=NCT+1
      GO TO 1140
1140 COST=COS(THETA(I))
      SINT=SIN(THETA(I))
      TANA= TAN(ALPHAS(I))
      ABR=BETA*TANA
      IF(ABR-1.0)1150,2570,2570
1150 IF(ABR)ABR-EPS)1160,1160,1170
1160 ABR=0.0
      SA=1.0
      GO TO 1180
1170 SA=SIGN(.5,ABR)
1180 APX2=ABR*ABR
      IN=I-NBODY
      NPT=NPART(I)
      TEST=ABS(Y(I,1))+ABS(ABS(THETA(I))-.5*PI)

C INFLUENCED PANEL J
C DO 2430 J=1,NPANEL
C JN=J-NBODY
C U(J)=0.0
C V(J)=0.0
C W(J)=0.0
C VPM(J)=0.
C WPM(J)=0.
C SINA=SIN(ALPHAS(J))
C COSA=COS(ALPHAS(J))
C DO 2430X=1,NPT
      BBETAX(1)=(X(I,M,2)-X(I,M,1))/((Y(I,M,2)-Y(I,M,1))*COST
1+Z(I,M,2)-Z(I,M,1))*SINT)
      BBETAX(3)=(X(I,M,4)-X(I,M,3))/((Y(I,M,4)-Y(I,M,3))*COST
1+Z(I,M,4)-Z(I,M,3))*SINT)
      BPX1=BBETAX(1)
      BPX3=BBETAX(3)
      IF(BETA)1190,1200,1190
1190 BBETAX(1)=BBETAX(1)/BETA
      BBETAX(3)=BBETAX(3)/BETA
1200 BBETAX(2)=BBETAX(1)
      BBETAX(4)=BBETAX(3)
C CORNER POINTS K OF INFLUENCING PANEL I
C DO 2420K=1,4

```



```

1390 IF (FTR1+1.)1450,1450,1390
1400 IF (FTR1-1.)1400,1420,1420
1410 FTR1=ACOS(FTR1)*SZ
1420 GO TO 1460
1430 IF (YPM-BPM*YPM)1420,1440,1450
1440 FTR1=PI/2.
1450 GO TO 1460
1460 FTR1=PI*SZ
1470 IF (EPX2-1.)1470,1480,1480
1480 FTR2=SQRT(TERM2)*ACOS((BPM*XIPM-YPM)/SQRT(TERM2))
1490 GO TO 1490
1500 FTR2=SQRT(TERM2)*ACOS((BPM*XIPM-YPM)/SQRT(TERM2))
1510 FTR2=SQRT(TERM2)*ACOS((BPM*XIPM-YPM)/SQRT(TERM2))
1520 FTR4=SQRT(XIPM2-TERM2)/TERM2
1530 FTR5=ACOSH(XIPM/TERM2)
1540 D=CONSTB*(BPM*FTR5+YPM*FTR4-FTR2)
1550 S=CONSTB*(BPM*FTR1-ZPM*FTR4)
1560 P=FTR1/(4.*PI)
1570 GO TO 2370
1580 IF (YPM)1570,1570,1520
1590 IF (XIPM-(BPM*YPM+SQRT(TERM2)*ABS(ZPM)))1570,1540,1530
1600 IF (YPM-BPM*XIPM)1570,1540,1550
1610 C1=5
1620 GO TO 1560
1630 CT=1.0
1640 D=CONSTA*SQRT(TERM2)*CT
1650 S=CONSTA*BPM*SZ*CT
1660 P=CT+SZ/4.
1670 GO TO 2370
1680 D=0.0
1690 S=0.0
1700 P=0.0
1710 GO TO 2370
1720 TERM2=1.+BPM2
1730 TERM2=SQRT(TERM2)
1740 IF (ZPM)1680,1590,1680
1750 IF (TERM2*AA*SZ)1600,1610,1620
1760 FTR1=0.
1770 GO TO 1630
1780 FTR1=PI/2.
1790 GO TO 1630
1800 FTR1=PI
1810 IF (YPM)1640,1720,1720
1820 TERM2=TERM2*(YPM+BPM*XIPM)
1830 IF (ABS(TERM2)-.001)1650,1650,1720
1840 TERM2=TERM2/ABS(YPM)
1850 IF (TERM2)1660,1670,1660
1860 FTR2=ALOG(TERM2*TERM2/(2.*TERM2))*(1.+BPM*TERM2/TERM2)
1870 GO TO 1730
1880 FTR2=ALOG(TERM2)
1890 GO TO 1730
1900 FTR1=(BPM*TERM2-XIPM*YPM)/SQRT(TERM2*(TERM2+TERM2*ZPM2))
1910 IF (FTR1+1.)1740,1740,1690
1920 IF (FTR1-1.)1710,1700,1700
1930 FTR1=0.
1940 GO TO 1720
1950 FTR1=ACOS(FTR1)*SZ
1960 FTR2=YPM-BPM*XIPM+TERM2*SQRT(XIPM2-TERM2)
1970 IF (FTR2.LE.0.0) GO TO 1650
1980 FTR2=ALOG(FTR2)
1990 FTR3=(XIPM+SQRT(XIPM2+TERM2))/TERM2
2000 IF (FTR3)1760,1750,1760
2010 FTR1=PI*SZ

```

```

00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070
00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310
00002320
00002330
00002340
00002350
00002360
00002370
00002380
00002390
00002400
00002410
00002420
00002430
00002440
00002450
00002460
00002470
00002480
00002490
00002500
00002510

```

```

1750 GO TO 1720
1750 FTR4=0.
GO TO 1770
1760 FTR4=BPM*ALOG(FTR3)
1770 IF (ZPM)1780,1790,1780
1780 FTR5=ATAN(YPM/ZPM)
GO TO 1800
1790 FTR5=PI/2.*SY
1800 P=(FTR1+FTR5)/(8.*PI)
S=CONSTB*(BPM*(FTR1+FTR5)-ZPM*FTR3)/2.
D=CONSTB*(YPM*FTR3+FTR4-TERME*FTR2)/2.
GO TO 2370
1810 IF (XPM)1570,1570,1820
1820 TERXD=BPM**2
TERMA=(XPM-BPM*YPM)**2
IF (ZPM)1830,1840,1830
1830 FTR1=ACOS((-XPM*YPM+BPM*TERMB)/SQRT(TERMA*(TERMA+ZPM2)*TERMD))*SZ
GO TO 1880
1840 IF (YPM)1850,1850,1860
1850 FTR1=0.
GO TO 1880
1860 IF (XPM-BPM*YPM)1850,1850,1870
1870 FTR1=PI
1880 P=FTR1/(4.*PI)
S=-((AES(XPM)*ZPM/TERMB-BPM*FTR1)/(4.*PI)
IF (BPM)1890,1900,1890
1890 D=(AES(XPM)*YPM/TERMB-BPM*ALOG(BPM*TERMC/SQRT(TERMA*ZPM2*TERMD)))
/(4.*PI)
GO TO 2370
1900 D=AES(XPM)*YPM/(TERMB*PI*4.)
GO TO 2370
1910 CONTINUE
C
C
VELOCITY COMPONENTS INDUCED BY WING SOURCES
ZPM=ZER
TERMAA=XIPM-BPM*YPM
TERMA=(XIPM-BPM*YPM)**2
TERMB=YPM2*ZPM2
TERMC=SQRT(TERMA)
IF (XPM)1910,1910,1920
1920 TERMD=ZPM2-1.
TERME=TERXD
IF (XIPM-TERMC)1930,1930,1940
1930 IF (TERMD)2100,1570,1570
1940 FTR1=ACOSH(XIPM/TERMC)
IF (TERMD)1950,1960,1970
1950 FTR2=ACOS((BPM*(XIPM-YPM)/SQRT(TERMA+TERMD*ZPM2))/SQRT(TERME)
GO TO 1980
1960 FTR2=SQRT(XIPM2-TERMB)/(XIPM-YPM)
GO TO 1980
1970 FTR2=ACOSH((BPM*(XIPM-YPM)/SQRT(TERMA+TERMD*ZPM2))/SQRT(TERMD)
1980 IF (ZPM)1990,2020,1990
1990 FTR3=-XIPM*YPM+BPM*TERMB)/SQRT(TERMA*(TERMA+TERMD*ZPM2))
IF (FTR3+1.0)2060,2060,2000
2000 IF (FTR3-1.0)2010,2030,2030
2010 FTR3=ACOS(FTR3)*SZ
GO TO 2070
2020 IF (YPM)2030,2030,2040
2030 FTR3=0.
GO TO 2070
2040 IF (XIPM-BPM*YPM)2030,2050,2060
2050 FTR3=PI/2.
GO TO 2070
2060 FTR3=PI*SZ
2070 IF (VSD)2090,2090,2090

```

```

00002520
00002530
00002540
00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002870
00002880
00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970
00002980
00002990
0003000
0003010
0003020
0003030
0003040
0003050
0003060
0003070
0003080
0003090
0003100
0003110
0003120
0003130
0003140
0003150
0003160

```



```

2080 P=(TERMAA*FTR2*YPM*FTR1-ZPM*FTR3)/(CHORD(NCT)*PI)
S=CONSTD*(TERMAA*(FTR1-BPM*FTR2)+BPM*ZPM*FTR3)
1-SORT(XIPM2-TERMB1)/CHORD(NCT)
D=CONSTD*(ZPM*(BPM*FTR1-TERMD*FTR2)-TERMAA*FTR3)
1/CHORD(NCT)
GO TO 2370
2090 P=FTR2/(BETA*PI)
S=(FTR1-BPM*FTR2)/PI
D=FTR3/PI
GO TO 2370
2100 IF(YPM)1570,1570,2110
2110 IF(XIPM-TERMC)2120,2130,1940
2120 IF(XIPM-BPM*YPM*SQRT(TERME)*ABS(ZPM))1570,2140,2130
2130 IF(YPM-BPM*XIPM)1570,2140,2150
2140 CT=5
GO TO 2160
2150 CT=1
2160 IF(LVSD)2170,2180,2180
2170 P=(TERMAA/SQRT(TERME)-ZPM*CT*SZ)/CHORD(NCT)
S=BPM*P*BETA
D=BETA*(TERMAA*CT*SZ-ZPM*SQRT(TERME))/CHORD(NCT)
GO TO 2370
2180 P=CT/(SQRT(TERME)*BETA)
S=BPM*P*BETA
D=CT*SZ
GO TO 2370
2190 TERMD=BPM2*1.
TERME=SQRT(TERMD)
FTR1=XIPM/TERMC
IF(FTR1)2210,2200,2200
FTR1=ASINH(FTR1)
GO TO 2220
2200 FTR1=-ASINH(-FTR1)
FTR2=(YPM*BPM*XIPM)/SQRT(TERMA+TERMD*ZPM2)
IF(FTR2)2240,2230,2230
FTR2=ASINH(FTR2)/TERME
GO TO 2250
2240 FTR2=-ASINH(-FTR2)/TERME
2250 IF(ZPM)2260,2290,2260
2260 FTR3=(BPM*TERME-XIPM*YPM)/SQRT(TERMB*(TERMA+TERMD*ZPM2))
IF(FTR3+1.)2330,2330,2270
2270 IF(FTR3-1.)2280,2300,2300
2280 FTR3=ACOS(FTR3)*SZ
GO TO 2340
2290 IF(YPM)2300,2300,2310
FTR3=0.
GO TO 2340
2310 IF(XIPM-BPM*YPM)2300,2320,2330
2320 FTR3=PI/2.
GO TO 2340
2330 FTR3=PI*SZ
2340 FTR4=SQRT(XIPM2-TERMB)
IF(LVSD)2350,2360,2360
P=(TERMAA*FTR2*YPM*FTR1-ZPM*FTR3)/(CHORD(NCT)*2.*PI)
S=CONSTD*(TERMAA*(FTR1-BPM*FTR2)+BPM*ZPM*FTR3-FTR4)/
1(2.*CHORD(NCT))
D=CONSTD*(ZPM*(BPM*FTR1-TERMD*FTR2)-TERMAA*FTR3)/CHORD(NCT)
GO TO 2370
2360 P=FTR2/(2.*BETA*PI)
S=(FTR1-BPM*FTR2)/(2.*PI)
D=FTR3/PI
2370 CONTINUE
SIM=1.
R(K)=R(K)+S*SINDT*SIM
IF(THKW.NE.1.0) GO TO 2390

```

```

IF(DELTA, EQ. 0.0. AND. ZPM. EQ. 0.0) D=0.0
GO TO 2400
2390 IF(I. EQ. J. AND. ISIDE. EQ. 1) P=0.
IF( ISIDE. GT. 1) GO TO 2400
IF( IN. LE. 0) GO TO 2400
VS2(IN)=0.
IF( J. LT. 1) GO TO 2400
NA=(IN-1)/NR+1
NB=(JN-1)/NR+1
IF( NA. EQ. NB) S=0.
IF( J. EQ. 1) VS2(IN)= .25*BPM1
IF( J. GT. 1) VS2(IN)= .25*(BPM1-BPM3)
2400 C(K)=C(K)+D*COSDT*SM*SIM
Q(K)=Q(K)-P*SM*SIM
RPM(K)=RPM(K)+S*SIM
CPM(K)=CPM(K)+D*SM*SIM
RPM(K)=RPM(K)-S*SM*SIM
CPM(K)=CPM(K)-D*SM*SM*SIM
2410 CONTINUE
2420 CONTINUE
C
U(J)=U(J)+Q(1)-Q(2)-Q(3)+Q(4)
V(J)=V(J)+(R(1)-R(2)-R(3)+R(4))
W(J)=W(J)+(C(1)-C(2)-C(3)+C(4))
VPM(J)=VPM(J)+(RPM(1)-RPM(2)-RPM(3)+RPM(4))
WPM(J)=WPM(J)+(CPM(1)-CPM(2)-CPM(3)+CPM(4))
VPM(J)=VPM(J)+(RPM(1)-RPM(2)-RPM(3)+RPM(4))
WPM(J)=WPM(J)+(CPM(1)-CPM(2)-CPM(3)+CPM(4))
2430 CONTINUE
C
IF(LVSD)2460,2440,2460
2440 DO 2450 J=1,NPANEL
UU(J)=U(J)
VV(J)=VPM(J)*COST-WPM(J)*SINT
WW(J)=WPM(J)*COST+VPM(J)*SINT
2450 A(J)=V(J)+W(J)
GO TO 2510
2460 IF(IT)2490,2490,2470
2470 DO 2480 J=1,NPANEL
US(J)=U(J)
VS(J)=VPM(J)*COST-WPM(J)*SINT
WS(J)=WPM(J)*COST+VPM(J)*SINT
2480 AS(J)=V(J)+W(J)
IF(IT)2510,2510,1080
2490 DO 2500 J=1,NPANEL
UU(J)=US(J)-U(J)*SL
VV(J)=VS(J)-(VPM(J)*COST-WPM(J)*SINT)*SL
WW(J)=WS(J)-(WPM(J)*COST+VPM(J)*SINT)*SL
2500 A(J)=AS(J)-(V(J)+W(J))*SL
C
IF(LVSD)2470,2440,2510
2510 WRITE(TAPEA)(A(J),J=1,NPANEL)
WRITE(TAPEB)(UU(J),VV(J),WW(J),J=1,NPANEL)
IF(IT)2530,2520,2530
2520 IF(LVSD)1120,2440,2530
C
C *****
C *****
2530 CONTINUE
C *****
C *****

```

```

00003830
00003840
00003850
00003851
00003852
00003853
00003854
00003855
00003856
00003857
00003858
00003859
00003860
00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003960
00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004040
00004050
00004060
00004070
00004080
00004090
00004100
00004110
00004120
00004130
00004140
00004150
00004160
00004170
00004180
00004190
00004200
00004210
00004220
00004230
00004240
00004250
00004260
00004270
00004280
00004290
00004300
00004310
00004320
00004330
00004340
00004350
00004360
00004370
00004380

```



```

JSAVE(1)=0
NSAVE(1)=NWIN
NPANEL=NWIN
NBODYS=0
NRG=1
GO TO 1070

C 1040 CONTINUE
C
C READ NUMBER OF BODY SOURCE SEGMENTS AND THE INDEX OF THE X -
C COORDINATE AT LEADING EDGE OF THE WING
C READ (NTAPEB) (XYZ(I),I=1,3),ZA,S,T
C ALPHA=XYZ(3)/XYZ(1)
C READ (NTAPEB) NBODYS,NXLE
C
C READ BODY X-COORDINATES, BODY RADIUS, AND INCREMENT OF BODY CAMBER
C READ (NTAPEB) (XB(I),R(I),ZDELTA(I),I=1,NBODYS)
C REWIND NTAPEB
C
C IF (NBODYS)1050,1280,1060
C
C BODY ONLY CASE
C KACE=2
C NPANEL=0
C NWIN=0
C NWINGS = 0
C WRITE (NTAPEB) NBODY,NWING,XMACH,SYM,KACE,THKOMP
C GO TO 1160
C
C WING AND BODY CASE
C 1060 KACE=3
C JSAVE(1)=0
C NSAVE(1)=NBODY
C JSAVE(2)=NWIN
C NSAVE(2)=NWING
C NPANEL=NWIN*NBODY
C NRG=2
C
C 1070 CONTINUE
C
C DO 1120 L=1,NRG
C J=JSAVE(L)
C N=NSAVE(L)
C
C DO 1100 I=1,N
C J=J+1
C
C READS IN PANEL COORDINATES
C READ (NTAPEB) NPN,NPART(J) (X(J,1,K),Y(J,1,K),Z(J,1,K),K=1,4)
C IF (NPART(J)-1)1080,1100,1080
C NPT=NPART(J)
C 1080 DO 1090 X=2,NPT
C READ (NTAPEB) (X(J,M,K),Y(J,M,K),Z(J,M,K),K=1,4)
C CONTINUE
C 1100 CONTINUE
C
C J=JSAVE(L)
C DO 1110 I=1,N
C J=J+1
C
C READS IN COORDINATES OF CENTROIDS, CONTROL POINTS, AREAS, THETAS,
C ALPHAS, AND CHORD LENGTHS
C READ (NTAPEB) NPN,XEAR(J),YEAR(J),ZBAR(J),XC(J),YC(J),ZC(J),AREA(J),
C 1),THETA(J),ALPHA(J),CHORD(J)

```

```

00000500
00000510
00000520
00000530
00000540
00000550
00000560
00000570
00000580
00000590
00000600
00000610
00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00010000
00010100
00010200
00010300
00010400
00010500
00010600
00010700
00010800
00010900
00011000
00011100
00011200
00011300
00011400

```

```

1110 CONTINUE
C READS IN THE NUMBER OF PANELS IN A COLUMN AND THE LOCATION OF THE
C CONTROL POINT
C READ (NTAPEC) NROW(L),XCTP
1120 CONTINUE
C IF (NEODY.NE.O) READ (NTAPEC) NTHETB
C IF (NEODY.NE.O) READ (NTAPEC) (THETB(N), N = 1, NTHETB)
C REWIND NTAPEC
C DO 1140 J=1,NWING
C JJ=J*NBODY
C STORES THICKNESS SLOPES AND CAMBER SLOPES
C ALPHAT(J)=0.0
C ALPHAC(J)=0.0
C NS=NEODY+1
1140 WRITE 1ST FILE ON TAPEC
C WRITE (NTAPEC) NEODY,NWING,XMACH,SYN,KACE,THKOMP
C
C WRITES COORDINATES OF CENTROIDS, CONTROL POINTS, AREAS, THETAS,
C ALPHAS, CHORD LENGTHS, NUMBER OF REGIONS, NUMBER OF ROWS PER
C COLUMN IN A REGION, AND CONTROL POINT LOCATION
C WRITE (NTAPEC) (I,XBAR(I),YBAR(I),ZBAR(I),XC(I),YC(I),ZC(I),AREA(100001430
C 1),THETA(I),ALPHAS(I),CHORD(I),I=1,NPANEL),NRG,(NROW(I),I=1,NRG),XC(00001440
C 2TP
C CALL FOR EOF (NTAPEC)
C
C WRITE THICKNESS SLOPES. 2ND FILE ON TAPEC
C WRITE (NTAPEC) (ALPHAT(I),I=1,NWING)
C CALL FOR EOF (NTAPEC)
C
C WRITE CAMBER SLOPES. 3RD FILE ON TAPEC
C WRITE (NTAPEC) (ALPHAC(I),I=1,NWING)
C CALL FOR EOF (NTAPEC)
C
C IF (NEODY)1160,1230,1160
1160 CONTINUE
C
C WRITE SLOPE OF BODY AXIS WITH RESPECT TO THE DEFINING AXIS
C FIRST PART OF 4TH FILE ON TAPEC
C WRITE (NTAPEC) ALPHA,DSB1,DSB2,XBS1,XBS2
C
C WRITE NUMBER OF BODY SOURCE SEGMENTS, INDEX OF X- COORDINATE AT
C LEADING EDGE OF WING, HEIGHT OF WING PLANE ABOVE BODY AXIS, X
C COORDINATE OF BODY, SECOND PART OF 4TH FILE ON TAPEC.
C WRITE (NTAPEC) NEODYS,NXLE,ZA,(XB(I),I=1,NBODYS)
C IF (NXING)1180,1170,1180
1170 CONTINUE
C
C FOR BODY ONLY CASE, READ NUMBER OF THETAS REPRESENTING BODY
C READ (NTAPEC) NDOUMY,NDUMMY,NDUMMY,NTHETB
C
C READ BODY THETAS
C READ (NTAPEC) (THETB(J),J=1,NTHETB)
C REWIND NTAPEC
1180 DO 1190 J = 1,NTHETB
1190 THETE(J) = 57.29578*THETB(J)
C IF (NWING.EQ.O) GO TO 1210
C FOR WING-BODY CASE COMPUTE THETAS FROM PANEL REPRESENTATION OF BODY
C NROWB = NROW(1)
C NTHETA = NEODY/NROWB
C DO 1200 J = 1, NTHETA
C JJ = (J-1)*NROWB+1

```

```

1200 THETAB(J) = ABS(THETA(JJ))*57.29578
C
C WRITE NUMBER OF THETAS, AND THETAS. 3RD PART OF 4TH FILE ON C
WRITE (NTAPEC) NTHETA, (THETAB(I),I=1,NTHETA)
1210 WRITE (NTAPEC) NTHETB, (THETB(I),I=1,NTHETB)
C
C WRITE RADIUS AND CAMBER INCREMENT OF BODY. LAST PART OF 4TH FILE
WRITE (NTAPEC) (R(I),I=1,NBODYS)
WRITE (NTAPEC) (ZDELTA(I),I=1,NBODYS)
CALL FOR EOF (NTAPEC)
IF (NBODY)1220,1220,1240
1220 CONTINUE
CALL FOR EOF (NTAPEC)
1230 CONTINUE
CALL FOR EOF (NTAPEC)
C
C STORE GEOMETRY DATA ON SCRATCH/SAVE TAPE
FOR USE IN FLOW VISUALIZATION LINK
1240 CONTINUE
IF (NBODY.NE.-1) NWINGS=NWING+NWING/NROW(NRG)
WRITE 5TH FILE ON TAPEC
WRITE (NTAPEC) KACE,NPANEL,NBODY,NWING,NBODYS,NWINGS
1,NROW,XMACH,SYM
CALL FOR EOF (NTAPEC)
C
C IF (NPANEL)1270,1270,1250
1250 CONTINUE
WRITE (NTAPEC) NPANEL
D) 1260 J=1,NPANEL
WRITE (NTAPEC) NPART(J)
NPT=NPART(J)
WRITE (NTAPEC) ((X(J,M,K),Y(J,M,K),Z(J,M,K),K=1,4),M=1,NPT)
1260 CONTINUE
WRITE (NTAPEC) (XBAR(J),YBAR(J),ZBAR(J),J=1,NPANEL)
WRITE (NTAPEC) (XC(J),YC(J),ZC(J),J=1,NPANEL)
WRITE (NTAPEC) (ALPHAS(J),THETA(J),CHORD(J),J=1,NPANEL)
1270 CONTINUE
CALL FOR EOF (NTAPEC)
1280 CONTINUE
C
C -----
C RETURN
C -----
1290 FORMAT(7F10.0)
END
CDECK REDUCE
OVERLAY(WOOD,4,0)
PROGRAM REDUCE
C
C .....
C REDUCE AERODYNAMIC INFLUENCE COEFFICIENTS MATRIX AND FORM THE
C (D) AND (E) MATRICES
C .....
C COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPEF,NTAPEI,
C 1 NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRW
C
C DIMENSION AB(100),ABB(100,100),ABW(100,25),AWW(110,100),AWW(110,25)
C 1),E(100,25),D(110),NSIZE(5)
C
C EQUIVALENCE (ABB(1,1),AWB(1,1))
C

```

00001840
00001850
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070
00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310

REDU1010
REDU1020
REDU1030
REDU1040
REDU1050
REDU1060

REDU1090
REDU1100
REDU1110
REDU1120
00000140
REDU1140


```

C      C      COMPUTE SIZE OF PARTIONS -
C      MAXP=25
C      CALL SIZE (NWING,MAXP,NPART,NSIZE)
C      DO 1000 J=1,NBODY
C      1000 READ (NTAPEF) (AWS(I,J),I=1,NWING)
C      CALL FSF(1,NTAPEF,IRR)
C
C      FORM (D) MATRIX
C      DO 1020 K=1,NBODY
C      READ (NTAPEF) (AB(I),I=1,NBODY)
C      DO 1010 I=1,NWING
C      D(I)=0.0
C      DO 1010 J=1,NBODY
C      D(I)=D(I)+AB(I,J)*AB(J)
C      1010 CONTINUE
C      WRITE (NTAPEF) (D(I),I=1,NWING)
C      1020 CONTINUE
C      CALL FOR EOF (NTAPEF)
C      REWIND NTAPEF
C      CALL FSF(1,NTAPEF,IRR)
C      DO 1030 J=1,NBODY
C      1030 READ (NTAPEF) (ABB(I,J),I=1,NBODY)
C
C      COPY INVERSE BODY MATRIX
C      DO 1040 J=1,NBODY
C      1040 WRITE (NTAPEF) (ABB(I,J),I=1,NBODY)
C
C      MATRIX REDUCTION
C      DO 1130 L=1,NPART
C      NS=NSIZE(L)
C      IF (L.EQ.1) GO TO 1060
C      DO 1050 J=1,NBODY
C      1050 READ (NTAPEF) (ABB(I,J),I=1,NBODY)
C      1060 REWIND NTAPEF
C      DO 1070 K=1,NS
C      1070 READ (NTAPEF) (ABW(I,K),I=1,NBODY), (AWW(I,K),I=1,NWING)
C
C      FORM (E) MATRIX
C      DO 1080 K=1,NS
C      DO 1080 M=1,NBODY
C      E(M,K)=0.
C      DO 1080 N=1,NBODY
C      E(M,K)=E(M,K)-ABB(M,N)*ABW(N,K)
C      1080 CONTINUE
C      DO 1090 J=1,NBODY
C      1090 READ (NTAPEF) (AWS(I,J),I=1,NWING)
C      CALL FSF(1,NTAPEF,IRR)
C      DO 1100 K=1,NS
C      DO 1100 I=1,NWING
C      DO 1100 M=1,NBODY
C      AWW(I,K)=AWS(I,K)+ABW(I,M)*E(M,K)
C      1100 CONTINUE
C
C      DO 1110 K=1,NS
C      1110 WRITE (NTAPEF) (E(I,K),I=1,NBODY)
C      DO 1120 K=1,NS
C      1120 WRITE (NTAPEF) (AWW(I,K),I=1,NWING)
C      1130 CONTINUE
C      REWIND NTAPEF
C      REWIND NTAPEF
C      CALL FOR EOF (NTAPEF)
C      REWIND NTAPEF

```

```

REDU1150
REDU1160
REDU1170
REDU1180
REDU1190
REDU1200
REDU1210
REDU1220
REDU1230
REDU1240
REDU1250
REDU1260
REDU1270
REDU1280
REDU1290
REDU1300
REDU1310
REDU1320
REDU1330
REDU1340
REDU1350
REDU1360
REDU1370
REDU1380
REDU1390
REDU1400
REDU1410
REDU1420
REDU1430
REDU1440
REDU1450
REDU1460
REDU1470
REDU1480
REDU1490
REDU1500
REDU1510
REDU1520
REDU1530
REDU1540
REDU1550
REDU1560
REDU1570
REDU1580
REDU1590
REDU1600
REDU1610
REDU1620
REDU1630
REDU1640
REDU1650
REDU1660
REDU1670
REDU1680
REDU1690
REDU1700
REDU1710
REDU1720
REDU1730
REDU1740
REDU1750
REDU1760
REDU1770
REDU1780
REDU1790

```



```

C      CALL FSF(1,NTAPEA,IRR)
      DO 1020 J=1,NWING
      READ (NTAPEB) (U(I),V(I),W(I),I=1,NBODY), (UU(I),VV(I),WW(I),I=1,NWING)
      WRITE (NTAPEB) (U(I),V(I),W(I),I=1,NBODY)
      WRITE (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)
1020 CONTINUE
C
      REWIND NTAPEA
      REWIND NTAPEB
      CALL FOR EOF (NTAPEB)
      CALL FSF(1,NTAPEA,IRR)
C
      DO 1030 J=1,NWING
      READ (NTAPEA) (UU(I),VV(I),WW(I),I=1,NWING)
      WRITE (NTAPEB) (UU(I),VV(I),WW(I),I=1,NWING)
1030 CONTINUE
      CALL FOR EOF (NTAPEB)
      REWIND NTAPEA
      REWIND NTAPEB
C
C -----
C -----
C -----
CDECK WOOD60
      OVERLAY(WOOD,6,0)
      PROGRAM WOOD60
      COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1      NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRW
      COMMON /TRANSFER/ IOVR10,IOVR60,IOVR70
      COMMON /COM60/ ISAVET
      IF (IOVR60.EQ.2) GO TO 100
      CALL SAVTAP(ISAVET)
      GO TO 999
100 CALL USETAP
999 CONTINUE
      END
CDECK SAVTAP
      SUBROUTINE SAVTAP(ISAVET)
C
C ..... WRITES AERODYNAMIC MATRICES ON A LOGICAL TAPE FOR FUTURE USE .....
C .....
C .....
1      COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
      NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRW
      COMMON /MTHICK/THKW
      DIMENSION A(210),B(210),C(210)
      DIMENSION DUX(10),NROW(2)
C
      IF (ISAVET)1010,1010,1000
1000 READ (NTAPEC)NBODY,NWING,XMACH,SYM,KACE,THKW
C *****
C      GO TO (1020,1010,1020),KACE
C
1010 CALL FSF(6,NTAPEC,IRR)
      GO TO 1090
1020 NPANEL=NBODY+NWING
      READ (NTAPEC) ( M, ( DUM(J), J=1,10), I=1,NPANEL), NRG,
1      (NROW(I), I=1, NRG), DUMMY
      NCOL=NWING/NROW(NRG)
      CALL FSF(6,NTAPEC,IRR)
      GO TO (1030,1090,1060),KACE

```

PART1310
 PART1320
 PART1330
 PART1340
 PART1350
 PART1360
 PART1370
 PART1380
 PART1390
 PART1400
 PART1410
 PART1420
 PART1430
 PART1440
 PART1450
 PART1460
 PART1470
 PART1480
 PART1490
 PART1500
 PART1510
 PART1520
 PART1530
 PART1550

SAVT1000
 SAVT1010
 SAVT1020
 SAVT1030
 SAVT1040
 SAVT1050

 SAVT1080
 SAVT1090
 SAVT1100
 SAVT1110
 SAVT1120
 SAVT1130
 SAVT1140
 SAVT1150
 SAVT1160
 SAVT1170
 SAVT1180
 SAVT1190
 SAVT1200

 SAVT1220
 SAVT1230
 SAVT1240
 SAVT1250


```

COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPEF,NTAPEE,NTAPEF,NTAPEI,
1 NTAPEO,NBODY,NWING,XMACH,SYN,KACE,NPOLAR,IRW
COMMON /NTHICK/THKM
DIMENSION A(210),B(210),C(210)
DIMENSION DUM(10),NROX(2)

C
C
C READ(NTAPEC)NBODY,NWING,XMACH,SYN,KACE,THKM
GO TO (1000,1070,1000),KACE
1000 NPAPEL=NBODY,NWING
READ (NTAPEC) (M, (DUM(J), J=1,10), I=1,NPAPEL), MRG,
1(NROW(I), I=1,NRG),DUMMY
NCOL=NWING/NROX(NRG)
CALL FSF( 6,NTAPEC,IRR)

C
C GO TO (1010,1070,1040),KACE
1010 IF (THKM .EQ. 0.) GO TO 1020
CALL TTAPE(0,NWING,NWING+NCOLW,NTAPEC,NTAPEA,A,B,C)
1020 CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING+1,NWING+1,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING+2,NWING+2,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
REXIND NTAPEA
IF (THKM .EQ. 0.) GO TO 1030
CALL TTAPE(1,NWING,NWING+NCOLW,NTAPEC,NTAPEB,A,B,C)
1030 CALL FOR EOF (NTAPEB)
CALL TTAPE(1,NWING,NWING,NTAPEC,NTAPEB,A,B,C)
CALL FOR EOF (NTAPEB)
REXIND NTAPEB
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
CALL FOR EOF (NTAPEE)
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
CALL FOR EOF (NTAPEE)
REXIND NTAPEE
GO TO 1070
1040 IF (THKM .EQ. 0.) GO TO 1050
CALL TTAPE(0,NPAPEL,NWING +NCOLW,NTAPEC,NTAPEA,A,B,C)
1050 CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING+1,NWING+1,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
CALL TTAPE(0,NWING+2,NWING+2,NTAPEC,NTAPEA,A,B,C)
CALL FOR EOF (NTAPEA)
REXIND NTAPEA
IF (THKM .EQ. 0.) GO TO 1060
CALL TTAPE(1,NPAPEL,NWING +NCOLW,NTAPEC,NTAPEB,A,B,C)
1060 CALL FOR EOF (NTAPEB)
REXIND NTAPEB
CALL TTAPE(1,NBODY,NBODY,NTAPEC,NTAPED,A,B,C)
CALL FOR EOF (NTAPED)
CALL TTAPE(1,NWING,NBODY,NTAPEC,NTAPED,A,B,C)
CALL FOR EOF (NTAPED)
CALL TTAPE(1,NBODY,NWING,NTAPEC,NTAPED,A,B,C)
CALL FOR EOF (NTAPED)
CALL TTAPE(1,NWING,NWING,NTAPEC,NTAPED,A,B,C)
CALL FOR EOF (NTAPED)
REXIND NTAPED
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)
CALL FOR EOF (NTAPEE)
CALL TTAPE(0,NWING,NWING,NTAPEC,NTAPEE,A,B,C)

```

```

USFT1080
USFT1090
USFT1100
USFT1110
USFT1120
USFT1130
USFT1140
USFT1150
USFT1160
USFT1180
USFT1190
USFT1200
USFT1210
USFT1220
USFT1230
USFT1240
USFT1250
USFT1260
USFT1270
USFT1280
USFT1290
USFT1300
USFT1310
USFT1320
USFT1330
USFT1340
USFT1350
USFT1360
USFT1370
USFT1380
USFT1390
USFT1400
USFT1410
USFT1420
USFT1430
USFT1440
USFT1450
USFT1460
USFT1470
USFT1480
USFT1490
USFT1500
USFT1510
USFT1520
USFT1530
USFT1540
USFT1550
USFT1560
USFT1570
USFT1580
USFT1590
USFT1600
USFT1610
USFT1620
USFT1630
USFT1640
USFT1650
USFT1660
USFT1670
USFT1680
USFT1690
USFT1700

```


0000000060	0000000090	0000000090
0000000090	000000100	000000100
000000110	000000110	000000110
000000120	000000130	000000130
000000130	000000140	000000140
000000150	000000170	000000170
000000180	000000180	000000180
000000210	000000210	000000210
000000230	000000230	000000230
000000260	000000260	000000260
000000290	000000290	000000290
000000330	000000330	000000330
000000340	000000340	000000340
000000350	000000350	000000350
000000360	000000360	000000360
000000410	000000410	000000410
000000430	000000430	000000430
000000440	000000440	000000440
000000450	000000450	000000450
000000460	000000460	000000460
000000470	000000470	000000470
000000480	000000480	000000480
000000490	000000490	000000490
000000500	000000500	000000500
000000510	000000510	000000510
000000520	000000520	000000520
000000530	000000530	000000530
000000540	000000540	000000540
000000550	000000550	000000550
000000560	000000560	000000560
000000570	000000570	000000570
000000580	000000580	000000580
000000590	000000590	000000590
000000600	000000600	000000600
000000610	000000610	000000610
000000620	000000620	000000620
000000630	000000630	000000630
000000640	000000640	000000640

```

THICK =0.
THICK =1.
VOUT = 0.
VOUT = 1.
XNACEL =0.
XNACEL =X.
XNACEL =-X.
RFAREA =0.
RFAREA =X.
XP,ZP
CBAR
SEMIS
KONFIG=KACE
NPNEL=NWING+NBODY
NS=NBODY+1
CDR=57.2957795
IF ( IRW .EQ. 2 ) GO TO 1111
IF ( KONFIG-2)1000,1910,1000
READ (NTAPE) NBODY,NWING,XMACH,SYM,KACE
READ (NTAPE) (J,XBAR(I),YBAR(I),ZBAR(I),XC(I),YC(I),ZC(I),AREA(I),
1) THETA(I),ALPHA(I),CHORD(I),I=1,NPNEL),MRG,(NROW(I),I=1,NRG),RAN
2) FOX
REXIND NTAPEC
1010 CONTINUE
NACEL=0
READ CARD SA
READ (NTAPE,1700)CASE,CPCALC,POLAR,THICK,XNACEL,PINF,PUNCH,
1 SOLID,WING,(SID(K),K=1,20),(IFORM(I),K=1,10)
IPUNCH = IFIX( PUNCH )
ISOLID = IFIX( SOLID )
NWG = IFIX( WING )
ANCL=ABS(XNACEL)
NACEL=ANCL
NUMBOD=0
IF (NEODY.NE.0) NUMBOD=1
XNGS(1)=0.
YNGS(1)=0.
ZNGS(1)=0.
NESTAT(1)=NBODYS
IPOLAR=0
POLAR = POLAR + 1
IF (CASE)1020,1680,1020
1020 CONTINUE

```



```

C RE'D CARD 6A
IF (NACEL)1120,1100,1030
1030 DO 1090 N=1,NACEL
      NDUM=NUMBOD+N
C
C READ CARD 6S1
READ (NTAPEI,1700) XNI(N),YNI(N),ZNI(N),XNXN(N),XNTN(N),ARN(N)
XNOS(NDUM)=XNI(N)
YNOS(NDUM)=YNI(N)
ZNOS(NDUM)=ZNI(N)
IF (NACEL)1040,1090,1050
1040 IF (N-1)1060,1050,1060
1050 NXN=XNXN(N)
      NSTAT(NDUM)=NXN
      NTN=XNTN(N)
C
C READ CARD 6S2
READ (NTAPEI,1700) (XN(M,N),M=1,NXN)
C READ CARD 6S3
READ (NTAPEI,1700) (RN(M,N),M=1,NXN)
C READ CARD 6S4
READ (NTAPEI,1700) (ZDN(M,N),M=1,NXN)
C READ CARD 6S5
READ (NTAPEI,1700) (THETAN(M,N),M=1,NTN)
C READ CARD 6S6
READ (NTAPEI,1700) XNS1(N),XNS2(N),DS1(N),DS2(N), ( DRNDX(J,N),
1 DRNDX(J,N),J=1,NXN)
NS1(N)=XNS1(N)
NS2(N)=XNS2(N)
GO TO 1090
C
C DO 1070 M=1,NXN
  XN(M,N)=XN(M,1)
  RN(M,N)=RN(M,1)
  ZDN(M,N)=ZDN(M,1)
C
C DO 1080 M=1,NTN
  THETAN(M,N)=THETAN(M,1)
C
  NS1(N)=NS1(1)
  NS2(N)=NS2(1)
  DS1(N)=DS1(1)
  DS2(N)=DS2(1)
C
C 1090 CONTINUE
  NUMBOD=NUMBOD+NACEL
  DO 1110 N=1,2
    XNCL(N)=0.
    XNCD(N)=0.
    XNCM(N)=0.
    DO 1110 J=1,NPANEL
      UNCL(J,N)=0.
      VNCL(J,N)=0.
      WNCL(J,N)=0.
      ANIN(J,N)=0.
  1110 CONTINUE
C
  1120 CONTINUE
  IF (CBAR.EQ.0.) CBAR=1.
  IF (SEMIS.EQ.0.) SEMIS=1.
C
  IF (VOUT)1130,1150,1130
  1130 CONTINUE
  DO 1140 J=1,9
  1140 NFRT(J)=J
      GO TO 1170
00001250
00001270
00001280
00001290
00001300
00001310
00001320
00001321
00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001790
00001800
00001810
00001820
00001830
00001840
00001850
00001860
00001870
00001880

```

```

1150 CONTINUE
DO 1160 J=1,9
1160 NFNT(J)=0
1170 CONTINUE
KASE=CASE
C
1180 IF (KONFIG-2)1200,1190,1200
1190 RFAREA=1.0
GO TO 1220
1200 RFAREA=0.0
DO 1210 J=NS,NPANEL
1210 RFAREA=RFAREA+AREA(J)
1220 CONTINUE
C
WRITE CASE DATA
CALL INOUT(NTAPEO,KASE,CPCALC,POLAR,THICK,VOUT,XMACH,SEMI,
1XP,ZP,CEAR,RFAREA,SYM)
C
C
ANY CONFIGURATION
IF (KONFIG.EQ.1) GO TO 1280
C
BODY ALONE OR WING-BODY CONFIGURATION
NROWB=NROW(1)
C
IF (KONFIG-2)1240,1240,1250
C
BODY ALONE CONFIGURATION
1240 READ (NTAPEC) NEODY,NWING,XMACH,SYM,KACE
GO TO 1260
C
WING-BODY CONFIGURATION
1250 CALL FSF(3,NTAPEC,IRR)
1260 CONTINUE
READ (NTAPEC) ALPHA,DSB1,DSB2,XBS1,XBS2
NE1 = XBS1
NE2 = XBS2
READ (NTAPEC) NEODYS,NXLE,ZA (XB(1),I=1,NBODYS)
IF (KONFIG.EQ.2) GO TO 1270
READ (NTAPEC) NTHETA,(THETAB(I),I=1,NTHETA)
C
INPUT BODY VARIABLES
1270 READ (NTAPEC) NTHETB,(THETB(I),I=1,NTHETB)
C
READ CARD 7A
READ (NTAPE1,1700) ARE, DADEG
C
READ CARD 8A
READ (NTAPEC) ( R(I), I=1,NBODYS )
C
READ CARD 9A
READ (NTAPEC) ( ZDELTA(I), I=1,NBODYS )
REWIND NTAPEC
C
REMAX = R(1)
DO 1271 I=2,NBODYS
REMAX = AMAX1( REMAX, R(I) )
1271 CONTINUE
C
IF ( KONFIG .EQ. 2 ) RFAREA = 3.14159 * REMAX**2
IF ( KONFIG .EQ. 2 ) WRITE (NTAPEO,1780) RFAREA
C
ARA=-ALPHA+ARB/CDR
WRITE (NTAPEO,1770) ZA
C
IF (KONFIG.EQ.2) GO TO 1290
C

```

00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070
00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310
00002320
00002330
00002340
00002350
00002370
00002400
00002420

00002430
00002440
00002450
00002460
00002470
00002480

```

C WING-BODY CONFIGURATION
CALL BCAM(NSOC'S,NROXB,XB,ZDELTA,XC,DIDXB,ACB)
CALL BTICK(NBODY'S,NRODY,XB,R,XC,ALPHA,ALPHAS)
C
C 1280 WING ALONE OR WING-BODY CONFIGURATION
CONTINUE
NROXX=NROX(NRG)
NCOLX=NWING/NROXX
C IF (KONFIG.EQ.3) GO TO 1290
C
C WING ALONE CONFIGURATION
ALPHA=0.
ARA=0.
C
C 1290 ANY CONFIGURATION
CONTINUE
CALL FSF(7,NTAPEC,IRR)
WRITE (NTAPEC) THICK,ARA
CALL FOR EOF (NTAPEC)
REWIND NTAPEC
ALPHA=ALPHA+CDR
ARADEG=ARA+CDR
WRITE (NTAPEC,1750) ALPHA
WRITE (NTAPEC,1760) ARADEG
C IF (KONFIG.EQ.2) GO TO 1400
C
C WING ALONE OR WING-BODY CONFIGURATION
INPUT WING VARIABLES
GO TO (1300,1320,1370),KASE
C
C 1300 READ CARD 10A
CONTINUE
ICAM =Z
CALL READ(NTAPEI,NTAPEO,NTAPEC,NWING,CL(NS),KACE,ICAM,NROW)
DO 1310 J=NS,NPANEL
1310 CL(J)=-CL(J)
GO TO 1390
C
C 1320 READ CARD 11A
CONTINUE
IF (KONFIG.EQ.1) READ (NTAPEI,1700) DUM,DADEG
READ (NTAPEI,1700) ARW,TWIST
IF (TWIST.NE.0.) GO TO 1340
DO 1330 J=1,NCOLW
1330 ARWT(J)=0.0
GO TO 1350
C
C 1340 READ CARD 11A
READ (NTAPEI,1700) (ARWT(I),I=1,NCOLW)
1350 CONTINUE
CALL FSF (2,NTAPEC,IRR)
C
C 1360 READ CARD 12A
ICAM=2
CALL READ(NTAPEI,NTAPEO,NTAPEC,NWING,ALPHA,KACE,ICAM,NROW)
REWIND NTAPEC
DO 1360 J=1,NWING
JJ=(J-1)/NROXX+1
JX=J-NBODY
COST=COS(THETA(JX))
ALPHA(J)=ALPHA(JJ)-ARA+CDR-(ARW+ARWT(JJ))/CDR
GO TO 1390
C

```

```

00002490
00002500
00002510
00002520
00002530
00002540
00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810

00002830
00002840
00002850
00002860
00002870

00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970
00002980
00002990

00003010
00003020
00003030
00003038
00003039
00003040
00003050
00003060

```



```

C      READ CARD 13A
1370 READ (NTAPE1,1700) CONSNT,CLBAR,XCPEAR
      IF (CONSNT.NE.0.) GO TO 1380
      WRITE (NTAPE0,1730) CLBAR
      GO TO 1390
1380 WRITE (NTAPE0,1730) CLBAR
      WRITE (NTAPE0,1740) XCPEAR
1390 CONTINUE
C
C      WING ALONE OR WING-BODY CONFIGURATION
      IF (THICK)1430,1400,1430
C
1400 CONTINUE
      CALL FSF(8,NTAPE0,IRR)
      CALL FOR EOF (NTAPE0)
      REWIND NTAPE0
      IF (KONFIG.EQ.2) GO TO 1480
C
      DO 1420 J=1,NPANEL
1420 ALPHA(J)=0.
      DO 1425 J=1,NWING
1425 AAS(J)=0.
      IF (KONFIG.EQ.1) GO TO 1460
      GO TO 1440
C
C      WING ALONE OR WING-BODY CONFIGURATION
1430 CONTINUE
C
      READ CARD 14A
      CALL TVEL(A,B,C,D,ALPHAT,UBWT,VBWT,WBWT,UBWT,VBWT,WBWT,UBWT,VBWT,WBWT,
1ALPHA,CHORD,THICK,NROW)
      REWIND NTAPE0
C
      DO 1455 J=1,NWING
      JJ=J+NBODY
1455 AAS(J)=ALPHA(JJ)
      IF (KONFIG.EQ.1) GO TO 1460
C
C      WING-BODY CONFIGURATION
1440 DO 1450 J=1,NBODY
      JJ=J-((J-1)/NROWB)*NROWB
      ALPHA(J)=ALPHAS(JJ)-(ARA
      AAS(J)=-ALPHA(J)
      ABT(J)=ABX(J)
1450 CONTINUE
C
C      ANY CONFIGURATION
1460 CONTINUE
      DO 1470 J=1,NWING
      UBWT(J)=0.
      VBWT(J)=0.
      WBWT(J)=0.
1470 ALPHA(J)=0.
C
1480 CONTINUE
      CALL FSF(9,NTAPE0,IRR)
      WRITE(NTAPE0) NUNREOD,(YNGS(I),ZNGS(I),NBSTAT(I),I=1,NUNREOD)
      IF (KONFIG.EQ.1) GO TO 1620
C
C      BODY ALONE OR WING-BODY CONFIGURATION
C
1490 XNOS = XB(1)
      IF (XNOS-1.)1500,1620,1510
1500 CALL OVERLAY(4,XNOS,7,5)

```

```

00003070
00003080
00003090
00003100
00003110
00003120
00003130
00003140
00003150
00003160
00003170
00003180
00003190
00003200
00003210
00003220
00003230
00003240
00003250
00003260
00003270
00003280
00003281
00003282
00003283
00003290
00003300
00003310
00003320
00003330
00003340
00003350
00003360
00003370
00003380
00003390
00003391
00003392
00003393
00003400
00003410
00003420
00003430
00003440
00003450
00003460
00003470
00003480
00003490
00003500
00003510
00003520
00003530
00003540
00003550
00003560
00003570
00003580
00003590
00003600
00003630
00003640
00003650
00003659
00003660

```

```

GO TO 1560
C 1510 CALL OVERLAY(4HWANG, 7, 6)
C 1560 CONTINUE
IF (NEODY) 1590, 1590, 1570
1570 DO 1580 J=1, NEODY
1580 ABX(J)=ABT(J)-AN1N(J,2)
1590 IF (N1NG) 1620, 1620, 1600
1600 DO 1610 J=1, N1NG
JJ=J+NEODY
1610 ALPHAX(J)=ALPHAX(J)+AN1N(JJ,1)+AN1N(JJ,2)
1620 CONTINUE
IF (N1NG.LE.0) GO TO 1628
DO 1625 J=1, N1NG
1625 ALPHAX(J)=ALPHAX(J)+AWS(J)
1628 CONTINUE
CALL FOR EOF(NTAPEC)
REWIND NTAPEC
C ANY CONFIGURATION
C CALL OVERLAY(4HWANG, 7, 7)
C 1111 CONTINUE
IF ( IRM .GT. 0 ) CALL OVERLAY(4HWANG, 7, 11)
C IF ( KONFIG .LT. 3 ) GO TO 1800
C ADDING PRESSURE DUE TO THE PRESENCE OF WING TO BODY PANEL
C CALL OVERLAY(4HWANG, 7, 9)
C 1800 CONTINUE
C NSYM = 1
C GO TO ( 1820, 1810, 1810 ), KONFIG
C INTERPOLATION OF PRESSURE
C 1810 CONTINUE
C BODY
C CALL OVERLAY(4HWANG, 7, 8)
C IF ( KONFIG .EQ. 3 ) NSYM = NSYM + 1
C IF ( KONFIG .EQ. 2 ) GO TO 1840
C 1820 CONTINUE
C WING
C CALL OVERLAY (4HWANG, 7, 10)
C 1840 CONTINUE
C NPOLAR = 1
C ANY CONFIGURATION
C READ ADDITIONAL POLARS
C IF ( POLAR ) 1630, 1680, 1630

```

00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003951
00003952
00003953
00003954
00003960
00003970
00003980
00003990

00004010
00004020


```

1110 CONTINUE
CALL FSF(8,NTAPEC,IRR)
WRITE (NTAPEC) NWINC
DO 1118 J=1,NC
J1=(J-1)*NR
DO 1116 I=1,NR
IJ=I+J1
IF(I.EQ.1) GO TO 1114
WS(IJ)=(ALPHAT(IJ-1)+ALPHAT(IJ))*0.5
GO TO 1116
1114 WS(IJ)=(ATLE(J)+ALPHAT(IJ))*0.5
1116 CONTINUE
1118 CONTINUE
DO 1170J=1,NWINC
READ (NTAPEC) (D(I),I=1,NPANEL)
READ (NTAPEB) (A(I),B(I),C(I),I=1,NPANEL)
JT=J-N*(NR+1)
IF (JT)1130,1130,1120
1120 N=N+1
WT=ATLE(N)
GO TO 1140
1130 JN=J-N
1140 WT=ALPHAT(JN)
CONTINUE
WRITE (NTAPEC) WT
DO 1160 I=1,NPANEL
IF (I.GT. NBODY) GO TO 1150
UEXT(I)=UEXT(I)+A(I)*WT
VEXT(I)=VEXT(I)+B(I)*WT
WEXT(I)=WEXT(I)+C(I)*WT
AN(I)=AN(I)+D(I)*WT
GO TO 1160
1150 IN=I-NBODY
UXWT(IN)=UXWT(IN)+A(I)*WT
VXWT(IN)=VXWT(IN)+B(I)*WT
WXWT(IN)=WXWT(IN)+C(I)*WT
AN(I)=AN(I)+D(I)*WT
1160 CONTINUE
1170 CONTINUE
C
1180 CONTINUE
CALL FOR EOF (NTAPEC)
REWIN NTAPEC
C
C -----
C RETURN
C -----
C
1190 FORMAT (7F10.0)
END
CDECK READ
SUBROUTINE READ(NTAPEI,NTAPEC,NTAPEB,NM,S,KACE,ICAMBR,NROW)
C
C ..... CONTROLS DATA READ IN OPTION FOR SPECIFYING WING CAMBER AND
C PRESSURE DISTRIBUTION, ALSO BODY CAMBER
C .....
C
C DIMENSION NROW(2)
C
C REAL S(1)
C INTEGER DICT(2)
C
C DATA DICT(1)/4HCOMS/
C DATA DICT(2)/4H$IVE/

```

```

00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920
00000930
00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130

```

```

READ1010
READ1020
READ1030
READ1040
READ1050
READ1060
READ1070
READ1080
READ1090
READ1100
READ1110
READ1120
READ1130

```

```

C
C      ICORER = 1  CONSTANT CAMBER, 2  COMPUTED, 3  READ IN
      GO TO ( 1060, 1080, 1000), ICORER
1000 CONTINUE
      IF (KACE .NE. 0) GO TO 1010
      READ (NTAPEI,1100) (S(I),I=1,NM)
      GO TO 1090
C
1010 GO TO (1020,1090,1030), KACE
1020 NC = NX / NROW(1)
      NR = NROW(1)
      GO TO 1040
1030 NC = NX / NROW(2)
      NR = NROW(2)
1040 K = -NR + 1
      DO 1050 I=1,NC
        K = K+NR
        KK = K+NR - 1
        READ (NTAPEI,1100) (S(J),J=K,KK)
1050 CONTINUE
      GO TO 1090
C
1060 CONTINUE
      READ (NTAPEI,1100) SCONST
      DO 1070 I=1,NM
        S(I)=SCONST
      GO TO 1090
1080 CONTINUE
      READ (NTAPEI) (S(I),I=1,NM)
1090 CONTINUE
C
C      -----
      RETURN
C      -----
1100 FORMAT(7F10.0)
      END
CDECK BTHICK
      SUBROUTINE BTHICK(NBODY,NBODY,NROW,XB,R,XC,ALPHA,THETA)
C
C      .....
C      COMPUTES BODY THICKNESS SLOPES FOR GIVEN BODY RADII DISTRIBUTION
C      .....
C
      DIMENSION XB(1),R(1),XC(1),ALPHA(1),THETA(1)
C
      NB=NBODYS-1
      NCOL=NBODY/NROW
C
      DO 1000 I=1,NB
        ALPHA(I+1)=(R(I+1)-R(I))/(XB(I+1)-XB(I))
        ALPHA(1)=ALPHA(2)
        DO 1030 J=1,NROW
          DO 1010 I=1,NB
            IF (XB(I)-XC(J))1010,1020,1020
          I=NBODYS
1010 CONTINUE
1020 THETA(J)=ALPHA(I-1)+(XC(J)-XB(I-1))/(XB(I)-XB(I-1))*(ALPHA(I)-
          1*ALPHA(I-1))
1030 CONTINUE
C
      DO 1040 J=1,NROW
        DO 1040 I=2,NCOL
          I=(I-1)*NROW+J
          THETA(IJ)=THETA(J)
1040 CONTINUE

```

READ1140

READ1180
READ1190
READ1200
READ1210
READ1220
READ1230
READ1240
READ1250
READ1260
READ1270
READ1280
READ1290
READ1300
READ1310
READ1320
READ1330
READ1340
READ1350
READ1360
READ1370
READ1380
READ1390
READ1400
READ1410
READ1420
READ1430
READ1440
READ1450
READ1460
READ1470
READ1480
READ1490

BTHI1000
BTHI1010
BTHI1020
BTHI1030
BTHI1040
BTHI1050
BTHI1060
BTHI1070
BTHI1080
BTHI1090
BTHI1100
BTHI1110
BTHI1120
BTHI1130
BTHI1140
BTHI1150
BTHI1160
BTHI1170
BTHI1180
BTHI1190
BTHI1200
BTHI1210
BTHI1220
BTHI1230
BTHI1240
BTHI1250
BTHI1260
BTHI1270


```

C -----
C RETURN
C -----
C END
CDECK BCAM
C SUEROUTINE BCAM(NBODYS,NROWB,XB,ZDELTA,XC,DZDXB,ACB)
C .....
C COMPUTES BODY CAMBER SLOPES, GIVEN BODY CAMBER SHAPE
C .....
C DIMENSION XB(1),ZDELTA(1),XC(1),DZDXB(1),ACB(1)
C
C NE=NBODYS-1
C DO 1000 I=1,NB
C   DZDXB(I+1)=(ZDELTA(I+1)-ZDELTA(I))/(XB(I+1)-XB(I))
C   DZDXB(1)=DZDXB(2)
C
C DO 1030 J=1,NROWB
C   DO 1010 I=1,NB
C     IF (XB(I)-XC(J))1010,1020,1020
C   1010 CONTINUE
C   1020 ACB(J)=DZDXB(I-1)*(XC(J)-XB(I-1))/(XB(I)-XB(I-1))*(DZDXB(I)-DZDXB(I-1))
C   1030 CONTINUE
C
C RETURN
C -----
C END
CDECK INOUT
C SUEROUTINE INCUT(NTAPE0,KASE,CPCALC,POLAR,THICK,VOUT,XMACH,SEMS,
C 1XP,ZP,CBAR,RFAREA,SYM)
C .....
C PRINTS OUT ALL INPUT AERODYNAMIC DATA
C .....
C
C WRITE (NTAPE0,1200)
C IF (SYM)1010,1000,1010
C 1000 WRITE (NTAPE0,1210)
C   GO TO 1020
C 1010 WRITE (NTAPE0,1220)
C 1020 CONTINUE
C
C   GO TO (1030,1040,1050),KASE
C 1030 WRITE (NTAPE0,1230)
C   GO TO 1060
C 1040 WRITE (NTAPE0,1240)
C   GO TO 1060
C 1050 WRITE (NTAPE0,1250)
C 1060 CONTINUE
C
C IF (CPCALC-1)1070,1080,1090
C 1070 WRITE (NTAPE0,1260)
C   GO TO 1100
C 1080 WRITE (NTAPE0,1270)
C   GO TO 1100
C 1090 WRITE (NTAPE0,1280)
C 1100 CONTINUE
C
C IF (POLAR)1120,1110,1120
C 1110 WRITE (NTAPE0,1290)

```

BTH11280
 BTH11290
 BTH11300
 BTH11310

BCAM1000
 BCAM1010
 BCAM1020
 BCAM1030
 BCAM1040
 BCAM1050
 BCAM1060
 BCAM1070
 BCAM1080
 BCAM1090
 BCAM1100
 BCAM1110
 BCAM1120
 BCAM1130
 BCAM1140
 BCAM1150
 BCAM1160
 BCAM1170
 BCAM1180
 BCAM1190
 BCAM1200
 BCAM1210
 BCAM1220
 BCAM1230

INOU1000
 INOU1010
 INOU1020
 INOU1030
 INOU1040
 INOU1050
 INOU1060
 INOU1070
 INOU1080
 INOU1090
 INOU1100
 INOU1110
 INOU1120
 INOU1130
 INOU1140
 INOU1150
 INOU1160
 INOU1170
 INOU1180
 INOU1190
 INOU1200
 INOU1210
 INOU1220
 INOU1230
 INOU1240
 INOU1250
 INOU1260
 INOU1270
 INOU1280
 INOU1290
 INOU1300
 INOU1310
 INOU1320


```

C DO 200 I=1, NE
  READ (5, 901) ICHECK, ID, IE, ND, NG1, NG2, NG3, FG4, DM
  NLM(1) = IE
  NG4 = FG4

C SEARCH GRID POINT NUMBER
  ICOUNT = 1
  DO 170 K=1, NGRIDP
    IF ( NG(K) ) .EQ. NG1 ) GO TO 101
    IF ( NG(K) ) .EQ. NG2 ) GO TO 102
    IF ( NG(K) ) .EQ. NG3 ) GO TO 103
    IF ( NG(K) ) .EQ. NG4 ) GO TO 104
    GO TO 110
  101 I1 = K
    GO TO 109
  102 I2 = K
    GO TO 109
  103 I3 = K
    GO TO 109
  104 I4 = K
    GO TO 150
  109 IF ( ICOUNT .EQ. 4 ) GO TO 150
    IF ( ICOUNT .EQ. 3 .AND. ICHECK .NE. IWORD1 ) GO TO 111
    ICOUNT = ICOUNT + 1
  110 CONTINUE

C TRIANGULAR ELEMENT
  111 CONTINUE
  DO 120 J=1, 3
    XC(J, I) = ( X( J, I1 ) + X( J, I2 ) + X( J, I3 ) ) / 3.0
  120 CONTINUE
  GO TO 200

C QUADRILATERAL ELEMENT
  150 CONTINUE
  X1 = ( X( 1, I1 ) + X( 1, I2 ) + X( 1, I3 ) ) / 3.0
  Y1 = ( X( 2, I1 ) + X( 2, I2 ) + X( 2, I3 ) ) / 3.0
  Z1 = ( X( 3, I1 ) + X( 3, I2 ) + X( 3, I3 ) ) / 3.0
  X2 = ( X( 1, I3 ) + X( 1, I4 ) + X( 1, I1 ) ) / 3.0
  Y2 = ( X( 2, I3 ) + X( 2, I4 ) + X( 2, I1 ) ) / 3.0
  Z2 = ( X( 3, I3 ) + X( 3, I4 ) + X( 3, I1 ) ) / 3.0

  S12 = SQRT( ( X(1, I1) - X(1, I2) )**2 + ( X(2, I1) - X(2, I2) )**2
    + ( X(3, I1) - X(3, I2) )**2 )
  S23 = SQRT( ( X(1, I2) - X(1, I3) )**2 + ( X(2, I2) - X(2, I3) )**2
    + ( X(3, I2) - X(3, I3) )**2 )
  S31 = SQRT( ( X(1, I3) - X(1, I1) )**2 + ( X(2, I3) - X(2, I1) )**2
    + ( X(3, I3) - X(3, I1) )**2 )
  S34 = SQRT( ( X(1, I3) - X(1, I4) )**2 + ( X(2, I3) - X(2, I4) )**2
    + ( X(3, I3) - X(3, I4) )**2 )
  S41 = SQRT( ( X(1, I4) - X(1, I1) )**2 + ( X(2, I4) - X(2, I1) )**2
    + ( X(3, I4) - X(3, I1) )**2 )
  S123 = 0.5 * ( S12 + S23 + S31 )
  S1341 = 0.5 * ( S31 + S34 + S41 )
  A123 = SQRT( S123 * ( S123 - S12 ) * ( S123 - S23 ) + ( S123 - S31 ) )
  A341 = SQRT( S1341 * ( S1341 - S31 ) * ( S1341 - S34 ) + ( S1341 - S41 ) )
  AT = A123 + A341
  XC(1, I) = ( X1 * A123 + X2 * A341 ) / AT
  XC(2, I) = ( Y1 * A123 + Y2 * A341 ) / AT
  XC(3, I) = ( Z1 * A123 + Z2 * A341 ) / AT

C 200 CONTINUE

```



```

C 901 FORMAT ( A5, A3, I8, F8.0, F8.4 )
C
RETURN
END
CDECK CONV
SUBROUTINE CONV( X, NG, NGRIDP, NSYM, ISYM)
C
C
C      CONVERT GRID POINT COORDINATES TO THE RECTANGULAR COORD.
C
C      DIMENSION X( 3, NGRIDP), NG(NGRIDP), ISYM(20)
C
C      DR = 0.0174532925
C
C      DO 250 I = 1, NGRIDP
C
C          READ OUTPUT OF BING FINITE ELEMENT GRID POINT COORDINATE
C
C          READ (5, 901) CHECK, IDUM, NG(I), NS, Y1, X2, X3, ND
C          R = X1
C          THETA = X2
C          PHI = X3
C          NGO = ISYM(NSYM) + 1
C          GO TO ( 100, 150, 200 ), NGO
C
C          RECTANGULAR COORD.
C
C      100 CONTINUE
C          X( 1, I) = X1
C          X( 2, I) = X2
C          X( 3, I) = X3
C          GO TO 250
C
C          CYLINDRICAL COORD.
C
C      150 CONTINUE
C          X( 1, I) = R * COS( THETA * DR )
C          X( 2, I) = R * SIN( THETA * DR )
C          X( 3, I) = X3
C          GO TO 250
C
C          SPHERICAL COORD.
C
C      200 CONTINUE
C          X( 1, I) = R * SIN( THETA*DR ) * COS( PHI * DR )
C          X( 2, I) = R * SIN( THETA*DR ) * SIN( PHI * DR )
C          X( 3, I) = R * COS( THETA*DR )
C
C      250 CONTINUE
C
C 901 FORMAT ( A5, A3, I8, 3F8.2, I8 )
C
RETURN
END
CDECK COORD
SUBROUTINE COORD( X, NG)
C
C
C      TRANSFORM COORDINATES OF THE GRID POINT OF FINITE ELEMENT
C      TO THE AERO CODE SYSTEM USING THE TRANSFORM MATRIX TFM
C
C      COMMON/CORTN/ NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
C      DIMENSION X(3,NG), TX(3)
C
C      NT = NTRANS(NSYM)

```

```

C DO 300 I=1, NG
C DO 210 ITRAN = 1, NT
C DO 200 J=1,3
  SUM = 0.0
  DO 150 K=1, 3
    JK = K + (J-1) * 3
    SUM = SUM + X( K,I) * BTFM( JK, ITRAN, NSYM)
  150 CONTINUE
  TX(J) = SUM + VA( J, ITRAN, NSYM)
  200 CONTINUE
  DO 205 M=1,3
    X( M, I) = TX( M )
  205 CONTINUE
C 210 CONTINUE
C 300 CONTINUE
C RETURN
C END
CDECK, SURFIT
  SURROUTINE SURFIT( X, Y, N3, B )
C
C COMPUTES COEFFICIENTS FOR SURFACE SPLINE.
C N TOTAL NUMBER OF INPUT POINTS, CAN BE RANDOMLY LOCATED.
C JEQ FOR EQUATION NUMBERING
C MUK FOR COEFFICIENT NUMBERING
C
C CF ARE THE COEFFICIENT MATRIX OF EQUATION
  W(X,Y) = B(1) + B(2)*X + B(3)*Y + SUM OF B(I) * R(I)**2 *
  LN( R(I)**2)
C
C COMMON/REPEAT/ IREPT
C DIMENSION IPIV(115), INXR(115), INXC(115), CF(115,115), TM(115)
C DIMENSION X(N3), Y(N3), B(N3)
C
C N4 = 115
C N2 = N3 - 1
C N1 = N3 - 2
C N = N3 - 3
C
C BYPASS MATRIX INVERSION FOR THE CASE WHERE THE DATA POINTS (X,
C Y ) ARE IDENTICAL FOR INTERPOLATION
C
  101 CONTINUE
  DO 100 JEQ = 1, N
    CF( JEQ, 1) = 1.0
    CF( JEQ, 2) = X( JEQ )
    CF( JEQ, 3) = Y( JEQ )
    DO 90 MUK = 1, N
      MUK1 = MUK + 3
      IF ( MUK.EQ. JEQ ) GO TO 90
      RJM = ( X( MUK ) - X( JEQ ) )**2 + ( Y( MUK ) - Y( JEQ ) )**2
      CF( JEQ, MUK1 ) = RJM * ALOG( RJM )
    90 CONTINUE
  100 CONTINUE
C
  DO 150 K=1,3
    CF( N1, K) = 0.0
    CF( N2, K) = 0.0
    CF( N3, K) = 0.0

```

```

150 CONTINUE
DO 200 MUK = 1, N
  MUK1 = MUK + 3
  CF( N1, MUK1 ) = 1.0
  CF( N2, MUK1 ) = X( MUK )
  CF( N3, MUK1 ) = Y( MUK )
200 CONTINUE
C
C
C
IA = N3
CALL INVERT( GOT, CF, IA, IPIV, INXR, INXC, N4 )
C
250 CONTINUE
B(N1) = B(N2) = B(N3) = 0.0
C
DO 300 I=1, N3
  SUM = 0.0
DO 290 J=1, N3
  SUM = SUM + CF(I, J) * B(J)
290 CONTINUE
TM(I) = SUM
300 CONTINUE
C
DO 400 I=1, N3
  B(I) = TM(I)
400 CONTINUE
C
RETURN
END
CDECK INVERT
SUBROUTINE INVERT (GOTON, A, IA, IPIVOT, INDXR, INXC, NROWS)
C .....
C .....
C .....
REAL A(NROWS, NROWS), PIVOT, T
INTEGER IPIVOT(IA), INDXR(IA), INXC(IA)
C
C
GOTON = 1
N = IA
DO 1000 J=1, N
  IPIVOT(J) = 0
DO 1090 I=1, N
  T = 0.0
DO 1020 J=1, N
    IF (IPIVOT(J).EQ.1) GO TO 1020
  DO 1010 K=1, N
    IF (IPIVOT(K).EQ.1) GO TO 1010
    IF ( .NOT. (ABS(A(J,K)) -ABS(T) .GT. 0.0) ) GO TO 1010
    IROW = J
    ICOL = K
    T = A(J,K)
1010 CONTINUE
1020 CONTINUE
IPIVOT(ICOL) = IPIVOT(ICOL)*1
IF (IROW.EQ.ICOL) GO TO 1040
DO 1030 L=1, N
  T = A(IROW,L)
  A(IROW,L) = A(ICOL,L)
  A(ICOL,L) = T
1030 A(ICOL,L) = T
1040 INDXR(I) = IROW
  INXC(I) = ICOL

```

```

INVE1010
INVE1020
INVE1030
INVE1040
INVE1050
INVE1060
INVE1070
INVE1080
INVE1090
INVE1100
INVE1110
INVE1120
INVE1130
INVE1140
INVE1150
INVE1160
INVE1170
INVE1180
INVE1190
INVE1200
INVE1210
INVE1220
INVE1230
INVE1240
INVE1250
INVE1260
INVE1270
INVE1280
INVE1290
INVE1300
INVE1310
INVE1320
INVE1330

```


163

INVB1110
INVB1120
INVB1130
INVB1140
INVB1150
INVB1160
INVB1170
INVB1180
INVB1190
INVB1200

```

C DIMENSION ABB(115,115),AMB(110)
C
C MDMEN=115
C
C READ AERODYNAMIC INFLUENCE MATRIX (INFLUENCE ON BODY DUE TO BODY
C AND INFLUENCE ON WING DUE TO BODY) INTO CORE
C
C CALL FSF(1,NTAPEA,IRR)
C DO 1000 J=1,NBODY
C READ (NTAPEA) (ABB(I,J),I=1,NBODY), (AMB(I),I=1,NWING)
C IF (EOF(NTAPEA)) 1040, 990
C 990 CONTINUE

```

INVB1220
INVB1230
INVB1240
INVB1250
INVB1260
INVB1270
INVB1280
INVB1290
INVB1300
INVB1310
INVB1320
INVB1330
INVB1340
INVB1350
INVB1360
INVB1370
INVB1380
INVB1390
INVB1400
INVB1410
INVB1420
INVB1430
INVB1440
INVB1450

```

C WRITE (NTAPEA) (AMB(I),I=1,NWING)
C 1000 CONTINUE
C CALL FOR EOF (NTAPEA)
C
C INVERT AERODYNAMIC INFLUENCE MATRIX (INFLUENCE ON BODY DUE TO BODY
C CALL SINVRT(ABB,MDMEN,NBODY,IRR1,IRR2,SCALE,DET,NDETXP)
C IF (IRR1)1010,1020,1010
C 1010 CONTINUE
C WRITE (NTAPEA,1050) IRR1,IRR2,SCALE
C REWIND NTAPEA
C *****
C STOP
C *****
C 1020 CONTINUE
C DO 1030 J=1,NBODY
C WRITE (NTAPEA) (ABB(I,J),I=1,NBODY)
C 1030 CONTINUE
C CALL FOR EOF (NTAPEA)
C REWIND NTAPEA

```

INVB1470
INVB1480
INVB1490
INVB1500
INVB1510
INVB1520
INVB1530

```

C -----
C PROGRAM EXITS
C GO TO 1200
C -----
C END OF FILE ON NTAPEA
C 1040 WRITE (NTAPEA,1060) NTAPEA,J,NBODY,NWING
C *****
C STOP
C *****
C 1200 CONTINUE

```

INVB1540
INVB1550
INVB1560
INVB1570

```

C 1050 FORMAT(1H1,33HERROR IN INVERSION OF BODY MATRIX,5X,
C 16HIRR1 =,13,5X,6HIRR2 =,13,5X,7HSCALE =,E12.6)
C 1060 FORMAT(1H0,33H***END OF FILE DETECTED ON UNIT ,12,3H J= ,15,
C 1 8H NBODY= ,13,8H NWING= ,13)

```

INVR1010
INVR1020
INVR1030
INVR1040
INVR1050
INVR1060

```

C CHECK INVRW
C OVERLAY(WANG, 7, 3)
C PROGRAM INVRW
C
C .....
C INVERT REDUCED MATRIX
C MAXIMUM SIZE MATRIX INVERSION =110
C .....
C COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEA,NTAPEE,NTAPEF,NTAPEI,

```

```

1 NTAPEO, NSODY, NWING, XMACH, SYM, KACE, NPOLAR, IRW
C DIMENSION ARWW(115,115)
C MDENEN=115
DO 1000 J=1, NWING
READ (NTAPEE) (ARWW(I,J), I=1, NWING)
1000 CONTINUE
CALL FOR EOF (NTAPEE)
C
C MATRIX INVERSION
CALL SINVRT(ARWW, MDENEN, NWING, IRR1, IRR2, SCALE, DET, NDETYP)
IF (IRR1) 1010, 1020, 1010
1010 CONTINUE
WRITE (NTAPEO, 1040) IRR1, IRR2, SCALE
REWIND NTAPEE
C *****
C STOP
C *****
C
1020 CONTINUE
DO 1030 J=1, NWING
WRITE (NTAPEE) (ARWW(I,J), I=1, NWING)
1030 CONTINUE
CALL FOR EOF (NTAPEE)
REWIND NTAPEE
C
C -----
C -----
1040 FORMAT(1H1, 3HERROR IN INVERSION OF REDUCED MATRIX, 5X,
10HIRR1 =, I3, 5X, 6HIRR2 =, I3, 5X, 7HSCALE =, E12.6)
END
CDECK MDXATE
OVERLAY(WANG, 7, 4)
PROGRAM MDXATE
C
C .....
C MAXIMUM SIZE MATRIX INVERSION =112
C MUST BE 2 PLUS MAXIMUM NUMBER OF WING PANELS(110)
C .....
C
COMMON / MAIN / NTAPEO, NTAPEE, NTAPEC, NTAPEF, NTAPEI,
1 NTAPEO, NSODY, NWING, XMACH, SYM, KACE, NPOLAR, IRW
C DIMENSION MW(115,115), XBAR(210), AREA(210)
NN=NWING+1
NNN=NWING+2
C
C COMMON/ MAIN / NTAPEO, NTAPEE, NTAPEC, NTAPEF, NTAPEI,
1 NTAPEO, NSODY, NWING, XMACH, SYM, KACE, NPOLAR, IRW
C DIMENSION MW(115,115), XBAR(210), AREA(210)
NN=NWING+1
NNN=NWING+2
C
C DRAG MINIMIZATION OPTION ELIMINATED BY SETTING DMIN = 0.0 HERE
CAN BE RESTORED BY PLACE THE STATEMENT " READ (LI,1020) DMIN
HERE AND REMOVE DMIN = 0.0.
C DMIN = 0.0
C
IF (DMIN) 1000, 1000, 1020
1000 CALL FSF(1, NTAPEO, IRR)
DO 1010 I=1, NNN
DO 1010 J=1, NNN
1010 MW(I,J)=0
GO TO 1130
1020 MDENEN=115

```

INVR1090
INVR1100
INVR1110
INVR1120
INVR1130
INVR1140
INVR1150
INVR1160
INVR1170
INVR1180
INVR1190
INVR1200
INVR1210
INVR1220
INVR1230
INVR1240
INVR1250
INVR1260
INVR1270
INVR1280
INVR1290
INVR1300
INVR1310
INVR1320
INVR1330
INVR1340
INVR1350
INVR1360
INVR1370
INVR1390
INVR1400
INVR1410

MDMA1010
MDMA1020
MDMA1030
MDMA1040
MDMA1050
MDMA1060
MDMA1070

MDMA1100
MDMA1110
MDMA1120
MDMA1130
MDMA1140

MDMA1160
MDMA1170
MDMA1180
MDMA1190
MDMA1200
MDMA1210
MDMA1220

```

1030 CONTINUE
      REWIND NTAPEE
      DO 1040 I=1,NWING
        K=I
        I1=I+NBODY
        DO 1040 J=1,K
          JJ=J+NBODY
          WW(I,J)=WW(I,J)+AREA(I1)-WW(J,I)+AREA(JJ)
          WW(J,I)=WW(I,J)
1040 CONTINUE
      DO 1050 J=1,NWING
        JJ=J+NBODY
        WW(J,NN)=--AREA(JJ)
        WW(NN,J)=--AREA(JJ)
        XA=XEAR(JJ)+AREA(JJ)
        WW(J,NNN)=XA
        WW(NN,J)=XA
1050 CONTINUE
      WW(NN,NN)=0.0
      WW(NN,NNN)=0.0
      WW(NNN,NN)=0.0
      WW(NNN,NNN)=0.0
      CALL FSF(1,NTAPEA,IRR)
      DO 1060 J=1,NNN
        WRITE (NTAPEA)(WW(I,J),I=1,NNN)
        CALL FOR EOF (NTAPEA)
1060 CONTINUE
      INVERT DRAG MINIMIZATION MATRIX CONSTRAINED FOR CL
      CALL SINVRT (WW,MOEMEN,NN,IRR1,IRR2,SCALE,DET,NDETXP)
      IF (IRR1)1070,1080,1070
1070 CONTINUE
      WRITE (NTAPE0,1170) IRR1,IRR2,SCALE
      REWIND NTAPEA
C *****
C *****
C *****
C *****
1080 CONTINUE
      DO 1090 J=1,NN
        WRITE (NTAPEA)(WW(I,J),I=1,NN)
        CALL FOR EOF (NTAPEA)
        REWIND NTAPEA
        CALL FSF(1,NTAPEA,IRR)
        DO 1100 J=1,NNN
          READ (NTAPEA)(WW(I,J),I=1,NNN)
          CALL FSF(2,NTAPEA,IRR)
1100 CONTINUE
      INVERT DRAG MINIMIZATION MATRIX CONSTRAINED FOR CL AND CM
      CALL SINVRT (WW,MOEMEN,NNN,IRR1,IRR2,SCALE,DET,NDETXP)
      IF (IRR1)1070,1110,1070
1110 CONTINUE
      DO 1120 J=1,NNN
        WRITE (NTAPEA)(WW(I,J),I=1,NNN)
        CALL FOR EOF (NTAPEA)
        REWIND NTAPEA
C -----
C -----

```

```

MDMA1230
MDMA1240
MDMA1260
MDMA1270
MDMA1280
MDMA1290
MDMA1300
MDMA1310
MDMA1320
MDMA1330
MDMA1340
MDMA1350
MDMA1360
MDMA1370
MDMA1380
MDMA1390
MDMA1400
MDMA1410
MDMA1420
MDMA1430
MDMA1440
MDMA1450
MDMA1460
MDMA1470
MDMA1480
MDMA1490
MDMA1500
MDMA1510
MDMA1520
MDMA1530
MDMA1540
MDMA1550
MDMA1560
MDMA1570
MDMA1580
MDMA1590
MDMA1600
MDMA1610
MDMA1620
MDMA1630
MDMA1650
MDMA1660
MDMA1670
MDMA1680
MDMA1690
MDMA1700
MDMA1710
MDMA1720
MDMA1730
MDMA1740
MDMA1750
MDMA1760
MDMA1770
MDMA1780
MDMA1790
MDMA1800
MDMA1810
MDMA1820
MDMA1830
MDMA1840
MDMA1850
MDMA1860
MDMA1870

```



```

C      PROGRAM EXITS
C      GO TO 1200
C      -----
1130 DO 1140 J=1,NNN
1140 WRITE (NTAPEA) (WM(I,J),I=1,NNN)
CALL FOR EOF (NTAPEA)
DO 1150 J=1,NN
1150 WRITE (NTAPEA) (WM(I,J),I=1,NN)
CALL FOR EOF (NTAPEA)
GO TO 1110
C 1200 CONTINUE
C
C      FORMATION OF DRAG MINIMIZATION MATRIX
1160 FORMAT(7F10.0)
1170 FORMAT(1H1,40HERROR IN INVERSION OF DRAG MINIMIZATION MATRIX
1,6HIRR1 =,13,5X,6HIRR2 =,13,5X,7HSCALE =,E12.6)
END
CDECK WANG75
OVERLAY (WANG, 7, 5)
PROGRAM WANG75
C
C      COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1 NTAPEO,NEODY,NWING,XMACH,SYM,KACE,NPOLAR,IRM
C      COMMON / BODYSP/ DRDX(51), DZDX(51)
C      COMMON / AVAR/ A(210),ACB(21),ABX(100),AUX(110),AREA(210),ARN(2),A000000090
2 RAT(20),ALPHA(210),ALPHAB(210),ALPHAS(210),ALPHAT(100000100
3 10),ALPHAX(110),ALPHAX(110),AWS(110),ABT(100),ANTN(00000110
210,2),ALPHAA,ALPHAD,ARA,ARADeg,ARB,ARW,ARAS,AT,AAA00000120
C      COMMON / BODS/ NURBOD,XNOS(3),YNOS(3),ZNOS(3),NBSTAT(3)
C      COMMON / BVAR/ B(210)
1 BECL,BBCD,BBCM
C      COMMON/CVAR/C(210),CHORD(210),CL(210),CPNN(51,11,2)
2 CLS(210)
C      COMMON / KVAR/ KASE,CPCALC,CBAR,CONSNT,CLBAR,CLX,CLM,CDM
C      COMMON / NVAR/ KASE,KONFIG,KPOLAR
1 NS,NPANEL,NACEL,NROBE,NRONW,NCOLW,NTHETA,NTHETS,
2 NXLE,NRG,NPOLR,NCLX
C      COMMON/RVAR/ R(51),RN(51,2),RATIOX,RAREA
C      COMMON/TVAR/ TITLE(20),THETA(210),THETAB(11),THETAS(11),THETAN
1 (11,2),TCL(11),TCD(11),TCM(11),THICK,TWIST
C      COMMON /UVAR/ UWBT(100),UWBT(110),UWWT(110),UNCL(210,2)
C      COMMON /VVAR/ VBWT(100),VBWT(110),VWWT(110),VNCL(210,2)
1 VOUT
C      COMMON /WVAR/ WBT(100),WBT(110),WWT(110),WNCL(210,2)
C      COMMON/XVAR/ XBAR(210),XC(210),XNI(2),XNXN(2),XNTN(2),XB(51),
1 XN(51,2),XNCD(2),XNCL(2),XNCM(2),XYZ(3),ZCL(11),
2 XCD(11),XNACEL,XPCPBAR
C      COMMON /YVAR/ YBAR(210),YC(210),YNI(2)
C      COMMON/ZVAR/ ZBAR(210),ZC(210),ZNI(2),ZDELTA(51),ZDN(51,2)
1 ZP,ZA
C      COMMON/PEDATA/ NEODYS,XNIDB(51),NTHETB,THETB(11),CPBB(51,11)
1 XCB(3,700),NG(350),NELM(700),NE,NGRIDP,PINF,IPUNCH
C      COMMON/EXTRA/ ARAN,DSB1,DSB2,DS1,DS2,NB1,NB2,NS1,NS2,
1 NTN,NXN,XNOSE
C      COMMON/NSLOPE/ DRNDX(51,2),DZNDX(51,2)
C      DIMENSION NST(2),NS2(2),DS1(2),DS2(2)

```

MDMA1890
MDMA1900
MDMA1910
MDMA1920
MDMA1930
MDMA1940
MDMA1950
MDMA1960
MDMA1970
MDMA1980

MDMA1990
MDMA2000
MDMA2010
MDMA2020
MDMA2030

000000090
1000000100
0000000110
0000000120
00000130
00000140
00000150

00000170
00000180
00000220
00000230

00000330
00000340
00000350
00000360

00000410
00000430

```

IF ( KONFIG -EQ. 1 ) GO TO 50
CALL SUBR00(NEODYS, NTHETB, O, XNOSE, 0.0, 0.0, CPCALC, VOUT,ARA,

```

```

1  XP, ZP, RFAREA, XB, R, THETA, ZDELTA, XC, YC, ZC, THETA,
2  UHET, VUHET, WUHET, ALPHA, CPBB, BBCL, BBCL, BBCL, BBCL, BBCL, BBCL,
3  NBZ, DSB1, DSE2)

```

```

C 50 CONTINUE
IF ( XNACEL ) 100, 500, 100
100 CONTINUE

```

```

C DO 200 N=1, NACEL

```

```

C DO 150 J=1, NXN
DRDX(J) = DRDX(J,N)
DZDX(J) = DZDX(J,N)
150 CONTINUE

```

```

C ARAN = AKA + ARN(N) / CDR
CALL SUBR0D( NXN, NTN, NACEL, XNI(N), YNI(N), ZNI(N), CPCALC, VOUT
1  ARAN, XP, ZP, RFAREA, XN(1,N), RN(1,N), THETA(1,N),
2  ZDN(1,N), XC, YC, ZC, THETA, UNCL(1,N), VNCL(1,N),
3  UNCL(1,N), ANIN(1,N), CPNN(1,N), XNCL(N), XNCL(N),
4  XNCL(N), NS1(N), NS2(N), DS1(N), DS2(N) )
200 CONTINUE

```

```

C 500 CONTINUE

```

```

C

```

```

CDECK TRAP
SUBROUTINE TRAP(XT,YT,ZT,NT)
DIMENSION XT(1),YT(1)
SUM=0.
DO 1000 I=2,NT
1000 SUM=SUM+.5*(XT(I)-XT(I-1))*(YT(I)+YT(I-1))
ZT=SUM
RETURN
END

```

```

TRAP1000
TRAP1010
TRAP1020
TRAP1030
TRAP1040
TRAP1050
TRAP1060

```

```

CDECK SUBR0D
SUBROUTINE SUBR0D(NBS,NT,NSTOR,XN,YN,ZN,CPC,VEL,ARA,XP,ZP,RFAREA,
1  XB,R,THETA,ZCAM,XC,YC,ZC,TA,U,V,W,EN,CPB,BCL,BCD,BCM,
2  NS1,NS2,DS1,DS2)
COMPUTES SINGULARITY STRENGTHS, VELOCITY COMPONENTS AND PRESSURES
.....
.....
.....

```

```

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080

```

```

COMMON / MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1  NTAPEO,NEOD, NW, XHACH,SYM,KACE,NPOLAR,IRW
COMMON / BODYSP / DRDX(51), DZDX(51)

```

```

00000110
00000120

```

```

C DIMENSION XB(1),R(1),THETA(1),ZCAM(1),XC(1),YC(1),
1  ZC(1),TA(1),U(1),V(1),W(1),EN(1),CPB(51,1),QC(51),
2  THETA(11),RR(210),SY(2),RB(51),UB(51,11),VB(51,11),
3  WB(51,11),VB(51,51),UC(51),VC(51),RB2(51)
4  X(51),ARC(51),Q(51),ZB(51)
5  DIMENSION A(52),B(52),C(52),XX(52),YA(11),YX(11)
6  DIMENSION CP(11),G(52)

```

```

00000160
00000180
00000190

```

```

C EQUIVALENCE ( UC(1), RR(1)), ( VC(1), RR(52))

```

```

00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280

```

```

C CALCULATION OF SINGULARITY STRENGTHS

```

```

NP=NX+NEOD
NB=NBS-1
KA=0
PI=3.1415926
B2=1.-E**EH

```



```

1180 EL=XB(NBS)-XB(M)
    XL=EX-EL
    D1=SQR(XL**2+RB2*RB2(N))
    D2=SQR(EX**2+RB2*RB2(N))
    D3=D1**3
    D4=D2**3
    US=1./D1-1./D2
    VS=B2*RB(N)*(1./D1*(XL+D1))-1./D2*(EX+D2))
    U(N)=U(N)+US*Q(M)
    V(N)=V(N)+VS*Q(M)
    IF(KA)1180,1190,1180
1180 UR=B2*RB(N)*(1./D4-1./D3)
    VR=(XL*(XL**2+2.*B2*RB2(N))/D3-EX*(EX**2+2.*B2*RB2(N))/D4)/RB2(N)
    WR=(XL/D1-EX/D2)/RB2(N)
    UC(N)=UC(N)+UR*QC(M)
    VC(N)=VC(N)+VR*QC(M)
    W(N)=W(N)+WR*QC(M)
1190 CONTINUE
    DO 1200 L=1,NT
    UB(N,L)=U(N)+UC(N)*COS(THETB(L))
    VB(N,L)=V(N)+VC(N)*COS(THETB(L))
    WB(N,L)=W(N)*SIN(THETB(L))
1200 CONTINUE
1210 CONTINUE
    C
    C
    C
    VELOCITY COMPONENTS ON THE WING
    IF(NW)1300,1300,1320
1220 IF(NSTOR)1230,1240,1230
1230 NS=1
    JM=2
    SY(1)=1
    SY(2)=-1
    GO TO 1250
1240 NS=NB00+1
    JM=1
    SY(1)=0
    SY(2)=1
1250 CONTINUE
    L=0
    C
    DO 1290 N=NS,NP
    L=L+1
    U(L)=0
    V(L)=0
    W(L)=0
    EN(L)=0
    DO 1290 J=1,JM
    DYC=YC(N)-SY(J)*YN
    DZC=ZC(N)-ZN
    IF(DYC.EQ.0..AND.DZC.EQ.0.) GO TO 1260
    THETN=ATAN2(DYC,DZC)
    GO TO 1270
1260 THETN=0
1270 COSTN=COS(THETN)
    SINTN=SIN(THETN)
    R2=(YC(N)-SY(J)*YN)**2+(ZC(N)-ZN)**2
    RR(L)=SQR(R2)
    BR2=B2*RB
    VR=0
    VT=0
    DO 1280 M=1,NB
    EX=XC(N)-XN-XB(M)
    EL=XB(NBS)-XB(M)
    XL=EX-EL
    D1=SQR(XL**2+BR2)

```

```

D2=SQRT(EX**2+BR2)
D3=D1**3
D4=D2**3
U(L)=U(L)+(1./D1-1./D2)*Q(M)+B2*RR(L)*(1./D4-1./D3)*COSTN*QC(M)
VR=VR+B2*RR(L)*(1./D1*(XL*D1)-1./D2*(EX+D2))*Q(M)+(XL*(XL**2-2*
1.*BR2)/D3-EX*(EX**2+2.*BR2)/D4)/R2*QC(M)*COSTN
1280 VT=VT+(XL/D1-EX/D2)/R2*QC(M)*SINTN
THETS = THETS + TA(N)
V(L)=VR*SINTN+VT*COSTN+V(L)
W(L)=VR*COSTN-VT*SINTN+W(L)
EN(L)=EN(L)+VR*COS(THETS)-VT*SIN(THETS)
C 1290 CONTINUE
C
C CALCULATE PRESSURES, FORCES, AND MOMENTS
C
1300 ARM = ARA
SINARM = SIN(ARM)
COSARM = COS(ARM)
IF (CEM.EQ.0.) GO TO 1310
Q000 = 1.42857/EM**2
Q001 = .2*EM**2
1310 DO 1360 N = 1, NT
COST = COS(THETB(N))
SINT = SIN(THETB(N))
DO 1360 M = 1, NB
VPM = VB(M,N) * COST + VB(M,N) * SINT
WPM = VB(M,N) * COST - VB(M,N) * SINT
UWPM = UB(M,N) * COSARM + WPM * SINARM
UWIND = 1. + UWPM
VWIND = VPM
WVIND = WPM * COSARM - UB(M,N) * SINARM
IF (CPC - 1.) 1320,1330,1340
1320 CPB(M,N) = -2. * UWPM
1330 CPB(M,N) = -2.*UWPM -B2*UWPM**2 - VWIND**2 - WVIND**2
GO TO 1360
1340 Q2 = UWIND**2+VWIND**2+WVIND**2
IF (CEM.EQ.0.) GO TO 1350
CPB(M,N) = Q000*((1. + Q001*(1.-Q2)) **3.5 - 1.)
GO TO 1360
1350 CPB(M,N) = 1. - Q2
1360 CONTINUE
C
IF (EM)1390,1380,1370
1370 CPSTAG = Q000*((1.*Q001)**3.5-1.)
GO TO 1390
1380 CPSTAG=1.
1390 CONTINUE
BCL=0.
ECM=0.
IF(NS1)1410,1410,1400
1400 IF(NS2)1410,1410,1420
1410 NS1=1
NS2=NB
1420 NBL=NS2+1-NS1
NET=NEL+1
M1=NS2-1
M1 = 1
DO 1440 M = NS1,M1
MM = MM + 1
RM = RB(M)
DO 1430 N = 1,NT
COST = COS(THETB(N))

```

```

CPBB = CPB(M,N)
CP(N) = CPBB
YA(N) = YA(N) * COST
YX(N) = YX(N) * COST
1430 CALL SIMP (GM,THETB,CP,NT,IRR)
CALL TRAP (THETB,YA,AM,NT)
CALL TRAP (THETB,YX,AM,NT)
IF (IRR .NE. 1) GO TO 1580
A(NM) = AM * RM
B(NM) = BM * RM
G(NM) = GM * RM
1440 CONTINUE
NN = NS1 - 1
DO 1450 N = 2,NEL
NN = NN + 1
C(N) = DZDX(NN) * A(N) + DRDX(NN) * G(N)
1450 XX(N) = X(NN)
XX(1) = XB(NS1)
XX(NS1) = XB(NS2)
IF (VEL-GT.O.) WRITE (6,1710)
IF (VEL-GT.O.) WRITE (6,1720)
IF (VEL-GT.O.) WRITE (6,1740)
C(1) = 5 * CPSTAG * DS1
C(NET) = 5 * CPSTAG * DS2
IF (R(NBS) .NE. 0.) C(NET) = 0.
A(1) = ZCAM(1)*C(1)
A(NET) = ZCAM(NBS)*C(NET)
IF (VEL-GT.O.) WRITE (6,1730)
IF (VEL-GT.O.) WRITE (6,1700)
IF (VEL-GT.O.) WRITE (6,1740)
IF (VEL-GT.O.) WRITE (6,1700)
CALL SIMP (CN,XX,A,NBT,IRR)
CN=-CN
IF (IRR .NE. 1) GO TO 1580
CALL SIMP (CX,XX,C,NBT,IRR)
IF (IRR .NE. 1) GO TO 1580
NN = NS1 - 1
DO 1460 N = 2,NEL
NN = NN + 1
1460 A(N) = A(N)*(X(NN)*XN-XP+RB(NN)*DRDX(NN))+ZB(NN)*C(N)*RB(NN)
* DRDX(NN)*B(N)
IF (VEL-GT.O.) WRITE (6,1750)
IF (VEL-GT.O.) WRITE (6,1700)
CALL SIMP (CM,XX,A,NBT,IRR)
IF (IRR .NE. 1) GO TO 1580
BCL=CN*cos(ARA)-CX*SIN(ARA)
BCD=CM*cos(ARA)+CN*SIN(ARA)
BCM = CM + CX*(ZN-ZP)
DO 1480 N=1,NBS
1480 XB(N)=XB(N)*X1
DO 1490 N=1,NT
1490 THETB(N)=THETB(N)*57.2957795
C
C
PRINT OUT VELOCITY COMPONENTS
IF (VEL)1500,1570,1500
1500 IF (NSTOR)1510,1520,1510
1510 WRITE (NTAPE0,1620) NSTOR,NSTOR
GO TO 1330
1520 WRITE (NTAPE0,1630)
1530 CONTINUE
WRITE (NTAPE0,1640)
WRITE (NTAPE0,1640) (THETB(M),M=1,NT)
WRITE (NTAPE0,1650)
DO 1540 N=1,NB
1540 WRITE (NTAPE0,1610) X(N),(UB(N,M),M=1,NT)

```



```

2 COMMON /KVAR/ CDR,CASE,CPCALC,CBAR,CONSNT,CLBAR,CLX,CLW,CDM 00000180
COMMON /NVAR/ KASE,KONFIG,KPOLAR 00000220
COMMON /NS/ NPANEL,NACEL,NROBE,NROW,NCOLW,NTHETA,NTHETS, 00000230
COMMON /NLE/ NRG,NPOLR,NCLX
COMMON /RVAR/ R(51),RN(51,2),RATIOX,RFAREA
COMMON /TVAR/ TITLE(20),THETA(210),THETAB(11),THETAN 00000330
COMMON /UVAR/ U(11),TCL(11),TCD(11),TCM(11),THICK,TWIST 00000340
COMMON /VVAR/ VBT(100),VWBT(110),VWMT(110),VNCL(210,2) 00000350
COMMON /WVAR/ WBT(100),WMT(110),WMT(110),WNCL(210,2) 00000360
COMMON /XVAR/ XBAR(210),XC(210),XNI(2),XNXN(2),XNTN(2),XB(51), 00000410
COMMON /YVAR/ YBAR(210),YC(210),YNI(2),YXNCM(2),XYZ(3),ZCL(11), 00000430
COMMON /ZVAR/ ZBAR(210),ZC(210),ZNI(2),ZDELTA(51),ZDN(51,2)
COMMON /PEDATA/ NEODYS,XMIDB(51),NTHETB,THETB(11),CPBB(51,11)
COMMON /CPB/ XCB(3,700),NG(350),NELM(700),NE,NGRIDP,PINF,IPUNCH
COMMON /EXTRA/ ARAN,DSB1,DSB2,DS1,DS2,NB1,NB2,NS1,NS2,
COMMON /NSLOPE/ DRDX(51,2),DZDX(51,2)
COMMON /NS1(2)/ NS2(2),DS1(2),DS2(2)
COMMON /CPB(110)/
IF ( KONFIG.EQ.1 ) GO TO 50
CALL KARMOR(NBODYS,NTHETB,0,XNOSE,0.0,0.0,CPCALC,VOUT,ARA,
1 XP,ZP,REAREA,XB,R,THETB,ZDELTA,XC,YC,ZC,THETA,
2 UNST,VWBT,WNST,ALPHAX,CPBB,BBCL,BBCL,BBCL,NB1,
3 NB2,DSB1,DSB2)
50 CONTINUE
IF ( XNACEL ) 100, 500, 100
100 CONTINUE
C DO 200 N=1, NACEL
C DO 150 J=1, NXN
DRDX(J) = DRDX(J,N)
DZDX(J) = DZDX(J,N)
150 CONTINUE
C ARAN = ARA + ARN(N) / CDR
CALL KARMOR( NXN,NTN,NACEL,XNI(N),YNI(N),ZNI(N),CPCALC,VOUT
1 ARAN,XP,ZP,REAREA,XN(1,N),RN(1,N),THETAN(1,N),
2 ZDN(1,N),XC,YC,ZC,THETA,UNCL(1,N),VNCL(1,N),
3 WNCL(1,N),ANIN(1,N),CPNN(1,N),XNCL(N),XNCL(N),
4 XNCL(N),NS1(N),NS2(N),DS1(N),DS2(N) )
200 CONTINUE
C 500 CONTINUE
C
CDECK KARMOR
END
SUBROUTINE KARMOR(NBODYS,NTHETA,NACEL,XN,YN,ZN,CPCALC,VOUT,ARA
1,XP,ZP,REAREA,XB,R,THETAB,ZDELTA,XC,YC,ZC,THETA,U,VV,WW,ANI,CPBB
2,BBCL,BBCL,BBCL,NS1,NS2,DS1,DS2)
C .....
C ..... CALCULATION OF VELOCITY COMPONENTS DUE TO BODY THICKNESS .....
C .....
C .....

```

```

C      COMMON/ MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1      NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRM
C      COMMON / BODYSP/ DRDX(51), DZDX(51)
C
C      DIMENSION XB(1),R(1),THETAB(1),ZDELTA(1),XC(1),YC(1),ZC(1)
1      U(1),VV(1),WW(1),AN(1),CPBB(51),THETA(1)
C      DIMENSION ALPHAC(51),T(51),TC(51),TX(51),UB(51),VB(51),
1      VTB(51),SY(2),FD(51),SD(51),NBS(11),COSTB(11),
2      SINTB(11),CP(11),YA(11),YB(11),A(51),D(51),G(51),
3      C(51),XBB(51)
C
C      EPS = 1.0E-6
C      PI=3.1415926
C      XMACH2=XMACH*XMACH
C      BT2=XMACH2-1
C      BETA=SQRT(BT2)
C      N1=NEODYS-1
C      X1 = XB(1)
C      DO 1000 N = 1, NEODYS
1000 XB(N) = XB(N) - X1
C      DO 1010 J=1,NTHETA
C      THETAB(J) = THETAB(J)/57.2957795
1010 COSTB(J) = COS(THETAB(J))
C      SINTB(J) = SIN(THETAB(J))
C
C      COMPUTE FIRST AND SECOND DERIVATIVES
C      DO 1015 N = 1, NEODYS
1015 ALPHAC(N) = ARA - DZDX(N)
C      DO 115 I=1,N1
C      FD(1) = DRDX(1)
115 CONTINUE
C      FD2 = FD(1) * FD(1)
C      BTAN = BETA * FD(1)
C      IF (BTAN .LT. 1.0) GO TO 1020
C      WRITE (6,1580)
C      *****
C      STOP
C      *****
C      1020 SBT2 = SQRT (1.-BT2*FD2)
C      SLOG = ALOG((1.+SBT2)/BTAN)*FD2
C      CALCULATE SOURCE STRENGTHS
C      DO 1150 I=1,N1
C      M=I+1
C      UBSUM=0.
C      VBSUM=0.
C      UEDSUM=0.
C      VEDSUM=0.
C      VTDSUM=0.
C      PHIS = 0.
C      PHID=0.
C      RDRDX = FD(M)*R(M)
C      RM=R(M)
C      RM2=RM*RM
C      RDRDM=RDRDX
C      RS=R22=ALPHAC(I)
C      TRM1 = XB(M)-XB(1)
C      BRM=BETA*RM
C      BRM2 = BRM*BRM

```



```

1000  RAB21 = SQRT((TRM1*TRM1-BRM2)
      IF (BRM2.EQ.0.) GO TO 1030
      UBS1 = -ALOG ((TRM1 + RAB21)/BRM)
      RAB21 = -S*(TRM1-RAB21-BRM2*UBS1)
      RAB21 = RAB21
      RUB21 = 5*(TRM1-RAB21 + BRM2*UBS1)
      RUB21 = RUB21
      RAB21 = RAB21-RDRDX*UBS1
      RUB21 = RUB21-RDRDX*RUB21
      IF (I.NE.1) GO TO 1050
      IF I EQUALS 1, DO TANGENT CONE SOLUTION
      T11 = FD2/(SBT2 * SLOG)
      TC11 = FD2*ALPHAC(1)/((FD2*.5)*SBT2 +.5*BT2*SLOG)
      DO 1040 K=1, NTHETA
      UB(1,K) = -SLOG*T11 /FD2
      VB(1,K) = SBT2*T11/FD(1)
      VTB(1,K) = 0.
      IF (RM.EQ.0.) GO TO 1040
      IF (RM1,K)=UB(1,K)+COS(B(K))*SBT2/FD(1)+TC11
      VB(1,K)=VB(1,K)-S*COS(B(K))* (SBT2*BT2*SLOG)/FD2*TC11
      VTB(1,K)=-.5*SINTB(K)*(SBT2-BT2*SLOG)/FD2*TC11
      1040 CONTINUE
      1050 CONTINUE
      IF (RM.EQ.0) GO TO 1060
      Q001 = RUB21*TC11/RM
      Q002 = RAB21*T11/RM
      Q003 = RAB21*TC11/RM2
      Q004 = RVTD1*TC11/RM2
      DO 1130 J=1, I
      TRMJ = XB(N)-XB(J) + BETA*R(J)
      TRMJ2 = TRMJ*TRMJ
      IF (RM.EQ.0.) GO TO 1100
      F1=SQRT((TRMJ2-BRM2)
      F2 = ALOG((TRMJ+F1)/BRM)
      RAB2 = TRMJ*F1-BRM2*F2
      UBS2 = 2.*(F1-TRMJ*F2)
      RN2=RAB2-RDRDM*UBS2
      RAB22 = -((TRMJ2-4.*BRM2)*F1/3.+BRM2*TRMJ*F2)
      RUB22 = RAB2
      RVTD2 = -((TRMJ2 + 2.*BRM2)*F1/3.-BRM2*TRMJ*F2)
      RM2=RAB22-RDRDM*RUB22
      1060 IF (J.NE.1) GO TO 1080
      T(J) = (RDRDX-RN1*T11)/RN2
      TC(J) = -(RS+RN1*TC11)/RRM2
      1080 RDRDX = RDRDX-RN2*T(J)
      RS=RS+RM2*T(J)
      IF (J.NE.1) GO TO 1090
      UBSUM = UBS1*T11
      VBSUM = Q001
      VDSUM = Q002
      VDSUM = Q003
      VDSUM = Q004
      1090 CONTINUE
      UBSUM = UBSUM+UBS2*T(J)
      VBSUM = VBSUM+RAB2*T(J)/RM
      UBSUM = UBSUM + RUB2*TC(J)/RM
      VBSUM = VBSUM+RAB22*TC(J)/RM2
      VDSUM = VDSUM+RVTD2*TC(J)/RM2
      GO TO 1130
      1100 IF (I.EQ.J) GO TO 1120
      IF (J.NE.1) GO TO 1110
      PHIS = TRM1*T11

```

```

PHID = 1.5*TRM1*TRM1*TC11
1110 PHIS = PHIS+TRMJ2*T(J)
PHID = PHID+TRMJ*TRMJ2*TC(J)
GO TO 1130
1120 T(J) = -PHIS/TRMJ2
TC(J) = -PHID/(TRMJ*TRMJ2)
C 1130 CONTINUE
C
DO 1140 K=1,NTHETA
UB(M,K) = UBSUM+UBDSUM*COSTB(K)
VB(M,K) = VBSUM+VEDSUM*COSTB(K)
1140 VTB(M,K) = VTDSUM*SINTB(K)
C 1150 CONTINUE
C *****
C
CALCULATION OF VELOCITY COMPONENTS IN THE FIELD
IF (NWIN)1160,1360,1160
1160 CONTINUE
IF (NACEL.NE.O) GO TO 1170
NS=NBODY+1
JN=1
SY(1)=0
GO TO 1180
1170 NS=1
JN=2
SY(1)=1
SY(2)=-1
CONTINUE
NPANEL=NBODY+NWIN
I1=0
DO 1350 I=NS,NPANEL
I1=I+1
U(I1)=0
VV(I1)=0
WW(I1)=0
AN(I1)=0
DO 1350 N=1,JN
XCN=XC(I1)-XN
YCN=YC(I1)-SY(N)*YN
ZCN=ZC(I1)-ZN
IF (YCN.EQ.O.) GO TO 1190
THETA = ATAN2( YCN, ZCN )
GO TO 1220
1190 IF (ZCN)1210,1200,1200
1200 THETA=0
GO TO 1220
1210 THETA=PI
1220 CONTINUE
COSTHA=COS(THETA)
SINTHA=SIN(THETA)
R2=YCN*YCN+ZCN*ZCN
IF (R2.LE.EPS) R2 = 0.
R1=SQRT(R2)
BR1=BETA/R1
BR2=BT2/R2
TR=XCN-XB(NBODY)+BETA*R(NBODY)
IF (R1.EQ.O.) GO TO 1240
IF (TRM-ER1)1240,1240,1230
G1=TRM-TRM-BR2
TRM0=TRM/BR1
G2=ALOG(TRM0/SQRT (TRM0-TRM0-1.))
G3=SQRT(G1)
1230
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001790
00001810
00001820
00001830
00001840
00001850
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00020000

```



```

VF=VF-T11*(TRM*TRM-BR2)/Q002 *Q014 *(Q003
1+TRM*G3-XI*(G3-TRM*(2.*XI*(1.-Q004 )/G3)))/Q005
VTF=VTF+Q006 *(Q007
+XI*TRM*(2.*XI/G3))/Q005
1300 CONTINUE
U(I1)=U(I1)+2.*T(J)*(TRM*G2-G3+XI*XI/Q008 )
1-T(C(J))*(TRM*XI)*G3-Q003 *XI*XI*(1.-XI*BR2/Q009 )/R1
2*COSTHA
VF=VF-T(J)*(TRM*XI)*G3-Q003 *TRM*XI*XI/G3/R1
1+T(C(J))*COSTHA*(TRM*TRM-4.*BR2)*G3/3.*TRM*Q003 *XI*(TRM-XI)
2*G3/3.*XI*XI*TRM*(1.+XI*(1.-Q004 )/Q010 )/R2
VTF=VTF+T(C(J))*SINTHA*((TRM+Q017 )*G3/3.-
1-TRM*Q003 *XI*(TRM-XI)*G3/3.*XI*XI*TRM*(1.+XI/Q010 )/R2
GO TO 1330
1310 IF (TRM.EQ.0.) GO TO 1330
G4=ALOG(TRM/TRM)
IF (J.NE.1) GO TO 1320
U(I1)=U(I1)+T11*(XI/TRM-G4)
G5=(G4+XI*XI/(2.*TRM2))/2.
VF=VF+Q011 *G5
VTF=VTF+Q012 *G5
1320 U(I1)=U(I1)+2.*T(J)*(XI-TRM*G4+XI*XI/Q013 )
G6=TRM*G4-XI*(1.-XI*XI/(6.*TRM2))
VF=VF+Q018 *T(C(J))*G6
VTF=VTF+Q019 *T(C(J))*G6
1330 CONTINUE
1340 CONTINUE
C
VV(II) = VF*SINTHA+VTF*COSTHA*VV(II)
WW(II) = VF*COSTHA-VTF*SINTHA*WW(II)
THETAS=THETAA+THETA(I)
AN(II) = VF*COS(THETAS)-VTF*SIN(THETAS)*AN(II)
1350 CONTINUE
1360 CONTINUE
C
C CALCULATION OF PRESSURES, FORCES, AND MOMENTS
BODYL=XB(NBODYS)-XB(1)
CPSTAG = 1.42857 * ((1.+2.*XMACH2)**3.5 - 1.)/XMACH2
ARJ ... ARA
SINARJ = SIN(ARJ)
COSARJ = COS(ARJ)
DO 1420 J=1,NTHETA
DO 1410 I=1,NBODYS
VPM = VTB(I,J) * COSTB(J) + VB(I,J) * SINTB(J)
WPM = VB(I,J) * COSTB(J) - VTB(I,J) * SINTB(J)
UWPM = UB(I,J)*COSARJ + WPM*SINARJ
UWIND = 1. + UWPM
VWIND = VPM
WIND = WPM * COSARJ - UB(I,J) * SINARJ
IF (CPALC - 1.) 1370,1380,1390
1370 CPB(I,J) = -2. * UWPM
GO TO 1400
1380 XM2 = XMACH2 - 1.
CPB(I,J) = -2.*UWPM + XM2*UWPM**2 - VWIND**2 - WWIND**2
GO TO 1400
1390 Q2 = UWIND ** 2 + VWIND ** 2 + WWIND ** 2
CPB(I,J) = 1.42857*((1.+2.*XMACH2*(1.-Q2))**3.5-1.)/XMACH2
1400 CONTINUE
1410 IF (R(NBODYS).EQ.0.) CPB(NBODYS,J)=CPSTAG
1420 CONTINUE
C
BECL=0.
BECD=0.
BECD=0.
BECD=0.

```

```

00003301
00003302
00003303
00003304
00003310
00003311
00003312
00003320
00003330
00003340
00003350
00003360
00003370
00003380
00003390
00003400
00003410
00003420
00003430
00003440
00003450
00003460
00003471
00003472
00003473
00003480
00003490
00003500
00003510
00003511
00003520
00003521
00003530
00003540
00003541
00003542
00003550
00003560
00003570
00003580
00003590
00003600
00003610
00003620
00003621
00003622
00003630
00003640
00003650
00003660
00003670
00003680
00003690
00003700
00003710
00003720
00003730
00003740
00003750
00003760
00003770
00003780

IF (NS1.EQ. 0) NS1 = 1
IF (NS2.EQ. 0) NS2 = NBODYS
NET = NS2 - NS1 + 1
MM = 0
DO 1440 M = NS1, NS2
  MM = MM + 1
  XEB(MM) = XB(M)
  RM = R(M)
DO 1430 N=1, NTHETA
  CPB = CPB(M, N)
  CP(N) = CPB
  YA(N) = CPB * COSTB(N)
  YB(N) = YA(N) * COSTB(N)
  CALL SIMP(GM, THETAB, CP, NTHETA, IRR)
  CALL SIMP(DM, THETAB, YB, NTHETA, IRR)
  CALL SIMP(AM, THETAB, YA, NTHETA, IRR)
  IF (IRR.NE.1) GO TO 1570
  A(MM) = AM*RM
  D(MM) = DM*RM
  G(MM) = GM*RM
1440 CONTINUE
  MM = 0
DO 1450 N = NS1, NS2
  MM = MM + 1
  C(MM) = DZDX(N)*A(MM) + FD(N)*G(MM)
  IF (N.EQ. 1) C(MM) = .5*CPSTAG*DS1
  IF (N.EQ. NBODYS .AND. R(NBODYS).EQ. 0.) C(MM) = .5*CPSTAG*DS2
1450 CONTINUE
  CALL SIMP (CX, XEB, C, NET, IRR)
  CALL SIMP (CZ, XEB, A, NET, IRR)
  CN = CZ
  IF (IRR.NE.1) GO TO 1570
  MM = 0
DO 1460 N = NS1, NS2
  MM = MM + 1
  C(MM) = ZDELTA(N)*C(MM)
  G(MM) = XE(N) + XN - XF + R(N)*FD(N)
  IF (N.EQ. 1) G(MM) = XB(N) + XN - XP + DS1/(2.*PI)
  IF (N.EQ. NBODYS .AND. R(NBODYS).EQ. 0.) G(MM) = XB(N) + XN - XP + DS2/(2.*PI)
  IF (N.EQ. 1) G(MM) = A(MM)*G(MM) + C(MM) + R(N)*DZDX(N)*D(MM)
1460 CALL SIMP (CM, XEB, A, NET, IRR)
  IF (IRR.NE.1) GO TO 1570
  BBCL = CN * COS(ARA) - CX * SIN(ARA)
  BECD = CX * COS(ARA) + CN * SIN(ARA)
  BECM = CM + CX * (ZN - ZP)
DO 1470 J=1, NTHETA
  THETAB(J) = THETAB(J) * 57.2957795
1470 DO 1475 N = 1, NBODYS
  1475 XB(N) = XE(N) + X1
C
C
C
OPTIONAL PRINT OF VELOCITY COMPONENTS
IF (VOUT) 1480, 1550, 1480
1480 CONTINUE
  WRITE (NTAPE0, 1600) T11, TC11, (XB(I), ZDELTA(I), R(I), FD(I), SD(I),
    1T(I), TC(I), I=1, N1)
  I = NBODYS
  WRITE (NTAPE0, 1680)
    XB(I), ZDELTA(I), R(I), FD(I), SD(I)
  IF (NACEL) 1490, 1500, 1490
1490 WRITE (NTAPE0, 1670) NACEL, NACEL
  GO TO 1510
1500 WRITE (NTAPE0, 1610)
1510 WRITE (NTAPE0, 1640)
  WRITE (NTAPE0, 1620) (THETAB(J), J=1, NTHETA)
  WRITE (NTAPE0, 1630)

```

```

DO 1520 I=1,NBODYS
1520 WRITE (NTAPE0,1590) XB(I),(UB(I,J),J=1,NTHETA)
      WRITE (NTAPE0,1650) (THETAB(J),J=1,NTHETA)
      WRITE (NTAPE0,1630)
DO 1530 I=1,NBODYS
1530 WRITE (NTAPE0,1590) XB(I),(VB(I,J),J=1,NTHETA)
      WRITE (NTAPE0,1660) (THETAB(J),J=1,NTHETA)
      WRITE (NTAPE0,1630)
DO 1540 I=1,NBODYS
1540 WRITE (NTAPE0,1590) XB(I),(VTB(I,J),J=1,NTHETA)
1550 CONTINUE
      WRITE (NTAPE0) NBODYS
      WRITE (NTAPE0) (XB(J),J=1,NBODYS)
      WRITE (NTAPE0) (T(J),J=1,NBODYS)
      WRITE (NTAPE0) T1,Tc11
1560 CONTINUE
C-----
C-----
C-----
C-----
C-----
1570 WRITE(NTAPE0,1690) IRR
      GO TO 1560
1580 FORMAT (53H****BODY POINT IS OUTSIDE MACH CONE - PROGRAM HALT IN
1184 SUBROUTINE KARXOR)
1590 FORMAT(1H ,F14.4,F15.5,F29.5,F10.5)
1600 FORMAT(1H//141H BODY GEOMETRY AND SOURCE STRENGTHS, T11=F8.5,5X,
15HT11=F8.5/56X,5HEIRST,9X,6HSECOND,11X,1HT,14X,2HTC/9X
29HX-STATION,7X,6HCAMBER,9X,6HRRADIUS,2X,2(5X,10HDERIVATIVE)//
3(1X, /F15.4))
1610 FORMAT(1H//166H VELOCITY COMPONENTS ON BODY DUE TO BODY LINE SOURCES
AND DOUBLETS)
1620 FORMAT(1H0,4X,11THETA(DEG.),F14.4,9F10.4/(F29.4,9F10.4))
1630 FORMAT(1H ,9X,1HX)
1640 FORMAT(1H0,5X,8HAXIAL(U))
1650 FORMAT(1H0,5X,10HRADIAL(VR))
1660 FORMAT(1H0,5X,14HTANGENTIAL(VT))
1670 FORMAT(1H ,38H VELOCITY COMPONENTS ON NACELLE PAIR (,I2,23H) DUE
11TO NACELLE PAIR (,I2,27H) LINE SOURCES AND DOUBLETS)
1680 FORMAT(1H ,5F15.4)
1690 FORMAT(1H0,18HINTEGRATION ERROR=I2)
END
CDECK FCALC
OVERLAY(CWANG, 7, 7)
PROGRAM FCALC
C-----
C-----
C-----
C-----
C-----
CONTROL SUBROUTINE FOR CALCULATION OF FORCES, MOMENTS
AND PRESSURES
C-----
C-----
COMMON / MAIN / NTAPEA,NTAPEB,NTAPEC,NTAPED,NTAPEE,NTAPEF,NTAPEI,
1 NTAPEO,NBODY,NWING,XMACH,SYM,KACE,NPOLAR,IRW
COMMON /AVAR/ A(210),ACB(21),ABX(100),AWX(110),AREA(210),ARN(2),A00000100
1 RVT(20),ALPHA(210),ALPHAB(210),ALPHAS(210),ALPHAT(100000110
2 10),ALPHAW(110),ALPHAX(110),AWS(110),ABT(100),AM1N(00000120
3 210,2),ALPHAA,ALPHAD,ARA,ARADEG,ARB,ARW,ARAS,AT,AA00000130
COMMON /BVAR/ B(210)
1 BECL,BECLD,BECM
COMMON /CVAR/C(210),CHORD(210),CL(210),CPNN(51,11,2)
1 CLS(210)
2 CDR,CASE,CPCALC,CLEAR,CONSNT,CLEAR,CLX,CLM,CDM
00003790
00003800
00003810
00003820
00003830
00003840
00003850
00003860
00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003960
00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004040
00004050
00004060
00004070
00004080
00004090
00004100
00004110
00004120
00004130
00004140
00004150
00004160
00004170
00004180
00004190
00004200
00004210
00004220
00000020
00000030
00000040
00000050
00000060
00000070
00000100
00000110
00000120
00000130
00000140
00000150
00000170
00000180

```



```

GO TO 1530
1010 CONTINUE
C
C WING-BODY CONFIGURATION
DO 1040 J=1,NBODY
IF (NACEL) 1020,1020,1030
1020 UEN(J)=0.
VEN(J)=0.
WEN(J)=0.
GO TO 1040
1030 UEN(J)=UNCL(J,1)+UNCL(J,2)
VEN(J)=VNCL(J,1)+VNCL(J,2)
WEN(J)=WNCL(J,1)+WNCL(J,2)
1040 CONTINUE
C
C WING ALONE OR WING-BODY CONFIGURATION
1050 CONTINUE
DO 1080 J=1,NWING
UWB(J)=0.
VWB(J)=0.
WWB(J)=0.
IF (NACEL) 1060,1060,1070
1060 UWN(J)=0.
VWN(J)=0.
WVN(J)=0.
GO TO 1080
1070 K=J+NBODY
UWN(J)=UNCL(K,1)+UNCL(K,2)
VWN(J)=VNCL(K,1)+VNCL(K,2)
WVN(J)=WNCL(K,1)+WNCL(K,2)
1080 CONTINUE
IF (NACEL) 1090,1090,1100
1090 XNCLT=0.
XNCLT=0.
XNCLT=0.
GO TO 1120
1100 DO 1110 J=1,NACEL
XNCL(J)=XNCL(J)/REAREA
XNCL(J)=XNCL(J)/REAREA
XNCL(J)=XNCL(J)/((CBAR*REAREA)
XNCLT=XNCL(1)+XNCL(2)
XNCLT=XNCL(1)+XNCL(2)
XNCLT=XNCL(1)+XNCL(2)
1120 CONTINUE
IF (IPOLAR .NE. 0) GO TO 1180
GO TO (1130,1180,1240),KASE
C
C CALCULATE WING ALPHA, GIVEN WING CL KASE = 1
1130 CONTINUE
IF (KONFIG-2) 1140,1160,1160
C
C WING ALONE CONFIGURATION
1140 CONTINUE
CALL CAMEW (NWING,NTAPEE,A,CL,ALPHA)
REWIND NTAPEE
DO 1150 J=1,NWING
ALPHA(J)=ALPHA(J)+ALPHA(J)
GO TO 1320
C
C WING-BODY CONFIGURATION
1160 CONTINUE
CALL FSF (1,NTAPEE,IRR)
CALL DCPI (NEODY,NWING,NTAPEE,A,ABX,CL(NS),CL)
REWIND NTAPEE
CALL CAMEWB (NEODY,NWING,NTAPEE,A,CL(NS),ABX,AWX)

```

```

00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001790
00001800
00001810
00001820
00001830
00001840
00001850
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070

REWIND NTAPEE
REWIND NTAPEF
DO 1170 J=1,NWING
1170 ALPHA(J)=AWX(J)+ALPHAX(J)
GO TO 1320
C
C CALCULATE WING CL, GIVEN WING ALPHA KASE = 2
1180 CONTINUE
IF (KONFIG-2)1190,1210,1210
C
C WING ALONE CONFIGURATION
1190 CONTINUE
DO 1200 J=1,NWING
1200 AX(J)=ALPHAX(J)-ALPHAX(J)
CALL FSF (1,NTAPEE,IRR)
CALL DCPD(NWING,NTAPEE,A,AWX,CL)
REWIND NTAPEE
GO TO 1320
C
C WING-BODY CONFIGURATION
1210 CONTINUE
DO 1220 J=1,NWING
1220 AX(J)=ALPHAX(J)-ALPHAX(J)
DO 1230 J=1,NBODY
READ (NTAPEF) (A(I),I=1,NWING)
DO 1230 I=1,NWING
1230 AX(I)=AWX(I)-A(I)+ABX(J)
CALL FSF (1,NTAPEE,IRR)
CALL DCPD (NWING,NTAPEE,A,AWX,CL(NS))
REWIND NTAPEE
CALL FSF (1,NTAPEE,IRR)
CALL DCP1 (NBODY,NWING,NTAPEF,A,ABX,CL(NS),CL)
REWIND NTAPEF
GO TO 1320
C
C OPTIMIZE CAMBER FOR GIVEN CL, OR FOR GIVEN CL AND CM KASE = 3
1240 CONTINUE
IF (CONSNT)1260,1250,1260
1250 CALL FSF(2,NTAPEA,IRR)
GO TO 1270
1260 CALL FSF(3,NTAPEA,IRR)
1270 CONTINUE
IF (KONFIG-2)1280,1300,1300
C
C WING ALONE CONFIGURATION
1280 CONTINUE
CALL OPTMW (NWING,NTAPEA,A,B,CONSNT,CLBAR,XCPBAR,RFAREA,AREA,CL)
REWIND NTAPEA
CALL CAXW (NWING,NTAPEE,A,CL,ALPHAX)
REWIND NTAPEE
DO 1290 J=1,NWING
1290 ALPHA(J)=ALPHAX(J)+ALPHAX(J)
GO TO 1320
C
C WING-BODY CONFIGURATION
1300 CONTINUE
CALL OPTMB (NWING,NBODY,NTAPEA,NTAPEF,THICK,A,B,ALPHA,ABX,ALPHAX,
1 AREA(NS),CONSNT,CLEAR,XCPBAR,RFAREA,CL(NS))
REWIND NTAPEA
CALL FSF (1,NTAPEF,IRR)
CALL DCP1 (NBODY,NWING,NTAPEF,A,ABX,CL(NS),CL)
REWIND NTAPEF
CALL CAXW (NBODY,NWING,NTAPEE,A,CL(NS),ABX,AWX)
REWIND NTAPEE
REWIND NTAPEF

```



```

DO 1310 J=1,NWING
1310 ALPHA(J)=AMX(J)*ALPHAX(J)
C
C WING ALONE OR WING-BODY CONFIGURATION
1320 CONTINUE
IF (KONFIG-2)1330,1340,1340
C
C WING ALONE CONFIGURATION
1330 CONTINUE
CALL FSF (1,NTAPEB,IRR)
CALL CVEL (NWIN,NWING,NTAPEB,A,B,C,CL,UWW,VWW,WWW)
REWIND NTAPEB
GO TO 1350
C
C WING-BODY CONFIGURATION
1340 CONTINUE
CALL FSF (1,NTAPEB,IRR)
CALL CVEL (NWIN,NBODY,NTAPEB,A,B,C,CL,UWB,VWB,WWB)
CALL FSF (2,NTAPEB,IRR)
CALL CVEL (NWIN,NWING,NTAPEB,A,B,C,CL(NS),UWW,VWW,WWW)
REWIND NTAPEB
CALL RITE(NFMT(6),NTAPEO,NWING,NROW,NCOLW,THETA,UWB,VWB,WWB)
CALL RITE(NFMT(7),NTAPEO,NWING,NROW,NCOLW,THETA,UWB,VWB,WWB)
C
C WING ALONE OR WING-BODY CONFIGURATION
1350 CONTINUE
CALL FSF(10,NTAPEC,IRR)
WRITE (NTAPEC) NPANEL
CALL FOR EOF (NTAPEC)
REWIND NTAPEC
DO 1365 J=1,NWING
JJ=J+NBODY
NJ=(J-1)/NR+1
VSS(J)=VST(J)*CL(JJ)
DO 1365 I=1,NWING
II=I+NBODY
NI=(I-1)/NR+1
IF(1.I7.J.AND.NI.EQ.NJ) VSS(J)=VSS(J)+VS2(I)*CL(II)
1365 CONTINUE
DO 1360 J=1,NWING
JJ=J+NBODY
TJ=THETA(JJ)
COSTJ=COS(TJ)
SINTJ=SIN(TJ)
VWX(J)=VSS(J)*COSTJ
VWY(J)=VSS(J)*SINTJ
IF(THICK.EQ.0.) GO TO 1360
VWX(J)=VSS(J)*COSTJ
VWY(J)=VSS(J)*SINTJ
UWX(J)=UWW(J)-.25*CL(JJ)
DO 1361 J=1,NWING
VWX(J)=VWX(J)+VWX(J)
VWY(J)=VWY(J)+VWY(J)
1361 CALL RITE(NFMT(4),NTAPEO,NWING,NROW,NCOLW,THETA,UWW,VWW,WWW)
DO 1365 J=1,NWING
JJ=J+NBODY
VWX(J)=VWX(J)-2.*VWX(J)
VWY(J)=VWY(J)-2.*VWY(J)
UWX(J)=UWW(J)+.5*CL(JJ)
1365 CALL RITE(NFMT(4),NTAPEO,NWING,NROW,NCOLW,THETA,UWW,VWW,WWW)
DO 1366 J=1,NWING
JJ=J+NBODY
VWX(J)=VWX(J)+VWX(J)
VWY(J)=VWY(J)+VWY(J)

```

```

00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
00002160
00002170
00002180
00002190
00002200
00002210
00002220
00002230
00002240
00002250
00002260
00002270
00002280
00002290
00002300
00002310
00002320
00002330
00002340
00002350
00002360
00002370
00002380
00002381
00002382
00002383
00002384
00002385
00002386
00002387
00002388
00002389
00002390
00002390
00002400
00002401
00002402
00002403
00002404
00002405
00002406
00002407
00002408
00002410
00002412
00002413
00002414
00002420
00002421
00002422
00002423
00002424
00002425
00002426
00002427
00002428
00002429
00002430

```

```

1366 UWN(J)=UWN(J)-.5*CL(JJ)
C COMPUTE COEFFICIENT OF PRESSURE ON WING WITH OR WITHOUT WING
C THICKNESS
CALL RITE(NFMT(5),NTAPEO,NWING,NROWW,NCOLW,THETA,UWMT,VWMT,WMT)
IF (THICK)1370,1410,1370

C WING ALONE OR WING-BODY CONFIGURATION
C WITH WING THICKNESS
1370 CONTINUE
DO 1375 J=1,NWING
  VWMT(J)=VWMT(J)-VWX(J)
  WMT(J)=WMT(J)+WXX(J)
  CALL RITE(NFMT(5),NTAPEO,NWING,NROWW,NCOLW,THETA,UWMT,VWMT,WMT)
DO 1376 J=1,NWING
  VWMT(J)=VWMT(J)+2.*VWX(J)
  WMT(J)=WMT(J)-2.*WXX(J)
  CALL RITE(NFMT(5),NTAPEO,NWING,NROWW,NCOLW,THETA,UWMT,VWMT,WMT)
DO 1377 J=1,NWING
  VWMT(J)=VWMT(J)-VWX(J)
  WMT(J)=WMT(J)+WXX(J)
DO 1380 J=1,NWING
  U(J)=U(J)+UWMT(J)+UWN(J)
  V(J)=V(J)+VWMT(J)+VWN(J)+VWX(J)+VWX(J)
  W(J)=W(J)+WMT(J)+WXX(J)+WXX(J)+WXX(J)+WXX(J)+WXX(J)
  CALL CP(O,NWING,XWACH,CPCALC,U,V,W,CPL,ARA)
  JJ=J+NBODY
DO 1390 J=1,NWING
  U(J)=U(J)+.5*CL(JJ)
  V(J)=V(J)+VWMT(J)+VWMT(J)+VWMT(J)+VWMT(J)+VWMT(J)-VWX(J)
  W(J)=W(J)+WMT(J)+WXX(J)+WXX(J)+WXX(J)+WXX(J)-WXX(J)-WXX(J)
  CALL CP(O,NWING,XWACH,CPCALC,U,V,W,CPL,ARA)
DO 1400 J=1,NWING
  ALPHA(J)=ALPHA(J)+WSS(J)
  ALPHA(J)=ALPHA(J)-WSS(J)
GO TO 1450

C WING ALONE OR WING-BODY CONFIGURATION
C WITHOUT WING THICKNESS
1410 CONTINUE
DO 1420 J=1,NWING
  U(J)=U(J)+UWMT(J)+UWN(J)
  V(J)=V(J)+VWMT(J)+VWMT(J)+VWMT(J)+VWMT(J)+VWMT(J)
  W(J)=W(J)+WMT(J)+WXX(J)+WXX(J)+WXX(J)+WXX(J)
  CALL CP(O,NWING,XWACH,CPCALC,U,V,W,CPL,ARA)
  JJ=J+NBODY
DO 1430 J=1,NWING
  U(J)=U(J)+VWMT(J)+VWMT(J)+VWMT(J)+VWMT(J)-VWX(J)
  W(J)=W(J)+WMT(J)+WXX(J)+WXX(J)+WXX(J)-WXX(J)
  U(J)=U(J)+.5*CL(JJ)
  CALL CP(O,NWING,XWACH,CPCALC,U,V,W,CPL,ARA)
DO 1440 J=1,NWING
  ALPHA(J)=ALPHA(J)
  ALPHA(J)=ALPHA(J)

C WING ALONE OR WING-BODY CONFIGURATION
C CALCULATE CAMBER SHAPE
1450 CONTINUE
JJ=1+(J-1)/NROWW
WAS(J)=ARCT(JJ)/CDR
WAS(J)=COS(WAS(J))*COS(ARAXX)
CALL INTPOL(NWING,NROWW,RATIOX,.5,CHORD(NS),ALPHA,ALPHA)
CALL CAMBER(NCOLW,NROWW,CHORD(NS),ALPHA,CSHAPE,CHORDL)

C COMPUTE COEFFICIENTS OF LIFT, DRAG, MOMENT ON WING

```

```

CALL WLDL (NWMG, NROW, XP, ZP, RFAREA, AREA(NS), XBAR(NS), ZBAR(NS),
X ALPHA, THETA(NS), CPU, WSCDU, WSCDU, WCLU, WCDU, WCMU, YBAR(NS), WAS)
CALL WLDL (NWMG, NROW, XP, ZP, RFAREA, AREA(NS), XBAR(NS), ZBAR(NS),
X ALPHA, THETA(NS), CPU, WSCDU, WSCDU, WCLL, WCDL, WCMU, YBAR(NS), WAS)
DO 1460 J=1, NCOLW
JN=(J-1)*NROW+(NROW+1)/2
JN=NBODY+JN
DY=AREA(JN)/CHORD(JN)
WSCD(J)=WSCDL(J)-WSCDU(J)
WSCJ(J)=WSCLL(J)-WSCLU(J)
1460 CONTINUE
WCL=WCLU-WCLL
WCD=WCDU-WCDL
CONTINUE
WCM=(WCMU-WCML)/CBAR
IF (KONFIG.EQ. 1) GO TO 1540
C
C WING-BODY CONFIGURATION
CALL CVEL (NBODY, NBODY, NTAPED, A, B, C, CL, UBB, VBB, WBB)
CALL FSF (2, NTAPED, IRR)
CALL CVEL (NBODY, NWMG, NTAPED, A, B, C, CL(NS), UBW, VBW, WBW)
REIND NTAPED
DO 1470 J=1, NBODY
UBW(J)=UBW(J)-.25*CL(J)
CALL RATE (NFMT(1), NTAPED, NBODY, NROWB, NTHETA, THETAB, UBB, VBB, WBB)
CALL RATE (NFMT(2), NTAPED, NBODY, NROWB, NTHETA, THETAB, UBW, VBW, WBW)
1470 CONTINUE
C
C COMPUTE COEFFICIENT OF PRESSURE ON BODY WITH OR WITHOUT THE
EFFECT OF WING THICKNESS
IF (THICK) 1480, 1500, 1480
1480 CONTINUE
CALL RATE (NFMT(3), NTAPED, NBODY, NROWB, NTHETA, THETAB, UBWT, VBWT, WBWT)
DO 1490 J=1, NBODY
U(J)=UBW(J)+UBWT(J)+UBN(J)
V(J)=VBW(J)+VBWT(J)+VBN(J)
W(J)=WBW(J)+WBWT(J)+WBN(J)
GO TO 1520
1500 CONTINUE
DO 1510 J=1, NBODY
U(J)=UBW(J)+UBW(J)+UBN(J)
V(J)=VBW(J)+VBW(J)+VBN(J)
W(J)=WBW(J)+WBW(J)+WBN(J)
1510 CONTINUE
1520 CONTINUE
CALL CP(1, NBODY, XMACH, CPCALC, U, V, W, CPB, ARA)
C
C COMPUTE COEFFICIENTS OF LIFT, DRAG, MOMENT ON BODY PANELS
CALL INTPOL (NBODY, NROWB, RATIO, CHORD, ALPHA, THETA, CPB)
CALL BLDL (NBODY, XP, ZP, RFAREA, AREA, XBAR, ZBAR, ALPHA, THETA, CPB)
1, BWCL, BXC, BXCX)
C
C BODY ALONE OR WING-BODY CONFIGURATION
1530 CONTINUE
BECL=EBCL/RFAREA
BBCL=BBCL/RFAREA
BBCL=BBCL/RFAREA
BBCL=BBCL/RFAREA
IF (KONFIG.EQ. 2) GO TO 1540
C
C WING-BODY CONFIGURATION
BXC=BXC/CFAR
BCL=BCL+BBCL
BCD=BCD+BBCL
BCM=BCM+BBCL
WCL=BCL+WCL+XNCLT
WCD=BCD+WCD+XNCLT

```



```

C      WBCM=B*CM+W*CM+X*NNCMT
C      ANY CONFIGURATION
C      WRITE OUTPUT
C 1540 CONTINUE
C      ARA=ARAXX
C      IF (KONFIG-2)1630,1560,1550
C      WING-BODY CONFIGURATION
C 1550 CONTINUE
C      WRITE (NTAPE0,1770)
C      GO TO 1570
C      BODY ALONE CONFIGURATION
C 1560 CONTINUE
C      WRITE (NTAPE0,1820)
C      BODY ALONE OR WING-BODY CONFIGURATION
C 1570 CONTINUE
C      WRITE (NTAPE0,2010) BB*CD,BB*CL,BB*CM
C      WRITE (NTAPE0,1830)
C      WRITE(NTAPE0,1860) (THETB(I),I=1,NTHETB)
C      WRITE (NTAPE0,1870)
C      IF(XMACH-LT.1.) GO TO 1590
C      NES = NEODYS
C      DO 1580 I=1,NEODYS
C      XMIDB(I) = XB(I)
C 1580 WRITE (NTAPE0,1880) XB(I), (CPBB(I,J),J=1,NTHETB)
C      GO TO 1610
C 1590 NES=NEODYS-1
C      DO 1600 I=1,NES
C      XX=5*(XB(I)+XB(I+1))
C      XMIDB(I) = XX
C 1600 WRITE (NTAPE0,1880) XX, (CPBB(I,J),J=1,NTHETB)
C 1610 IF(KONFIG.EQ.2) GO TO 1750
C      WING-BODY CONFIGURATION
C      WRITE (NTAPE0,1790)
C      WRITE (NTAPE0,2010) BW*CD,BW*CL,BW*CM
C      WRITE (NTAPE0,1840)
C      CALL OUTB (NTAPE0,NBODY,NTHETA,NROWB,THETAB,CPB)
C      WRITE (NTAPE0,1850)
C      CALL OUTB (NTAPE0,NBODY,NTHETA,NROWB,THETAB,ALPHAB)
C      WING ALONE OR WING-BODY CONFIGURATION
C 1630 CONTINUE
C      IF (NACEL .EQ. 0) GO TO 1680
C      WING ALONE OR WING-BODY CONFIGURATION WITH NACELLE(S)
C      DO 1670 J=1,NACEL
C      NTN=X*NTN(J)
C      NXN=X*NXN(J)
C      WRITE (NTAPE0,1890) J
C      WRITE (NTAPE0,2010) X*NNCD(J),X*NNCL(J),X*NNCM(J)
C      WRITE (NTAPE0,1900)
C      WRITE (NTAPE0,1860) (THETAN(I,J),I=1,NTN)
C      WRITE (NTAPE0,1870)
C      IF(XMACH-LT.1.) GO TO 1650
C      DO 1640 I=1,NXN
C      1640 WRITE (NTAPE0,1880) XN(I,J), (CPNN(I,K,J),K=1,NTN)
C      GO TO 1670
C      NX=N*NXN-1
C 1650 DO 1660 I=1,NXS

```

```

      XX=5*(XN(I,J)+XN(I+1,J))
1660 WRITE(NTAPE0,1880) XX, (CPNN(I,K,J),K=1,NTN)
1670 CONTINUE
C
1680 CONTINUE
      DO 1690 J=NS,NPANEL
1690 CL(J)=CL(J)
C
      IF (KONFIG-2)1700,1710,1710
C
      WING ALONE CONFIGURATION
1700 CONTINUE
      WRITE (NTAPE0,1810)
      GO TO 1720
C
      WING-BODY CONFIGURATION
1710 CONTINUE
      WRITE (NTAPE0,1780)
C
      WING ALONE OR WING-BODY CONFIGURATION
1720 CONTINUE
      WRITE (NTAPE0,2010) WCD,WCL,WCM
      WRITE (NTAPE0,1980)
      WRITE (NTAPE0,2000) (I,I=1,NCOLW)
      WRITE (NTAPE0,1760) (WSCD(I),I=1,NCOLW)
      WRITE (NTAPE0,1990)
      WRITE (NTAPE0,2000) (I,I=1,NCOLW)
      WRITE (NTAPE0,1760) (WSCD(I),I=1,NCOLW)
      WRITE (NTAPE0,1910)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,CPU)
      WRITE (NTAPE0,1920)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,CPL)
      WRITE (NTAPE0,1930)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,CL(NS))
      IF (THICK)1730,1740,1730
1730 WRITE (NTAPE0,1950)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,ALPHAU)
      WRITE (NTAPE0,1960)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,ALPHA)
      WRITE (NTAPE0,1970)
      CALL OUTW (NTAPE0,NWING,NCOLW,NROWW,ALPHA)
      WRITE (NTAPE0,1940)
      WRITE (NTAPE0,1760) (CHORDL(I),I=1,NCOLW)
C
      IF (KONFIG.EQ.1) GO TO 1750
C
      WING-BODY CONFIGURATION
      WRITE (NTAPE0,1800)
      WRITE (NTAPE0,2010) WBCC,WBCL,WBCM
C
      ANY CONFIGURATION
1750 CONTINUE

```

REDUCE POLAR BY 1 FOR EACH PASS

POLAR = POLAR - 1

00004720
00004740
00004750
00004760
00004770
00004780
00004790
00004800

FORMAT STATEMENTS
1760 FORMAT(1H, F29.5, 9F10.5)
1770 FORMAT(1H1, 48H PRESSURES, FORCES, AND MOMENTS ON ISOLATED BODY)
1780 FORMAT(1H1, 66H PRESSURES, FORCES, AND MOMENTS ON WING PANELS IN P00004800

AD-A048 840

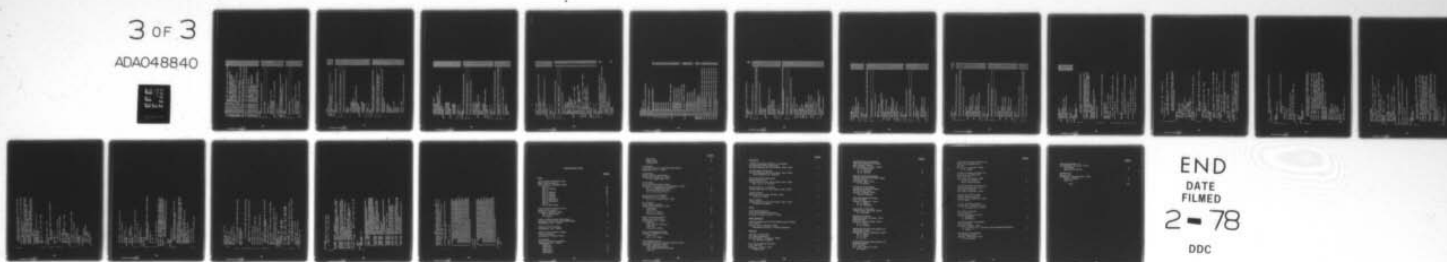
MCDONNELL DOUGLAS ASTRONAUTICS CO HUNTINGTON BEACH CALIF F/G 1/1
AERODYNAMIC COMPUTER CODE FOR COMPUTING PRESSURE LOADING ON COM--ETC(U)
JAN 78 K K WANG
MDC-67215

UNCLASSIFIED

NL

3 OF 3

ADAO48840



END
DATE
FILMED
2-78
DDC


```

1790 FORMAT(1H1, 70H INCREMENTAL PRESSURES, FORCES, AND MOMENTS ON BODY)
1 PANELS DUE TO WING)
1800 FORMAT(1H1, 44H FORCES AND MOMENTS ON WING-BODY COMBINATION)
1810 FORMAT(1H1, 38H PRESSURES, FORCES AND MOMENTS ON WING)
1820 FORMAT(1H1, 38H PRESSURES, FORCES AND MOMENTS ON BODY)
1830 FORMAT(1H0/32H BODY PRESSURE COEFFICIENTS(CP))
1840 FORMAT(1H0/37H BODY PANEL PRESSURE COEFFICIENT(CP))
1850 FORMAT(1H0/25H BODY PANEL SLOPE(DR/DX))
1860 FORMAT(1H0, 4X, 11H THETA( DEG. ), F14.4, 9F10.4, / (F29.4, 9F10.4))
1870 FORMAT(1H, 2X, 1H X)
1880 FORMAT(1H, F14.4, F15.5, 9F10.5, / (F29.5, 9F10.5))
1890 FORMAT(1H1, 57H PRESSURES, FORCES, AND MOMENTS ON ISOLATED MACELLES)
1 PAIR, 12)
1900 FORMAT(1H0/34H MACELLE PRESSURE COEFFICIENTS(CP))
1910 FORMAT(1H0/52H UPPER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP))
1920 FORMAT(1H0/52H LOWER SURFACE WING PANEL PRESSURE COEFFICIENTS(CP))
1930 FORMAT(1H0/36H WING PANEL PRESSURE DIFFERENCE(CL))
1940 FORMAT(1H0/23H WING CHORD LENGTHS(C))
1950 FORMAT(1H0/39H UPPER SURFACE WING PANEL SLOPE(DZ/DX))
1960 FORMAT(1H0/39H LOWER SURFACE WING PANEL SLOPE(DZ/DX))
1970 FORMAT(1H0/26H WING CAMBER SLOPE(DZ/DX))
1980 FORMAT(1H0/25H SECTION CL DISTRIBUTION)
1990 FORMAT(1H0/25H SECTION CL DISTRIBUTION)
2000 FORMAT(1H0, 2X, 14H SPANWISE STATION, 18, 9110, / (18X, 18, 9110))
2010 FORMAT(1H0/6H CD =, F10.5, 10X, 4HCL =, F10.5, 10X, 4HCM =, F10.5)
END

CHECK OUTW
SUBROUTINE OUTW (NTAPE0, NWING, NCOLW, NROWW, Z)
C
C .....
C WING OUTPUT FORMAT
C .....
C
C DIMENSION Z(1)
C
C WRITE (NTAPE0, 1010) (I, I=1, NCOLW)
C WRITE (NTAPE0, 1020)
C DO 1000 J=1, NROWW
C 1000 WRITE (NTAPE0, 1030) (J, (Z(I), I=J, NWING, NROWW))
C
C RETURN
C
1010 FORMAT(1H0, 2X, 16H SPANWISE STATION, 18, 9110, / (18X, 18, 9110))
1020 FORMAT(1H, 2X, 17H CHORDWISE STATION)
1030 FORMAT(1H, 110, F19.5, 9F10.5, / (F29.5, 9F10.5))
END

CHECK OUTB
SUBROUTINE OUTB (NTAPE0, NBODY, NTHETA, NROWB, THETA, Z)
C
C .....
C BODY OUTPUT FORMAT
C .....
C
C DIMENSION Z(1), THETA(1)
C
C WRITE (NTAPE0, 1010) (THETA(I), I=1, NTHETA)
C WRITE (NTAPE0, 1020)
C DO 1000 J=1, NROWB
C 1000 WRITE (NTAPE0, 1030) (J, (Z(I), I=J, NBODY, NROWB))
C
C .....

```

```

00004810
00004820
00004830
00004840
00004850
00004860
00004870
00004880
00004890
00004900
00004910
00004920
00004930
00004940
00004950
00004960
00004970
00004980
00004990
00005000
00005010
00005020
00005030
00005040
00005050
00005060
00005070
00005080

```

```

C -----
C RETURN
1010 FORMAT(1H0,4X,11THETA(DEG.),F14.4,9F10.4/(F29.4,9F10.4))
1020 FORMAT(1H0,6X,7NROW NO.)
1030 FORMAT(1H,110,F19.5,9F10.5/(F29.5,9F10.5))
C -----
C END
CDECK BLD
SUBROUTINE BLD (NM,XP,ZP,RFAREA,AREA,XBAR,ZBAR,ALPHAM,THETAM
1,CPM,CL,CD,CM)
C
C .....
C COMPUTES COEFFICIENT OF LIFT, DRAG, AND MOMENT ON BODY
C .....
C .....
C DIMENSION AREA(1),XBAR(1),ZBAR(1),ALPHAM(1),THETAM(1),CPM(1)
C
C DRAG=0.
C XLIFT=0.
C XM=0.0
C
C DO 1000 J=1,NM
C F=CPM(J)*AREA(J)
C XL=F*COS(THETAM(J))
C XD=F*ALPHAM(J)
C XM=XX-XL*(XBAR(J)-XP)+XD*(ZBAR(J)-ZP)
C XLIFT=XLIFT+XL
C DRAG=DRAG+XD
C 1000 CONTINUE
C
C CL=XLIFT/RFAREA
C CD=DRAG/RFAREA
C CM=XM/RFAREA
C
C -----
C RETURN
C -----
C END
CDECK WLD
SUBROUTINE WLD (NM,NROW,XP,ZP,RFAREA,AREA,XBAR,ZBAR,ALPHAM,
1 THETAM,CPM,SCL,SCD,CL,CD,CM,YBAR,AMS)
C
C .....
C COMPUTES COEFFICIENT OF LIFT, DRAG, AND MOMENT ON WING
C SPANWISE DISTRIBUTION OF LIFT AND DRAG COEFFICIENTS
C .....
C .....
C DIMENSION AREA(1),XBAR(1),ZBAR(1),ALPHAM(1),THETAM(1),CPM(1)
C 1,SCL(1),SCD(1),YBAR(1)
C DIMENSION AMS(1)
C
C PI=3.14159
C NCOL=NM/NROW
C WDRAG=0.
C WXLIFT=0.
C WXM=0.
C J=0
C DO 1010 K=1,NCOL
C DRAG=0.
C XLIFT=0.
C SUM=0.0
C CON=1.0
C
C DO 1000 I=1,NROW
C J=J+1
C IF(1.EQ.1) TEST=ABS(YBAR(J))+ABS(ABS(THETAM(J))-.5*PI)

```

OUTB1140
OUTB1150
OUTB1160
OUTB1170
OUTB1180

BLDM1000
BLDM1010
BLDM1020
BLDM1030
BLDM1040
BLDM1050
BLDM1060
BLDM1070
BLDM1080
BLDM1090
BLDM1100
BLDM1110
BLDM1120
BLDM1130
BLDM1140
BLDM1150
BLDM1160
BLDM1170
BLDM1180
BLDM1190
BLDM1200
BLDM1210
BLDM1220
BLDM1230
BLDM1240
BLDM1250
BLDM1260
BLDM1270
BLDM1280

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000105
00000110
00000111
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000201
00000210
00000220
00000230
00000231


```

NWRIT=NP
DO 8 N=1, NP
IF (NTEST.LE.3) GO TO 6
NN=N*NBODY
AN(N)=W(N)*COS(THETA(NN))-V(N)*SIN(THETA(NN))
GO TO 8
6 THETB=THET(N)
AN(N)=W(N)*COS(THETB)-V(N)*SIN(THETB)
8 CONTINUE
IGO=NFMT
GO TO(10,20,30,40,50,60,70,300,200), IGO
10 WRITE (NTAPE0,6030)
GO TO 200
20 WRITE (NTAPE0,6040)
GO TO 200
30 WRITE (NTAPE0,6045)
GO TO 200
40 WRITE (NTAPE0,6050)
GO TO 300
50 WRITE (NTAPE0,6055)
GO TO 300
60 WRITE (NTAPE0,6060)
GO TO 300
70 WRITE (NTAPE0,6065)
GO TO 300
C 200 CONTINUE
PRINT OUT VELOCITY COMPONENTS AT BODY PANELS
WRITE (NTAPE0,6010)
CALL OUTB (NTAPE0, NP, NCOL, NROW, THETA, U)
WRITE (NTAPE0,6015)
CALL OUTB (NTAPE0, NP, NCOL, NROW, THETA, V)
WRITE (NTAPE0,6020)
CALL OUTB (NTAPE0, NP, NCOL, NROW, THETA, W)
WRITE (NTAPE0,6025)
CALL OUTB (NTAPE0, NWRIT, NCOL, NROW, THETA, AN)
GO TO 999
C 300 CONTINUE
PRINT OUT VELOCITY COMPONENTS AT WING PANELS
WRITE (NTAPE0,6010)
CALL OUTW (NTAPE0, NP, NCOL, NROW, U)
WRITE (NTAPE0,6015)
CALL OUTW (NTAPE0, NP, NCOL, NROW, V)
WRITE (NTAPE0,6020)
CALL OUTW (NTAPE0, NP, NCOL, NROW, W)
WRITE (NTAPE0,6025)
CALL OUTW (NTAPE0, NWRIT, NCOL, NROW, AN)
6000 FORMAT(1H, 10F11.5)
6010 FORMAT(1H0, 5X, 8HAXIAL(U))
6015 FORMAT(1H0, 5X, 13HTRANSVERSE(V))
6020 FORMAT(1H0, 5X, 11HVERTICAL(W))
6025 FORMAT(1H0, 5X, 9HNORMAL(N))
6030 FORMAT(1H1, 76H VELOCITY COMPONENTS ON BODY PANELS DUE TO BODY PAN
1RCES)
6040 FORMAT(1H1, 76H VELOCITY COMPONENTS ON BODY PANELS DUE TO WING PAN
1RCES)
6045 FORMAT(1H1, 55H VELOCITY COMPONENTS ON BODY PANELS DUE TO WING SOU
1RCES)
6050 FORMAT(1H1, 76H VELOCITY COMPONENTS ON WING PANELS DUE TO WING PAN
1RCES)
6055 FORMAT(1H1, 55H VELOCITY COMPONENTS ON WING PANELS DUE TO WING SOU
1RCES)
6060 FORMAT(1H1, 76H VELOCITY COMPONENTS ON WING PANELS DUE TO BODY PAN
1RCES)
6065 FORMAT(1H1, 73H VELOCITY COMPONENTS ON WING PANELS DUE TO BODY LIN
1E SOURCES AND DOUBLET)

```

010
011
012
013
014
015
016
017
018
019
020
021
022
023
024
027
028
029
030
031
032
033
034

035
036
038
039
040
041
042
043
044

047
048
049
050

051
052
053
054
055
056
057
058
059
060
061
062
063
064

6070 FORMAT(1H0,5HNFMT=,110,18HIN SUBROUTINE RITE)

066
067

999 CONTINUE
RETURN

END

CDECK CVEL

C SUBROUTINE CVEL(M,N,NTAPEX,A,B,C,CL,U,V,W)

C COMPUTES VELOCITY COMPONENTS FOR A GIVEN PANEL PRESSURE DIFFERENCE

C CVEL1000

C CVEL1010

C CVEL1020

C CVEL1030

C CVEL1040

C CVEL1050

C CVEL1060

C CVEL1070

C CVEL1080

C CVEL1090

C CVEL1100

C CVEL1110

C CVEL1120

C CVEL1130

C CVEL1140

C CVEL1150

C CVEL1160

C CVEL1170

C CVEL1180

C CVEL1190

C CVEL1200

C CVEL1210

C CVEL1220

C CVEL1230

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE

C OPTIMIZE WING-BODY CASE


```

1090 CONTINUE
DO 1100 J=1,NW
1100 CL(J)=0.
DO 1110 J=1,NW
READ (NTAPEX) (A(I),I=1,NW)
DO 1110 I=1,NW
1110 CL(I)=CL(I)+A(I)*B(J)
C -----
C RETURN
C -----
C END
CDECK OPTMW
SUBROUTINE OPTMW (NW,NTAPEX,A,B,CONSNT,CLBAR,XCPBAR,RFAREA,AREA,CL)
1)
C .....
C OPTIMIZE WING ONLY CASE
C .....
C .....
C DIMENSION A(1),B(1),AREA(1),CL(1)
C
NN=NW+3
B(NN)=CLBAR*RFAREA
C
NN=NN+3
C TEST IF PITCHING MOMENT CONSTRAINT
IF (CONSNT)1000,1010,1000
1000 CONTINUE
NN=NN+2
B(NN)=XCPBAR*CLBAR*RFAREA
1010 CONTINUE
DO 1020 J=1,NW
1020 CL(J)=0.
DO 1050 J=1,NW
READ (NTAPEX) (A(I),I=1,NW)
IF (J-NW)1050,1050,1030
1030 CONTINUE
DO 1040 I=1,NW
1040 CL(I)=CL(I)+A(I)*B(J)
1050 CONTINUE
C -----
C RETURN
C -----
C END
CDECK DCPD
SUBROUTINE DCPD (NM,NTAPEX,A,ALPHAM,CLM)
C .....
C COMPUTES WING PANEL PRESSURE DIFFERENCE
C .....
C .....
C DIMENSION A(1),ALPHAM(1),CLM(1)
C
DO 1000 J=1,NM
CLM(J)=0.0
1000 CONTINUE
C
DO 1010 J=1,NM
READ (NTAPEX) (A(I),I=1,NM)
DO 1010 I=1,NM
CLM(I)=CLM(I)+A(I)*ALPHAM(J)
1010 CONTINUE
C -----
C

```

OPTM1350
OPTM1360
OPTM1370
OPTM1380
OPTM1390
OPTM1400
OPTM1410
OPTM1420
OPTM1430
OPTM1440
OPTM1450

CLOPTM1000
OPTM1010
OPTM1020
OPTM1030
OPTM1040
OPTM1050
OPTM1060
OPTM1070
OPTM1080
OPTM1090
OPTM1100
OPTM1110
OPTM1120
OPTM1130
OPTM1140
OPTM1150
OPTM1160
OPTM1170
OPTM1180
OPTM1190
OPTM1200
OPTM1210
OPTM1220
OPTM1230
OPTM1240
OPTM1250
OPTM1260
OPTM1270
OPTM1280
OPTM1290
OPTM1300

DCPD1000
DCPD1010
DCPD1020
DCPD1030
DCPD1040
DCPD1050
DCPD1060
DCPD1070
DCPD1080
DCPD1090
DCPD1100
DCPD1110
DCPD1120
DCPD1130
DCPD1140
DCPD1150
DCPD1160
DCPD1170
DCPD1180

```

C -----
C RETURN
C -----
C END
CDECK CAMBWB
C SUPERROUTINE CAMBWB (NB,NW,NTAPEX,NTAPEY,A,CLW,ALPHAB,ALPHAW)
C
C .....
C FOR WING-BODY CASES, COMPUTES NORMAL VELOCITY COMPONENTS ON WING
C .....
C
C DIMENSION A(1),ALPHAW(1),ALPHAB(1),CLW(1)
C
C DO 1000 J=1,NW
C   ALPHAW(J)=0.
C 1000 CONTINUE
C DO 1010 J=1,NW
C   READ (NTAPEX) (A(I),I=1,NW)
C   DO 1010 I=1,NW
C     ALPHAW(I)=ALPHAW(I)+A(I)*CLW(J)
C 1010 CONTINUE
C DO 1020 J=1,NB
C   READ (NTAPEY) (A(I),I=1,NW)
C   DO 1020 I=1,NW
C     ALPHAW(I)=ALPHAW(I)+A(I)*ALPHAB(J)
C 1020 CONTINUE
C
C -----
C RETURN
C -----
C END
CDECK DCPI
C SUPERROUTINE DCPI (NB,NW,NTAPEX,A,ALPHAB,CLW,CLB)
C
C .....
C COMPUTES BODY PANEL PRESSURE DIFFERENCE
C .....
C
C DIMENSION A(1),ALPHAB(1),CLW(1),CLB(1)
C
C DO 1000 J=1,NB
C   CLB(J)=0.
C 1000 CONTINUE
C DO 1010 J=1,NB
C   READ (NTAPEX) (A(I),I=1,NB)
C   DO 1010 I=1,NB
C     CLB(I)=CLB(I)+A(I)*ALPHAB(J)
C 1010 CONTINUE
C DO 1020 J=1,NW
C   READ (NTAPEX) (A(I),I=1,NB)
C   DO 1020 I=1,NB
C     CLB(I)=CLB(I)+A(I)*CLW(J)
C 1020 CONTINUE
C
C -----
C RETURN
C -----
C END
C SUPERROUTINE CAMBW(NW,NTAPEX,A, CLW,ALPHAW)
C
C .....
C FOR WING ONLY CASE, COMPUTES NORMAL VELOCITY COMPONENTS ON WING
C .....
C
C DIMENSION A(1),ALPHAW(1),CLW(1)
C

```

DCPD1190
DCPD1200

CAMB1000
CAMB1010
CAMB1020
CAMB1030
CAMB1040
CAMB1050
CAMB1060
CAMB1070
CAMB1080
CAMB1090
CAMB1100
CAMB1110
CAMB1120
CAMB1130
CAMB1140
CAMB1150
CAMB1160
CAMB1170
CAMB1180
CAMB1190
CAMB1200
CAMB1210
CAMB1220
CAMB1230
CAMB1240

DCPI1000
DCPI1010
DCPI1020
DCPI1030
DCPI1040
DCPI1050
DCPI1060
DCPI1070
DCPI1080
DCPI1090
DCPI1100
DCPI1110
DCPI1120
DCPI1130
DCPI1140
DCPI1150
DCPI1160
DCPI1170
DCPI1180
DCPI1190
DCPI1200
DCPI1210
DCPI1220
DCPI1230
DCPI1240

CAMB1000
CAMB1010
CAMB1020
CAMB1030
CAMB1040
CAMB1050
CAMB1060
CAMB1070

MCDONNELL DOUGLAS


```

C      WRITE (6,801) ( X(I), Y(I), COF(I), I=1, NC1 )
C      CALL SURFIT( X, Y, NC3, COF)
C      DO 230 K=1, NC3
C      CF( K, NW, 1 ) = COF( K )
C      230 CONTINUE
C      DO 215 J =1, NC1
C      JA = J + ( NW-1 ) * NPT
C      COF( J ) = CPL( JA ) * PCONV
C      215 CONTINUE
C      WRITE (6,802) ( X(I), Y(I), COF(I), I=1, NC1 )
C      CALL SURFIT( X, Y, NC3, COF)
C      DO 240 K=1, NC3
C      CF( K, NW, 2 ) = COF( K )
C      240 CONTINUE
C      250 CONTINUE
C      COMPUTES PRESSURE AT DESIRED LOCATION ( CENTROID OF ELEMENT ),
C      FOR EACH COMPLETE WING.
C      CALL PWING( NW )
C      NW = NW + 1
C      IF ( NW .LE. NWG ) GO TO 10
C      801 FORMAT (1H0,*, PRESSURE AT CONTROL POINT - UPPER SURFACE*/ 15X,
C      1 *X*,9X,*Y*,9X,*PRESSURE*/((11X,F8.4,2X,F8.4,2X,E12.4) )
C      802 FORMAT (1H0,*, PRESSURE AT CONTROL POINT - LOWER SURFACE*/ 15X,
C      1 *X*,9X,*Y*,9X,*PRESSURE*/((11X,F8.4,2X,F8.4,2X,E12.4) )
C      803 FORMAT (1H1,*, TOTAL LIFTING PRESSURE ON THE WING AT THE*
C      A * CONTROL POINT*/15X,*X*
C      1 9X,*Y*,9X,*PRESSURE*/((11X,F8.4,2X,F8.4,2X,E12.4) )
C      RETURN
C      END
C      PWING
C      SUBROUTINE PWING( NW )
C      INTERPOLATES PRESSURE ON WING AT GIVEN LOCATION X,Y FOR
C      LOCATION XC, YC OR CENTROID OF ELEMENT
C      COMMON/COEFFB/ CF(100, 4, 2)
C      COMMON/CORTRN/ NSYN,NTRANS(20), ISYM(20), VA(3,2,20), BTFM(9,2,20)
C      COMMON/PBDATA/ NEODYS, XMIDB(51), NTHETB, THETB(11), CPBB(51,11)
C      1,XCB(3,700), NG(350), NELM(700), NE,NGRIDP,PINF,IPUNCH,CPB
C      2 SID(20)
C      COMMON/PCORD/ X(210) Y(210), NP
C      COMMON/ WINGOT/ CPU, CPL, NWG, ISOLID,IFORM(10)
C      DIMENSION CPU(110), CPL(110)
C      DIMENSION P(210)
C      DIMENSION CPB(110), XI(3,350)
C      INTEGER CHECK, WORD1
C      DATA WORD1/ 5HCQUAD/
C      WRITE TITLE OF WING PRESSURE OUTPUT

```

```

IF ( NW .GT. 1 ) GO TO 50
WRITE (6,901)
WRITE (6,908) NWG
CONTINUE
50 CONTINUE
WRITE (6,910) NW
NPUNCH = 0
NSID = IFIX( SID(NSYM) )
NS = 2
IF ( ISOLID .NE. 0 ) NS = 1
DO 150 K=1,NS
    CHECK SIGN OF SID(NSYM) FOR PRESSURE OUTPUT SIGN AS DESIRED.
    ASID = ABS( SID(NSYM) )
    PSIGN = SID(NSYM) / ASID
    NSID = IFIX( ASID )
    READ IN FINITE ELEMENT SPECIFICATIONS FROM PING OUTPUT CARDS.
    READ (5,902) NGRIDP, NE
    CALL CONV( XI, NG, NGRIDP, NSYM, ISYM )
    CALL COORD( XI, NGRIDP )
    CALL CENTRO( XI, XCB, NG, NGRIDP, NMLM, NE )
    DO 100 IE = 1, NE
        CHANGE THE SIGN OF Y COORDINATE OF THE LEFT WING TO REFLECT THE SYMMETRY OF WING ARRANGEMENT
        YCOORD = ABS( XCB( 2, IE ) )
        SUM = CF(1,NW,K) + CF(2,NW,K)*XCB(1,IE) + CF(3,NW,K)*YCOORD
        DO 110 J = 1, NP
            J3 = J + 3
            RI = ( XCB(1,IE) - X(J) )**2 + ( YCOORD - Y(J) )**2
            IF ( RI .LT. 1.E-9 ) GO TO 110
            SUM = SUM + CF( J3, NW, K ) * RI * ALOG( RI )
        110 CONTINUE
        P(IE) = SUM * PSIGN
    100 CONTINUE
    IF ( IFORM(NW) .NE. 1 ) NSYM = NSYM
    IF ( IFORM(NW) .EQ. 1 ) NSYM = NSYM + 1
    IF ( ISOLID .EQ. 0 .AND. K .EQ. 1 ) WRITE (6,903)
    IF ( ISOLID .EQ. 0 .AND. K .EQ. 2 ) WRITE (6,904)
    WRITE (6,909)
    WRITE (6,906) ( NMLM(J), XCB(1,J), XCB(2,J), P(J), J=1,NE )
    PUNCH PRESSURE AND GRID POINT IDENTIFICATION IN THE FORM OF BULK DATA FORMAT OF NASTRAN
    IF ( IPUNCH .EQ. 0 ) GO TO 150
    DO 220 L=1, NE
        PUNCH 807, ( NSID, P(L), NMLM(L) )
    220 CONTINUE
    NPUNCH = NPUNCH + NE

```



```

1 2P, ZA
1 COMMON/REDATA/ NBOODYS, XNIDB(51), NTHETB, THETB(11), CPBB(51,11)
1 XCB(3,700) NG(350) NEM(700) NE, NGRIDP, PINF, IPUNCH, CPB
COMMON/CORTAN/ NSYM, NTRANS(20), ISYM(20), VA(3,2,20), BTM(9,2,20)
COMMON/RINGOT/ CPU, CPL, NMG, ISOLID, IEORM(10)
COMMON/EXTRA/ ARAN, DSB1, DSB2, DS1, DS2, NB1, NB2, NS1, NS2,
1 NTN, NXN, XN0SE
C
C DIMENSION CPU(110), CPL( 110), CPB(110), XNS1(2), XNS2(2), NS1(2),
1 NS2(2), DS1(2), DS2(2)
C
C REWIND 12
1 IF ( 12M .EQ. 2 ) GO TO 100
C
C WRITE(12) DATE, NTAPEA, NTAPEB, NTAPEC, NTAPEF, NTAPEE, NTAPEF, NTAPEI,
1 NTAPEO, NBOODY, XNMG, XNACH, SYM, KACE, DRDX, DZDX, NPOLAR, A,
2 ACB, ABX, AXZ, AREA, ARN, ARNT, ALPHA, ALPHAB, ALPHAS,
3 ALPHAT, ALPHAN, ALPHAX, AWS, ABT, ANIN, ALPHAA, ALPHAD, ARAT,
4 ARADeg, ARB, ARW, ARAS, AT, AAA, NUMEOD, XNOS, TNOS, ZNOS, NBSTAT,
5 B, BBCL, BBOD, BBOD, C, CHORD, CL, CPNN, CLS, CDR, CASE, CPCALC, CBAR,
6 CONSN, CLEAR, CLX, CLM, CDM, D, DZDXB, DADEG, DARAD, IPOLAR, KASE, KONFIG,
7 KPOLAR, NEXT, NROW, NS, NPANEL, NACEL, NROWE, NROW, NCOL, NTHETA,
8 NTHETS, NMLE, NRG, NPOL, NCLX, POLAR, A, RM, RATIOX, RFAREA, SEMIS, SLC,
9 TITLE, THETA, THETAB, THETAS, THETAN, TCL, TCD, TCM, THICK, TWIST, UBMT,
A UMBT, UMBT, UNCL, VENT, VMBT, VMBT, VNCL, VOUT, VMBT, VMBT, VMBT, VNCL,
B XBAR, XC, XN1, XNIN, XNIN, XB, XN, XNCD, XNCL, XNIN, XN1, XCL, XCD, XP,
C XNACL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL,
D XNIDB, NTHETB, THETB, CPBB, XCB, NS, NEM, NE, NGRIDP, PINF, IPUNCH, CPB,
E NSYM, NTRANS, ISYM, VA, BTM, CPU, CPL, NMG, ISOLID, ARAN, DSB1, DSB2, DS1,
F DS2, NS1, NS2, NTN, NXN, XN0SE
C GO TO 200
C
C 100 CONTINUE
C
C READ (12) DATE, NTAPEA, NTAPEB, NTAPEC, NTAPEF, NTAPEE, NTAPEF, NTAPEI,
1 NTAPEO, NBOODY, XNMG, XNACH, SYM, KACE, DRDX, DZDX, NPOLAR, A,
2 ACB, ABX, AXZ, AREA, ARN, ARNT, ALPHA, ALPHAB, ALPHAS,
3 ALPHAT, ALPHAN, ALPHAX, AWS, ABT, ANIN, ALPHAA, ALPHAD, ARAT,
4 ARADeg, ARB, ARW, ARAS, AT, AAA, NUMEOD, XNOS, TNOS, ZNOS, NBSTAT,
5 B, BBCL, BBOD, BBOD, C, CHORD, CL, CPNN, CLS, CDR, CASE, CPCALC, CBAR,
6 CONSN, CLEAR, CLX, CLM, CDM, D, DZDXB, DADEG, DARAD, IPOLAR, KASE, KONFIG,
7 KPOLAR, NEXT, NROW, NS, NPANEL, NACEL, NROWE, NROW, NCOL, NTHETA,
8 NTHETS, NMLE, NRG, NPOL, NCLX, POLAR, A, RM, RATIOX, RFAREA, SEMIS, SLC,
9 TITLE, THETA, THETAB, THETAS, THETAN, TCL, TCD, TCM, THICK, TWIST, UBMT,
A UMBT, UMBT, UNCL, VENT, VMBT, VMBT, VNCL, VOUT, VMBT, VMBT, VMBT, VNCL,
B XBAR, XC, XN1, XNIN, XNIN, XB, XN, XNCD, XNCL, XNIN, XN1, XCL, XCD, XP,
C XNACL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL, XNCL,
D XNIDB, NTHETB, THETB, CPBB, XCB, NMG, NEM, NE, NGRIDP, PINF, IPUNCH, CPB,
E NSYM, NTRANS, ISYM, VA, BTM, CPU, CPL, NMG, ISOLID, ARAN, DSB1, DSB2, DS1,
F DS2, NS1, NS2, NTN, NXN, XN0SE
C 200 CONTINUE
C REWIND 12
C
C END

```

DISTRIBUTION LIST

	<u>Copies</u>
<u>Navy</u>	
Naval Surface Weapons Center	
White Oak Laboratory	
Silver Spring, Maryland 20910	
WA-30	1
WA-30 (Huang)	30
WA-31	1
WA-31 (Matra)	10
WA-31 (Kiddy)	10
WA-31 (Graff)	1
WA-11 (Hardy)	1
WA-43 (Edwards)	1
WR-15 (Kushner)	1
WX-21	3
WS-10 (Reinhard)	1
Naval Surface Weapons Center	
Dahlgren Laboratory	
Dahlgren, Virginia 22448	
DK-74 (Blackman)	1
DG (Soper)	1
Office of Chief of Naval Operations	
Operations Evaluation Group (OP-03EG)	
Washington, D. C. 20350	1
Defense Nuclear Agency	
Washington, D. C. 20301	2
Defense Documentation Center	
Cameron Station	
Alexandria, Virginia 22314	12
Commander	
Naval Sea Systems Command	
Washington, D. C. 20360	
SEA-03A	1
SEA-0333	1
SEA-035-13	2
SEA-035A	1
SEA-55212	1

	<u>Copies</u>
SEA-0632	2
SEA-654312	1
PMS-403-02	1
Commander Naval Air Systems Command (AIR-320-B) Washington, D. C. 20360	1
Commander Pacific Missile Test Center Point Mugu, California 93042 T. W. Elliott (Code 5331)	1
Commander Naval Air Development Center Johnsville, Warminster, Pennsylvania 18974 Dr. E. McQuillan (Code 3033) Herman Rubin (Code 3033) K. T. Yen (Code 30331)	1 1 1
Naval Research Laboratory Washington, D. C. 20390 Dr. M. R. Achter (Code 6340)	1
Commander Naval Weapons Center China Lake, California 93557 Code 4062 Code 45703 Mr. E. L. Jeter James E. Serpanos	1 1 1 1
Office of Naval Research Department of the Navy Washington, D. C. 20360 Code 461 Code 439 (N. Perrone) Code 470 Technical Library	1 1 1 2
Naval Postgraduate School Monterey, California 93940 Code 2124 Dr. J. G. Cantin	1 1
Commanding Officer Naval Ship Research and Development Center Bethesda, Maryland 20034 Code 1844 (Jim McKee) Code 1844 (Gordon Everstine) Code 564	1 1 2

Copies

Air Force

AFFDL/PTS (CAPT Gilbert L. Camburn)
AF Flight Dynamics Laboratory
Wright-Patterson Air Force Base, Ohio 45433 1

AF Materials Laboratory
Wright-Patterson Air Force Base, Ohio 45433
Code MAAN (B. R. Emrich) 1

Flight Dynamics Laboratory
Structures Division
Wright-Patterson Air Force Base, Ohio 45433
Mr. Leo J. D. Bernier 1

AFML/LLM (W. G. Ramke)
Wright Patterson Air Force Base, Ohio 45433 1

AFATL/DLRV
Eglin Air Force Base, Florida 32542
James M. Heard 2

AFAL/TEM-3
Wright-Patterson Air Force Base, Ohio 45433
Richard A. Ireland 1

Army

Commanding General
U.S. Army Missile Command
Redstone Arsenal, Alabama 35809 1

Other Agencies

NASA Scientific and Technical Information Facility
P. O. Box 33
College Park, Maryland 20740
Acquisitions Branch - Foreign Exchange 2

Industry

Aerospace Corporation
1111 East Mill Street
San Bernardino, California 92408
Dr. Robert L. Hallse 1

Booz Allen Applied Research
P. O. Box 874
Shalimar, Florida 32579
William Day 1

	<u>Copies</u>
Applied Physics Laboratory The Johns Hopkins University 8621 Georgia Avenue Silver Spring, Maryland 20910	
L. B. Weckesser	1
W. C. Caywood	1
R. M. Rivello	1
Battelle Memorial Institute Defense Metals Information Center 505 King Avenue Columbus, Ohio 43201	
H. D. Moran	1
Brunswick Corporation Technical Products Division 325 Brunswick Lane Marion, Virginia 24354	
Robert Copeland	1
General Dynamics/Pomona P.O. Box 2507 Pomona, California 91766	
R. A. Miller	1
D. A. Underhill	1
University of Maryland College Park, Maryland 20740	
Dr. Schaeffer	1
Raytheon Company Missile Systems Division, VB1-3 Hartwell Road Bedford, Massachusetts 01730	
R. D. Howe	1
D. H. Sanders	1
McDonnell Douglas Astronautics Co. 5301 Bolsa Avenue Huntington Beach, California 92647	
W. F. Bozich	1
K. K. Wang	1
R. S. Lee	1
McDonnell Douglas Astronautics Co. Eastern Division P.O. Box 516 St. Louis, Missouri 63166	
J. Gubser	1

Copies

Lockheed Missiles and Space Co.
Dept 81-12, Building 154
Box 504
Sunnyvale, California 94088
J. A. Bailie

1

Lockheed Missile and Space Co.
Dept 52-30, Building 103
P.O. Box 504
Sunnyvale, California 94088
Robert M. Beasley
Senior Staff Scientist

1

1

Lockheed Missile and Space Co.
Technical Information Center
3251 Hanover Street
Palo Alto, California 94034

1

Hughes Aircraft Company
Missile System Division
Canoga Park, California 91340
R. J. Oedy

1

Hughes Aircraft Company
Culver City, California 90230
L. E. Gates, M.S. H-164

1

The Boeing Company
P.O. Box 3999
Seattle, Washington 98124
R. Blaisdell
K. Brettmann

1

1

Martin-Marietta Corporation
P.O. Box 5837
Orlando, Florida 32805

G. H. Sprague, Jr. (Director Aeromechanical Division)
G. Fotieo

1

1

Honeywell, Incorporated
600 2nd Street North
Hopkins, Minnesota 55343
J. D. Brannan

1

Fairchild Republic Co.
Farmingdale, New York 11735
Jim Clarke
Mail Stop Z-19A-08

Copies

1
1

Raytheon Co.
Spencer Lab
Burlington, Massachusetts 01803
Doris A. Holden
Dept 7113

1
1

Total

150